

During the period that the temporary superheater (fig. 20) was being installed, a series of runs was made using steam at line temperatures - approximately 240°F. Steam from the main plant supply was put through a reducing valve and then through a steam-jacketed section of line to insure that it would be dry. Immediately before the connection to the generator, the line was trapped and a bleed connection used so that the line could be thoroughly warmed before starting.

The test procedure for these runs was as follows:

1. The generator was brought up to approximately 2,200°F. using the regular heat-up burner.
2. With the heat-up burner on, the steam flow was adjusted to the desired amount and the generator vent valve closed.
3. Using the steam and products of combustion from the generator and CO₂ added at the Aerotec hoppers, the dust-removal train was purged.
4. On completion of purging the generator burner was shut off and the coal-oxygen feed started at the desired rates.
5. The usual tests were made and readings taken as outlined for runs 1-14.
6. These runs were of approximately 3-to 6-hour duration.

Tests Made Using Steam at 1,600°-2,000°F. (runs 26-31)

After the temporary steam superheater (figs. 20 and 21) was completed, trial steam runs were made, and then gasifying runs made on Sewickley and Wyoming coals.

The test procedures for these runs were as follows:

1. The generator was heated to approximately 2,200°F. using the heat-up burner and the hot products of combustion from the superheater.
2. The steam was turned on about 3 hours before the start of the run and so adjusted that, when mixed with the products of combustion from the superheater, the desired superheated steam temperature was obtained. This procedure was followed so that the superheater would be at steady operating conditions before the coal-oxygen feed was started. With steam from the superheater at 2,000°F. the generator temperature at this stage was approximately 2,100°F. or about 300°F. lower than the temperature reached near the end of the runs.
3. Using the combined steam and ROC from the generator and CO₂ added at the Aerotec hoppers, the dust train was purged. The generator heat-up burner was shut off after purging.
4. When the unit was purged, the coal-oxygen feed was started at the predetermined rate.

5. The small increase in generator pressure caused by gasification made necessary some slight readjustments in the flows of gas and steam to the superheater.

6. During the test the usual samples were taken and temperatures and flows recorded as in the other runs.

7. The POC from the superheater was sampled every half hour and complete analyses made. Since there had been some variations in the composition of the natural gas supplied to this area, a sample of this gas was also taken once during the run for complete analysis. For control purposes, Orsat samples were run on the POC from the superheater every 20 to 30 minutes.

RESULTS

In general, the pilot plant performed very well. Continuous operation was possible, the runs being terminated voluntarily when the residue containers became full. The performance data that follow indicate that this process could furnish low-cost synthesis gas on a commercial scale. The percentage gasification of the coal was very high and the oxygen requirement lower than any other oxygen process known.

Calculated Results of Gasification Runs

The calculated results of the gasification runs are presented in tables 1, 2 and 3, the first table being for the high-temperature steam runs, the second for the low-temperature steam runs, and the third for the intermediate-temperature steam runs. Before the results of a run were calculated, the data collected during the run were averaged with respect to time, and temperature and pressure corrections made where necessary. Gas samples were analyzed for CO_2 , O_2 , illuminants, H_2 , CO , and CH_4 . Residue samples were analyzed for moisture, volatile matter, fixed carbon, ash, and particle-size distribution. Columns 1 to 7 give the conditions used in the experiments and columns 8 to 23 present the average results of the experiments. Columns 24 to 32 show the results in terms of calculated ratios.

Material balances on carbon, hydrogen, and oxygen are given in columns 33 to 59. Since synthesis-gas measurements for the first eight runs were inaccurate, results for these eight runs are based on residue data. Results beginning with run 9, when the Roots-Connersville gas meter was installed, are based on the carbon determined by the synthesis-gas measurement. Since the measurements of moisture in the synthesis gas leaving the generator were of doubtful accuracy (discussed later), the undecomposed steam in the synthesis gas was calculated as the average of the determinations from the hydrogen and oxygen balances.

TABLE I. - Calculated results on pilot-plant runs, using high-temperature steam (runs 1 - 14)

Run No.	Duration, hr.	Raw-coal rate, lb./hr.	Process-steam rate, lb./hr.	Process-oxygen rate, S.C.F./hr.	Steam-inlet temp., °F.	Steam/lb. raw coal, lb.	Oxygen/lb. raw coal, lb.	Synthesis-gas analysis, percent					Outlet temp., °F.	Gross heating value, B.t.u./S.C.F.	Syn. gas, thousands of S.C.F./hr.	(CO + H ₂)', thousands of S.C.F./hr.	H ₂ :CO ratio
								CO ₂	H ₂	CO	CH ₄	N ₂					
1	9.47	211.5	4.03	4	2,960	2.28	0.47	21.1	51.4	28.8	2.6	-4.3	1,893	296.0	7.59	6.99	1.78
2A	2.80	200.0	293	1,116	3,048	2.97	.47	24.4	46.2	21.1	2.7	4.3	1,920	251.1	8.35	5.62	2.19
2B	8.13	257.7	609	1,469	3,022	2.36	.48	19.3	49.2	27.3	3.0	-6	1,934	247.2	10.49	7.99	1.80
3	7.83	293.7	737	1,534	2,816	2.51	.47	17.7	43.8	27.9	2.3	6.5	2,091	263.6	11.57	6.30	1.57
4A	7.75	309.0	674	1,664	2,772	2.18	.46	16.8	44.6	26.9	2.0	7.5	2,134	269.3	12.99	9.29	1.66
4B	.57	314.0	820	1,692	2,385	2.61	.46	19.6	45.6	25.5	2.5	5.4	2,120	269.3	12.61	9.09	1.63
4C	2.33	354.0	866	1,887	2,850	2.45	.45	16.7	43.5	27.4	2.1	7.7	2,139	269.3	14.71	10.43	1.59
5	7.73	299.0	752	1,765	2,889	2.52	.51	20.6	46.3	28.3	1.6	1.6	2,096	263.5	11.83	8.82	1.64
6A	.63	186.0	581	1,170	2,630	3.12	.53	19.1	49.4	26.8	1.5	2.9	2,123	267.6	8.40	6.40	1.84
6B	2.25	232.0	667	1,460	2,638	2.88	.53	19.5	47.8	27.5	1.1	3.8	2,105	258.1	10.09	7.60	1.74
7	5.43	236.0	815	1,740	2,783	3.42	.62	22.2	55.9	27.1	2.0	-8.3	2,035	298.5	9.75	8.09	2.06
8	8.00	200.4	498	1,220	3,195	2.49	.52	18.1	50.3	27.6	2.3	-1	1,808	283.5	8.16	6.36	1.62
9A	2.87	207.0	507	1,086	3,096	2.45	.44	19.0	41.2	26.3	1.5	11.6	1,915	238.1	10.14	6.84	1.57
9B	3.00	193.3	506	954	3,043	2.63	.42	17.3	43.0	25.9	2.5	10.3	1,960	259.1	10.03	6.91	1.66
9C	3.00	187.0	507	669	3,050	2.71	.39	15.4	48.7	25.6	2.1	6.7	1,960	269.4	9.67	7.18	1.90
10	9.50	198.5	502	856	3,058	2.53	.36	17.8	51.2	25.8	2.6	2.1	1,790	282.6	8.18	6.30	1.98
11	6.10	245.0	510	853	3,055	2.08	.29	17.4	52.7	28.5	3.1	-2.0	1,935	301.2	8.88	7.17	1.85
12	5.52	247.0	507	853	3,303	2.05	.29	16.9	49.0	26.5	3.0	3.9	1,905	281.8	8.68	6.55	1.85
13	5.00	311.6	505	1,150	2,777	1.62	.31	15.2	49.1	30.5	2.9	1.8	1,915	294.5	8.94	7.12	1.61
14	5.00	305.4	500	1,153	2,706	1.64	.32	16.5	53.1	30.6	3.2	-3.9	1,910	307.8	9.00	7.04	1.74
Ave.	4.80	249.5	607	1,268	2,904	2.18	.44	18.6	48.2	27.1	2.3	2.8	1,984	273.7	10.00	7.46	1.78

Generator temp., °F.

Run No.	4.5 ft. above floor o. generator.	11.5 ft. above floor of generator	16.5 ft. above floor of generator	In horizontal outlet	Lb./hr.	Carbon, percent	Oxygen, S.C.F.	Ratios/l,000 S.C.F.(CO:F ₂)		Ration/lb. raw coal					
								Steam introduced, lb.	Steam decomposed, lb.	Process oxygen, S.C.F.	Steam introduced, lb.	Steam decomposed, lb.	Synthetic gas, S.C.F.	CO + H ₂ , S.C.F.	
1	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
2A	2,291	1,697	1,893	1,550	38.9	64.5	34.7	193.6	79.3	15.5	5.58	2.28	0.45	39.9	28.8
2B	2,170	1,904	1,920	1,452	24.8	63.7	35.6	198.6	105.6	19.8	5.58	2.97	.56	41.7	28.1
3	2,341	2,027	1,930	(1)	30.9	63.7	32.2	183.8	76.2	17.7	5.70	2.36	.55	40.5	31.0
4A	2,360	2,097	2,091	1,968	49.6	70.0	35.4	197.0	88.8	16.4	5.56	2.51	.46	39.4	28.2
4B	2,322	2,049	2,134	1,674	46.8	69.9	33.3	179.6	72.6	18.4	5.39	2.18	.55	42.0	30.1
4C	2,320	1,936	2,120	2,002	47.5	69.9	34.5	186.2	90.2	20.2	5.39	2.61	.59	40.1	28.9
5	2,396	2,022	2,139	2,018	53.6	69.9	33.9	180.9	63.0	18.0	5.33	2.45	.53	41.5	29.5
6	2,400	2,220	2,096	2,018	3.0	85.2	33.9	202.3	85.2	17.2	5.97	2.52	.51	39.6	29.5
6A	2,275	2,372	2,123	1,968	12.7	61.0	29.1	182.8	90.8	9.5	6.29	3.12	.33	45.2	31.4
6B	2,330	2,380	2,105	1,987	24.0	61.0	30.5	192.1	87.8	13.1	6.29	2.88	.43	45.5	32.8
7	2,412	2,395	2,035	1,912	24.1	46.8	29.4	215.1	100.7	15.8	7.31	3.42	.54	41.0	34.0
8	2,202	1,870	1,868	1,644	30.9	62.9	31.5	191.9	78.4	16.8	6.09	2.49	.53	40.7	31.7
9A	2,265	1,977	1,935	1,822	23.1	63.4	30.3	155.8	74.2	22.2	5.15	2.45	.73	48.9	33.0
9B	2,312	1,991	1,950	1,870	35.1	63.3	28.0	138.0	73.5	23.6	4.94	2.63	.94	51.8	35.7
9C	2,296	2,008	1,960	1,883	44.9	66.1	26.1	121.0	70.6	22.7	4.55	2.71	.87	51.7	38.4
10	2,172	1,865	1,790	1,675	61.5	69.1	31.5	135.0	79.7	21.6	4.28	2.53	.69	41.2	31.7
11	2,172	1,905	1,935	1,813	54.6	70.9	34.2	119.0	70.0	21.2	3.48	2.08	.62	35.0	29.3
12	2,150	1,905	1,795	1,525	75.0	37.7	130.2	77.4	20.3	3.45	2.05	.54	35.2	26.6	
13	2,192	1,906	1,915	1,807	116.6	72.0	43.7	161.9	72.0	15.3	3.69	1.62	.35	28.7	22.9
14	2,165	1,935	1,910	1,842	116.8	71.7	40.5	153.0	66.3	16.9	3.78	1.64	.42	29.5	24.7
Ave.	2,281	2,019	1,984	1,837	46.7	67.0	33.3	170.9	81.1	18.1	5.20	2.48	0.55	40.7	30.5

(1) F.C. net working.

TABLE 1. - Calculated results on pilot plant runs, using high temperature steam (runs 1 - 14) - Cont.

Carbon balance										Hydrogen balance										Run No.
					Based on measurement of gas volume					Based on measurement of residue					Hydrogen balance					Run No.
Run No.	C ₂ in coal, lb./hr.	O ₂ in P.O.C. entering generator, lb./hr.	Total carbon in coal, lb./hr.	Total carbon in P.O.C. entering gen., lb./hr.	Total carbon in coal, lb./hr.	Total carbon gasified, %	Total carbon gasified, %	Total carbon gasified, %	Total carbon gasified, %	H ₂ in coal, lb./hr.	In dry syn. gas, lb./hr.	In uncomposed steam, lb./hr.	Total H ₂ gen., lb./hr.	In dry syn. gas, lb./hr.	In uncomposed steam, lb./hr.	Run No.				
1	58	49	50	51	52	53	54	55	56	57	58	59	58	59	60	61	62	63	64	1
2	13.4	30.7	429.4	99.5	573.0	288.1	344.9	389.7	388.0	389.8	390.0	390.2	390.4	390.6	390.8	391.0	391.2	391.4	391.6	2
3	21.0	32.0	527.2	94.2	664.3	246.6	417.7	494.1	489.9	482.0	593.0	111.0	1,623	1,074	1,130	1,132	1,134	1,136	1,138	3
4	16.3	26.9	541.3	124.0	708.5	290.9	417.6	465.3	465.8	467.5	609.0	141.4	1,866	1,137	1,146	1,148	1,150	1,152	1,154	4
5	10.5	18.8	655.2	138.0	830.5	310.5	520.0	637.4	585.0	601.2	737.0	135.8	2,207	1,137	1,146	1,148	1,150	1,152	1,154	5
6	19.5	6.4	599.0	140.5	765.4	333.2	432.2	519.3	486.0	502.8	674.0	171.2	2,078	1,143	1,152	1,154	1,156	1,158	1,160	6
7	19.0	3.2	729.0	142.3	894.7	345.8	548.9	655.2	617.5	636.4	820.0	183.5	2,137	1,143	1,152	1,154	1,156	1,158	1,160	7
8	22.4	9.5	769.9	159.4	961.3	378.6	582.7	700.2	655.5	677.8	866.0	188.2	2,165	1,143	1,152	1,154	1,156	1,158	1,160	8
9	18.9	22.1	668.5	150.7	860.2	347.4	522.8	622.8	576.9	599.8	752.0	152.2	2,034	1,137	1,146	1,148	1,150	1,152	1,154	9
10	6A	11.8	63.5	516.5	98.9	710.7	231.1	479.6	500.4	539.6	520.3	581.0	61.0	2,287	1,127	1,132	1,134	1,136	1,138	10
11	6B	14.7	62.1	593.0	123.2	793.0	284.5	508.5	565.2	572.1	567.7	667.0	99.3	2,257	1,132	1,134	1,136	1,138	1,140	11
12	15.0	43.2	724.5	146.9	929.5	295.5	634.1	660.6	713.4	687.0	815.0	128.0	2,214	1,132	1,134	1,136	1,138	1,140	12	
13	12.5	22.4	642.9	103.0	580.8	220.4	360.4	377.1	405.5	391.3	498.0	106.7	2,003	1,137	1,146	1,148	1,150	1,152	13	
14	19.4	12.2	450.9	89.9	568.4	281.0	281.4	392.0	317.0	355.0	507.0	152.0	2,100	1,136	1,145	1,147	1,149	1,151	14	
15	14.1	12.5	451.5	80.6	558.7	274.0	281.7	370.0	322.0	345.0	508.0	163.0	2,120	1,139	1,148	1,150	1,152	1,154	15	
16	13.0	12.2	450.9	73.3	550.2	252.0	298.2	351.9	336.0	341.0	507.0	163.0	2,140	1,140	1,142	1,144	1,146	1,148	16	
17	13.8	12.6	446.4	71.7	544.7	225.0	319.7	372.0	360.0	366.0	502.0	135.0	2,170	1,148	1,150	1,152	1,154	1,156	17	
18	17.0	11.8	453.4	72.0	554.2	248.0	306.2	372.0	345.0	358.0	510.0	152.0	2,165	1,149	1,151	1,153	1,155	1,157	18	
19	17.3	15.0	450.9	72.0	555.2	238.0	317.2	390.0	357.0	374.0	507.0	133.0	2,240	1,136	1,138	1,140	1,142	1,144	19	
20	21.8	16.9	448.9	97.0	584.6	248.0	336.6	412.0	379.0	396.0	505.0	109.0	2,525	1,130	1,132	1,134	1,136	1,138	20	
21	21.1	18.6	444.5	97.3	581.5	259.0	322.5	383.0	363.0	373.0	500.0	127.0	2,275	1,158	1,160	1,162	1,164	1,166	21	
22	Ave.	16.4	23.6	539.7	108.7	688.5	277.2	411.3	480.5	462.9	471.7	607.0	135.4	2,125	1,136	1,138	1,140	1,142	1,144	22

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TABLE I. - Calculated results of pilot-plant runs, using high-temperature steam (Runs 1 - 14) - Cont.																		
Heat balance, millions of B.t.u. per hour																		
	Run No.	In undecomposed steam, lb./hr.	Net heat of combustion of coal	Sensible heat in steam	Sensible heat in 20°C. gases	Total heat in	Net heat of combustion of gas	Sensible heat in gas	Sensible heat in undecomposed steam	Sensible heat of residue	Net heat of combustion of unburned C	Total heat out	Heat loss measured by heat balance, B.t.u./hr.	Calculated heat loss from shell, 10° B.t.u./hr.	Calculated heat stored in bricks 10° B.t.u./hr.	Calculated heat loss, B.t.u./hr.		
9	1	51.7	2,556	.62	.63	.64	.65	.66	.67	.68	.69	.70	.71	.72	.73	.74	.75	
9	2	68.6	2,513	.990	.110	3,613	1,905	.422	.468	.014	.223	3,032	.581	.068	.276	.1,720	.1,754	
9	3	57.7	3,238	1.003	.119	4,365	2,714	.501	.558	.017	.285	3,975	.390	1/	1/	1/	1/	
9	4	72.8	3,708	1.126	.056	4,890	2,770	.604	.636	.030	.503	4,525	.365	.095	.159	.865	.865	
9	5	77.8	3,901	1.004	.018	4,923	3,069	.628	.553	.029	.473	4,752	.171	1/	1/	1/	1/	
9	6	69.2	3,931	1.011	.000	4,942	3,072	.601	.695	.029	.482	4,859	.083	1/	1/	1/	1/	
9	7	55.6	4,469	1.331	.030	5,830	3,469	.721	.747	.033	.543	5,513	.317	.154	.435	1,661	1,661	
9	8	62.8	3,775	1.173	.072	5,020	2,825	.600	.646	.019	.381	4,479	.541	.114	.163	.926	.926	
9	9	73.4	41.9	2,318	.868	.238	3,454	2,026	.866	.960	.008	.11	3,581	.127	1/	1/	1/	
9	10	43.5	2,929	.982	.178	4,089	2,352	.719	.614	.015	.212	3,912	.177	.103	.315	.1,802	.1,802	
9	11	41.1	3,009	1.213	.092	4,310	2,618	.511	.715	.015	.165	4,024	.286	.108	.314	.1,773	.1,773	
9	12	39.1	2,550	.904	.081	3,515	2,091	.312	.354	.016	.282	3,085	.430	.113	.257	.546	.546	
9	13	41.3	2,594	.874	.041	3,509	2,197	.453	.320	.010	.000	2,980	.529	.130	.241	.1,792	.1,792	
9	14	41.4	2,422	.857	.041	3,320	2,348	.462	.320	.010	.000	3,140	.180	.137	.109	.1,273	.1,273	
9	15	43.4	2,343	.857	.040	3,240	2,352	.457	.321	.009	.000	3,139	.101	.137	.003	.749	.749	
9	16	45.7	2,395	.851	.043	3,269	2,068	.347	.297	.024	.223	2,979	.310	.114	.156	1,360	1,360	
9	17	42.5	11	2,956	.865	.039	3,860	2,397	.412	.318	.043	.432	3,602	.256	.117	.000	.478	.478
9	18	53.4	12	2,980	.952	.053	3,965	2,214	.405	.328	.053	.596	3,595	.389	.158	.082	.976	.976
9	19	13	3,759	.767	.020	4,516	2,388	.430	.350	.089	1,100	4,357	.219	.163	.041	.655	.655	
9	20	14	3,685	.735	.054	4,474	2,501	.438	.341	.083	.980	4,343	.131	.151	.168	.56	.56	
equilib-			Ave.	3,107	.928	.072	4,138	2,472	.513	.471	.028	.360	3,823	.285	.122	.166	1,224	1,224

1 Not counted in vertical averages.

Thermal efficiencies

Run No.	A	B	C	D
	76	77	78	79
1	77.1	57.7	75.4	82.5
2A	75.8	52.7	73.6	71.9
2B	83.8	62.2	80.6	85.2
3	74.7	56.6	78.0	85.2
4A	78.7	62.3	82.9	89.7
4B	78.1	62.2	82.3	91.1
4C	77.6	59.2	80.9	87.4
5	74.8	56.3	77.5	82.8
6A	86.4	58.7	82.3	84.6
6B	83.3	57.5	80.0	83.6
7	87.7	60.7	84.8	87.5
8	82.6	59.5	76.4	82.1
9A	84.7	62.6	81.3	81.3
9B	96.9	70.7	90.8	90.8
9C	100.4	72.6	92.9	92.9
10	87.2	63.5	80.1	84.9
11	81.1	62.1	78.4	86.2
12	79.3	55.6	71.4	81.8
13	63.5	52.2	68.3	65.1
14	67.9	55.9	70.5	85.9
Ave	80.7	60.1	79.5	85.4

- A. Net heat of combustion of gas (B.t.u.)/net heat of combustion of coal.
 - B. Net heat of combustion of gas (B.t.u.)/total heat in.
 - C. Net heat of combustion of gas plus sensible heat in undecomposed steam and in dry gas above 400°F./total heat in.
 - D. Net heat of combustion of gas plus sensible heat in undecomposed steam and in dry gas above 400°F. plus 70% of the heat of combustion of ungasified carbon/total heat in.

TABLE 2. - Calculated results on pilot-plant runs, using low-temperature steam (runs 15A - 253)

Run No.	Duration, hr.	Process-coal rate, lb./hr.	Process-steam rate, lb./hr.	Process oxygen rate, S.C.F./hr.	Input ratios	Synthesis gas	Synthesis-gas analysis, percent							Gross heating value B.t.u./S.C.F.	Syn.gas, thousands cu. S.C.F./hr.	(CO+H ₂), thousands of S.C.F./hr.	H ₂ :CO ratio
							CO ₂	H ₂	CO	CH ₄ + N ₂	CO ₂	H ₂	CO	CH ₄ + N ₂	CO ₂	H ₂	CO
15A 1.50	1.50	242.3	381	2,792	25	6	7	8	9	10	11	12	13	14	15	16	17
15B 2.00	2.00	242.3	318	2,723	245	1.31	.95	33.7	33.3	28.3	2.5	1.4	1,713	231.6	8.41	5.19	1.18
15C 3.00	242.3	245	2,614	245	1.01	.92	30.2	35.8	26.6	2.7	3.5	1,763	238.1	8.22	5.13	1.35	
16A 2.33	264.0	243	2,654	235	1.92	.85	24.6	36.3	29.2	2.1	1.6	1,811	236.9	8.26	5.41	1.24	
16B 1.19	264.0	297	2,659	237	1.13	.85	24.4	37.4	35.1	2.0	.5	1,870	254.3	9.00	6.46	1.02	
16C 2.40	264.0	345	2,659	240	1.31	.85	27.0	36.4	31.8	1.2	3.1	1,948	236.6	9.50	6.48	1.07	
17	6.00	245.6	146	2,550	233	.59	.88	13.7	36.4	45.8	1.6	1.0	2,010	208.1	8.61	7.10	.80
18	7.00	230.4	98	2,370	234	.43	.87	19.5	32.3	50.6	1.9	1.9	1,913	292.9	7.34	6.08	.44
19	6.50	245.7	60	2,171	230	.21	.75	3.4	27.1	64.7	1.9	1.9	2,030	322.5	7.36	6.79	.42
20	2.50	477.5	298	4,830	241	.62	.86	16.8	35.1	43.8	2.0	1.7	1,843	261.7	15.04	11.88	.86
21	4.50	406.9	315	3,968	242	.77	.83	18.0	37.8	40.9	1.9	.9	2,103	280.8	12.37	9.73	.93
22A	1.50	487.4	260	4,061	235	.53	.71	18.1	36.2	43.9	1.2	.3	1,867	275.6	12.51	10.02	.83
22B	2.00	487.4	278	4,069	237	.27	.71	15.8	37.0	44.5	1.7	.7	1,938	287.8	13.62	11.10	.83
23A	1.50	458.0	182	3,725	235	.40	.69	12.2	36.3	48.9	1.5	.8	1,955	291.5	12.35	10.52	.74
23B	2.50	458.0	172	3,526	235	.38	.65	10.5	35.1	50.6	2.2	1.1	1,975	306.3	12.39	10.45	.69
24A	1.00	477.0	95	3,322	235	.19	.59	6.5	34.3	54.4	2.9	.8	1,880	323.1	11.33	10.05	.63
24D	2.00	477.0	90	3,193	235	.19	.57	6.5	35.9	54.1	2.5	.7	1,895	323.9	11.39	10.25	.66
25A	1.25	446.0	178	3,785	245	.40	.72	12.4	35.5	50.6	.8	.3	1,950	291.6	12.55	10.81	.70
25B	3.75	446.0	176	4,120	245	.40	.84	11.2	32.5	51.8	1.5	2.1	2,060	294.4	13.58	11.45	.63
Ave.	2.89	361.2	220	3,270	238	.68	.79	17.2	35.1	43.7	1.9	1.3	1,915	280.1	10.70	8.52	.86

Run No.	Generator temp., °F. -			In horizontal outlet of generator	Residue (dry basis)	Ratios/1,000 S.C.F.(CO + H ₂)		Ratios/lb. raw coal		Steam introduced, lb.	Steam decomposed, lb.	Process oxygen, S.C.F.	Steam decomposed, lb.	Synthetic gas, S.C.F.	CO + H ₂ , S.C.F.
	4.5 ft. above floor of generator	11.5 ft. above floor of generator	16.5 ft. above floor of generator			Oxygen, S.C.F.	Coal, lb.	CO	CH ₄						
18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	
15A 2,162	1,780	1,713	1,620	56.3	56.3	538.0	74.0	15.2	11.5	1.56	.347	31.7	31.4		
15B 2,100	1,858	1,763	1,700	57.6	56.5	531.0	69.0	16.1	11.2	1.31	.297	33.9	21.2		
15C 2,195	1,920	1,811	1,765	56.5	55.9	44.3	469.0	45.3	14.3	10.9	1.01	.339	34.1	22.3	
16A 2,115	1,870	1,825	1,758	13.0	66.3	40.8	411.0	37.6	12.9	10.1	.92	.314	34.1	24.5	
16B 2,238	1,932	1,870	1,803	91.7	56.4	38.0	383.0	42.7	14.8	10.1	1.13	.390	36.4	26.4	
16C -----	2,040	1,948	1,681	29.9	54.0	40.0	410.0	53.2	15.0	10.1	1.31	.368	36.0	24.4	
17	2,311	2,100	2,040	51.7	56.9	34.6	359.0	20.6	8.2	10.4	.59	.238	35.2	28.9	
18	2,358	1,960	1,913	46.1	54.1	37.9	390.0	16.1	3.3	10.3	.43	.141	31.8	26.4	
19	2,481	2,108	2,030	60.1	61.9	36.2	320.0	8.8	3.7	6.0	.24	.103	29.8	27.5	
20	2,455	2,080	1,843	1,690	92.2	54.8	40.3	407.0	25.1	6.9	10.1	.62	.172	31.5	24.8
21	2,468	2,107	2,103	1,978	59.1	52.8	41.8	408.0	32.4	7.3	9.8	.77	.174	30.4	23.9
22A 2,182	-----	1,867	1,760	106.5	62.3	48.6	405.2	25.9	4.8	8.3	.53	.099	25.7	20.6	
22B 2,291	-----	1,938	1,840	75.2	62.3	43.9	366.6	25.0	5.5	8.4	.57	.142	27.9	22.8	
23A 2,230	2,030	1,955	1,820	107.4	62.1	43.5	354.0	17.3	4.6	8.1	.49	.106	27.0	23.0	
23B 2,310	2,060	1,975	1,830	104.9	62.4	43.8	337.5	16.5	4.8	7.7	.38	.110	26.6	22.6	
24A -----	2,120	-----	1,735	84.0	66.1	47.5	330.5	9.1	2.6	7.0	.19	.055	23.8	21.1	
24B -----	2,355	-----	1,750	123.8	66.5	46.5	311.5	8.8	3.1	6.7	.19	.066	23.9	21.5	
25A 2,347	2,028	1,950	-----	91.4	58.7	41.3	320.1	16.5	5.0	8.5	.40	.120	28.1	24.2	
25B 2,375	2,165	2,060	1,845	56.6	51.0	39.0	386.1	15.5	4.0	9.9	.40	.103	30.4	25.7	
Ave. 2,306	2,018	1,918	1,603	71.8	58.6	42.3	354.1	29.1	8.1	9.4	.68	.193	30.6	23.9	

TABLE 2. - Calculated results on pilot-plant runs, using low-temperature steam (runs 15A - 25B). - Cont.

Carbon balance		Hydrogen balance											
		Based on measurement of gas volume					Based on measurement of residue						
Run No.	Total carbon in coal, lb./hr.	Fixed carbon in coal, lb./hr.	Carbon in syn. gas, lb./hr.	Ungasified carbon, lb./hr.	Total carbon gasified, %	Fixed carbon gasified, %	Total carbon gasified, %	Fixed carbon gasified, %	H ₂ in coal, lb./hr.	H ₂ in steam, lb./hr.	Total to gen., lb./hr.	In dry syn. gas, lb./hr.	In undecomposed steam, lb./hr.
15A	172.6	121.9	175.1	2.5	101.4	102.1	81.6	75.4	10.1	42.7	52.8	17.1	35.7
15B	172.6	121.9	158.9	13.7	92.1	88.8	81.1	74.7	20.1	35.3	45.1	18.0	27.4
15C	172.6	121.9	162.9	9.8	94.3	92.0	82.6	75.1	10.1	27.3	37.4	17.7	19.7
16A	187.9	133.3	180.3	7.6	96.0	94.3	86.1	80.3	11.1	27.0	38.1	19.0	19.1
16B	187.9	133.3	189.1	1.2	100.6	100.9	86.1	80.3	11.1	27.0	38.1	19.0	19.1
16C	187.9	133.3	182.2	5.7	97.0	95.7	85.1	80.3	11.1	33.0	44.1	21.0	23.1
Ave.	257.1	189.7	216.5	40.6	86.9	82.2	83.4	77.4	15.1	24.4	39.5	22.1	17.5

Oxygen balance				Steam balance				Computed equilibrium temperatures					
Run No.	O ₂ in coal, lb./hr.	O ₂ in steam, lb./hr.	Trace oxygen, lb./hr.	Total O ₂ generator, lb./hr.	In dry synthesis gas, lb./hr.	In undecomposed steam, lb./hr.	Undecomposed steam from H ₂ balance, lb./hr.	Undecomposed steam from O ₂ balance, lb./hr.	Average undecomposed steam, lb./hr.	Total steam introduced, lb./hr.	Steam decomposed, lb./hr.	Shift reactor, °F.	C°CO ₂ reaction, °F.
15A	49	50	51	52	53	54	55	56	57	58	59	60	61
15B	17.6	541.4	235.8	594.8	348.0	246.8	322.0	278.0	300.0	384.0	94.0	1,910	1,109
15C	17.6	282.9	230.1	530.6	312.0	218.6	247.0	265.0	246.0	318.0	72.0	1,780	1,110
16A	17.6	216.2	223.4	459.2	316.0	141.2	177.6	159.0	168.3	215.5	77.2	1,580	1,135
16B	19.2	264.0	224.6	507.8	347.0	160.8	208.0	184.0	160.0	243.0	83.0	1,730	1,182
16C	19.2	306.9	224.6	550.7	350.0	200.7	270.0	226.0	248.0	345.0	97.0	1,806	1,177
Ave.	27.9	195.5	276.1	499.5	356.8	142.7	157.2	160.6	158.8	219.9	61.1	2,159	1,256

TABLE 2. - Calculated results of pilot-plant runs, using low-temperature steam (runs 15A - 25B) - Cont.

Heat balance, millions of B.t.u., per hour

Run No.	Ket heat of combustion of coal	Sensible heat in steam	Total heat in	Net heat of combustion of gas	Sensible heat in gas	Sensible heat in undecomposed steam	Sensible heat of residue	Net heat of combustion of unburned C	Total heat out	Heat loss measured by heat balance, B.t.u./hr.	Calculated heat loss from shell 10 ⁶ B.t.u./hr.	Calculated heat stored in bricks, 10 ⁶ B.t.u./hr.	Calculated heat loss, B.t.u./lb. coal
15A	62	63	65	66	67	68	69	70	71	72	73	74	75
15A	2,920	0.032	2,952	1,766	0.298	0.237	0.015	0.000	2,334	0.618	0.070	0.423	2,035
15B	2,920	.026	2,946	1,762	.302	.202	.022	.145	2,433	.513	.073	.322	1,630
15C	2,920	.020	2,940	1,826	.314	.146	.022	.136	2,424	.516	.085	.107	.792
16A	3,180	.019	3,199	2.11	.346	.139	.023	.129	2,748	.451	.105	.891	3,773
16B	3,180	.024	3,204	2,281	.300	.172	.016	.000	2,849	.325	.108	.396	1,909
16C	3,180	.028	3,208	2,063	.397	.232	.022	.071	2,785	.423	.113	.390	1,905
17	3,005	.013	3,016	2,320	.384	.082	.021	.071	2,878	.340	.114	.355	1,908
18	2,816	.008	2,824	2,018	.300	.056	.023	.162	2,559	.265	.087	.419	2,196
19	3,003	.005	3,008	2,259	.325	.031	.024	.128	2,767	.241	.106	.077	.745
20	5,637	.024	5,861	3,943	.585	.203	.066	.549	5,346	.515	.091	.929	2,136
21	4,974	.026	5,000	3,216	.570	.241	.076	.701	5,804	.196	.105	.111	1,268
22A	5,959	.021	5,980	3,206	.503	.196	.058	1,352	5,315	.665	.069	1,006	2,206
22B	5,959	.023	5,982	3,643	.535	.199	.042	1,076	5,095	.387	.074	.419	1,011
23A	5,660	.014	5,674	3,394	.502	.131	.061	1,070	5,158	.516	.088	.594	1,336
23B	5,660	.015	5,675	3,494	.501	.121	.060	1,115	5,291	.384	.089	.306	.862
24A	5,894	.007	5,901	3,433	.433	.061	.046	1,538	5,511	.390	.115	.516	1,323
24B	5,894	.007	5,901	3,456	.438	.055	.068	1,551	5,568	.333	.107	.006	.218
25A	5,511	.015	5,526	3,426	.507	.161	.052	.073	5,021	.505	.063	1,222	2,926
25B	5,511	.015	5,526	3,752	.575	.138	.034	.512	5,011	.515	.085	.720	1,805
Ave.	4,420	.018	4,438	2,809	.437	.148	.040	.588	4,021	.417	.093	.496	1,683

Thermal efficiencies

Run No.	A	B	C	D
15A	76	77	78	79
15B	61.2	60.5	75.5	75.5
15C	60.3	59.8	74.0	77.2
16A	61.9	61.4	74.4	77.6
16B	66.4	66.0	78.5	81.3
16C	71.7	71.2	82.5	85.5
17	77.2	76.9	89.9	91.6
18	71.7	71.5	82.0	86.0
19	75.2	75.1	85.1	86.1
20	67.6	67.3	78.3	84.3
21	64.7	64.3	77.9	87.8
22A	53.8	53.6	63.4	79.2
22B	51.1	60.9	72.5	82.1
23A	60.0	59.8	69.0	82.2
23B	61.7	61.6	70.6	84.4
24A	58.2	56.2	65.1	83.3
24B	58.6	58.6	65.4	83.9
25A	62.2	62.0	71.4	82.5
25B	68.1	67.9	78.7	85.2
Ave.	64.6	64.3	75.7	83.4

- A. Net heat of combustion of gas (B.t.u.)/net heat of combustion of coal.
- B. Net heat of combustion of gas (B.t.u.)/total heat in.
- C. Net heat of combustion of gas plus sensible heat in undecomposed steam and in dry gas above 400°F./total heat in.
- D. Net heat of combustion of gas plus sensible heat in undecomposed steam and in dry gas above 400°F. plus 70% of the heat of combustion of ungasified carbon/total heat in.

TABLE 3. - Calculated results on pilot-plant runs, using intermediate-temperature steam (runs 26A - 31B)

Conditions		Input ratios		Synthesis gas										
Run No.	Duration, hr.	Raw-coal rate, lb./hr.	Process-steam rate, lb./hr. (includes moisture from F.C.C.)	Steam-inlet temp., °F.	Steam/in. raw coal, lb.	Oxygen/lb. raw coal, lt.	Synthesis-gas analysis, percent CH ₄							
26A	1.65	399	3,605	570	5	1.24	0.16							
26B	2.00	399	3,657	1,655	1.23	.78	22.0							
27	4.00	417	500	3,520	2,024	1.20	.71							
28	4.00	428	484	3,571	1,600	1.13	.70							
29	3.00	443	464	3,310	2,015	1.05	.63							
30A	2.00	421	470	3,775	2,066	1.12	.76							
30B	2.75	421	461	3,761	2,042	1.10	.76							
31A	1.50	429	461	3,967	2,002	1.08	.79							
31B	2.50	425	468	3,582	1,997	1.10	.77							
Ave.	2.60	420	477	3,672	1,899	1.14	.74							
Generator temp., °F.		Residue (dry basis)		Ratios/l,000 S.C.F. (CO+H ₂)		Ratios/lb. raw coal								
26A	4.5 ft. above floor of generator	11.5 ft. above floor of generator	16.5 ft. above floor of generator	In horizontal outlet	lb./hr.	Carbon, percent	Cos., lb.							
26B	18	19	20	21	22	23	24							
27	2,270	1,860	1,802	1,750	102.4	61.1	39.3							
28	2,375	1,952	1,925	1,770	62.5	61.9	39.0							
29	2,341	2,071	2,004	1,790	72.9	60.7	38.3							
30A	2,430	2,130	2,100	1,885	34.4	63.5	39.0							
30B	2,393	2,100	2,056	1,820	35.2	67.2	42.0							
31A	2,490	2,100	2,116	1,795	29.9	61.7	35.8							
31B	2,536	2,175	2,192	1,993	24.5	56.4	33.2							
Ave.	2,422	2,086	2,058	1,832	46.2	61.1	37.3							
Carbon balance		Hydrogen balance												
Run No.	Total carbon in coal, lb./hr.	Fixed carbon in coal, lb./hr.	Total carbon in generator, lb./hr.	Carbon in synthesis gas, lb./hr.	Ungasified carbon, lb./hr.	Total carbon gasified, %	Based on measurement of residue	Total carbon gasified, %	Fixed carbon gasified, %	H ₂ in coal, lb./hr.	H ₂ in steam, (including H ₂ from P.O.C.), lb./hr.	Total to generator, lb./hr.	La dry synthesis gas, lb./hr.	In undecomposed steam, lb./hr.
26A	33	34	35	36	37	38	39	40	41	42	43	45	46	47
26B	296.5	211.5	15.3	228.9	67.6	71.2	68.0	78.8	71.2	21.2	54.8	76.0	30.7	45.3
27	296.5	211.5	14.1	243.1	53.4	82.0	71.6	87.0	82.1	21.2	54.3	75.5	30.6	44.9
28	309.8	221.0	19.2	258.0	51.8	83.3	76.5	89.8	80.5	22.1	55.6	77.7	32.7	45.0
29	296.6	211.0	13.6	262.5	34.1	88.5	85.1	92.6	89.8	23.5	53.8	77.3	30.9	46.4
30A	289.2	205.4	17.2	279.4	9.8	96.6	95.2	95.2	93.6	21.5	52.2	73.7	32.5	41.2
30B	289.2	205.4	16.3	209.0	2.2	99.9	99.9	95.2	93.6	21.5	51.6	73.1	34.8	30.3
31A	294.5	209.1	14.3	262.5	12.0	95.9	94.3	94.6	92.7	21.7	51.2	72.9	32.4	40.5
31B	294.5	209.1	14.5	289.6	5.9	98.3	97.7	94.7	92.6	21.7	52.0	73.7	32.5	41.2
Ave.	297.1	211.4	15.7	261.1	33.0	89.0	84.7	90.7	87.2	22.1	53.0	75.1	31.9	43.2

TABLE 3. - Calculated results of pilot-plant runs, using intermediate-temperature steam (runs 26A - 31B) - Cont.

Oxygen balance										Steam balance				Computed equilibrium temperatures			
Run No.	Net heat of combustion of coal, lb./hr.	O ₂ in P.O.C. entering generator, lb./hr.	O ₂ in steam, lb./hr.	Process oxygen, lb./hr.	Total to generator, lb./hr.	In dry synthesis gas, lb./hr.	In undecomposed steam, lb./hr.	Undecomposed steam from H ₂ balance, lb./hr.	Average undecomposed steam, lb./hr.	Total steam introduced, lb./hr.	Steam undecomposed, lb./hr.	Shift reaction, lb./hr.	C-CO reaction, lb./hr.				
26A	48	48	02 in coal, lb./hr. *														
26B	26.3	47.9	02 in P.O.C. entering generator, lb./hr.														
27	26.3	47.9	02 in steam, lb./hr.														
28	70.2	63.6	436.2	301.6	52	53	54	55	56	58	59	60	61				
29	72.6	61.3	434.7	297.6	807.9	556.1	371.5	407.7	417.9	412.0	403.0	403.0	403.0	2,481	1,207		
30A	73.3	67.5	417.0	312.0	860.6	523.2	337.4	370.8	379.6	375.2	470.0	94.6	2,144	1,204			
30B	73.3	57.6	412.4	309.7	855.2	528.0	329.2	344.7	365.9	355.3	464.0	103.7	2,150	1,246			
31A	71.8	63.2	409.8	316.9	861.7	529.8	342.9	364.5	384.6	374.6	461.0	86.4	2,195	1,229			
31B	71.8	59.6	416.0	316.1	863.5	531.3	332.2	370.8	373.7	372.3	468.0	95.7	2,210	1,238			
Ave.	57.0	56.3	424.0	298.8	835.1	495.1	341.0	389.4	383.6	386.0	477.0	91.0	2,268	1,228			
Heat Balance, millions of B.t.u. per hour																	
Run No.	Net heat of combustion of coal, lb./hr.	Sensible heat in P.O.C. gases	Total heat in	Net heat of combustion of gas	Sensible heat in gas	Sensible heat in undecomposed steam	Sensible heat of residue	Net heat of combustion of unburned C	Total heat out	Heat loss measured by heat balance, B.t.u./hr.	Calculated heat loss from shell, 10 ⁶ B.t.u./hr.	Calculated heat stored in bricks, 10 ⁶ B.t.u./hr.	Steam undecomposed, lb./hr.	Shift reaction, lb./hr.	C-CO reaction, lb./hr.		
26A	62	63	64	65	66	67	68	69	70	71	72	73	74	75			
26B	5.074	0.400	0.033	5.507	3.207	0.525	0.372	0.062	0.907	5.073	0.434	0.116	0.958	2,692			
27	5.303	.392	.030	5.496	3.244	.566	.384	.033	.561	4.768	.728	.112	.663	1,942			
28	4.904	.373	.030	5.307	3.478	.604	.397	.056	.642	5.337	.524	.081	.518	1,435			
29	5.044	.471	.038	5.553	3.298	.604	.496	.023	.343	4.764	.789	.119	.313	1,014			
30A	4.917	.495	.038	5.450	3.699	.685	.408	.034	.269	5.095	.355	.119	.645	1,815			
30B	4.917	.474	.035	5.426	3.962	.733	.403	.031	.203	5.332	.094	.118	.119	563			
31A	5.011	.461	.033	5.503	3.738	.693	.412	.037	.249	5.129	.376	.122	.392	1,209			
31B	5.011	.468	.037	5.516	3.610	.731	.423	.035	.249	5.248	.268	.125	.329	1,056			
Ave.	5.020	.449	.036	5.513	3.560	.648	.424	.037	.416	5.075	.438	.125	.465	1,396			

Thermal efficiencies

Run No.	A	B	C	D
26A	75	77	78	79
26B	63.2	58.2	71.8	83.1
27	63.9	59.0	72.2	92.3
28	68.0	61.5	76.4	84.1
29	65.4	59.4	75.3	87.2
30A	75.2	67.9	86.0	89.4
30B	83.5	73.0	92.7	95.3
31A	74.6	67.9	85.3	89.0
31B	76.0	69.1	88.1	91.2
Ave.	70.9	64.6	81.2	86.4

- A. Net heat of combustion of gas (B.t.u.)/net heat of combustion of coal.
- B. Net heat of combustion of gas (B.t.u.)/total heat in.
- C. Net heat of combustion of gas plus sensible heat in undecomposed steam and in dry gas above 400°F./total heat in.
- D. Net heat of combustion of gas plus sensible heat in undecomposed steam and in dry gas above 400°F. plus 70% of the heat of combustion of ungasified carbon/total heat in.

- Cont.

ated equilib-
temperatures

C-30 reaction,
gr.

61
1,207
1,204
1,239
1,224
1,221

1,246
1,255
1,229
1,238

1,228

stored in bricks,
10⁵ B.t.u./ar.
Calculated heat loss:
B.t.u./lb. coal

75
2,692
1,942
1,136
1,014
828

1,815
563
1,209
1,088

1,396

total

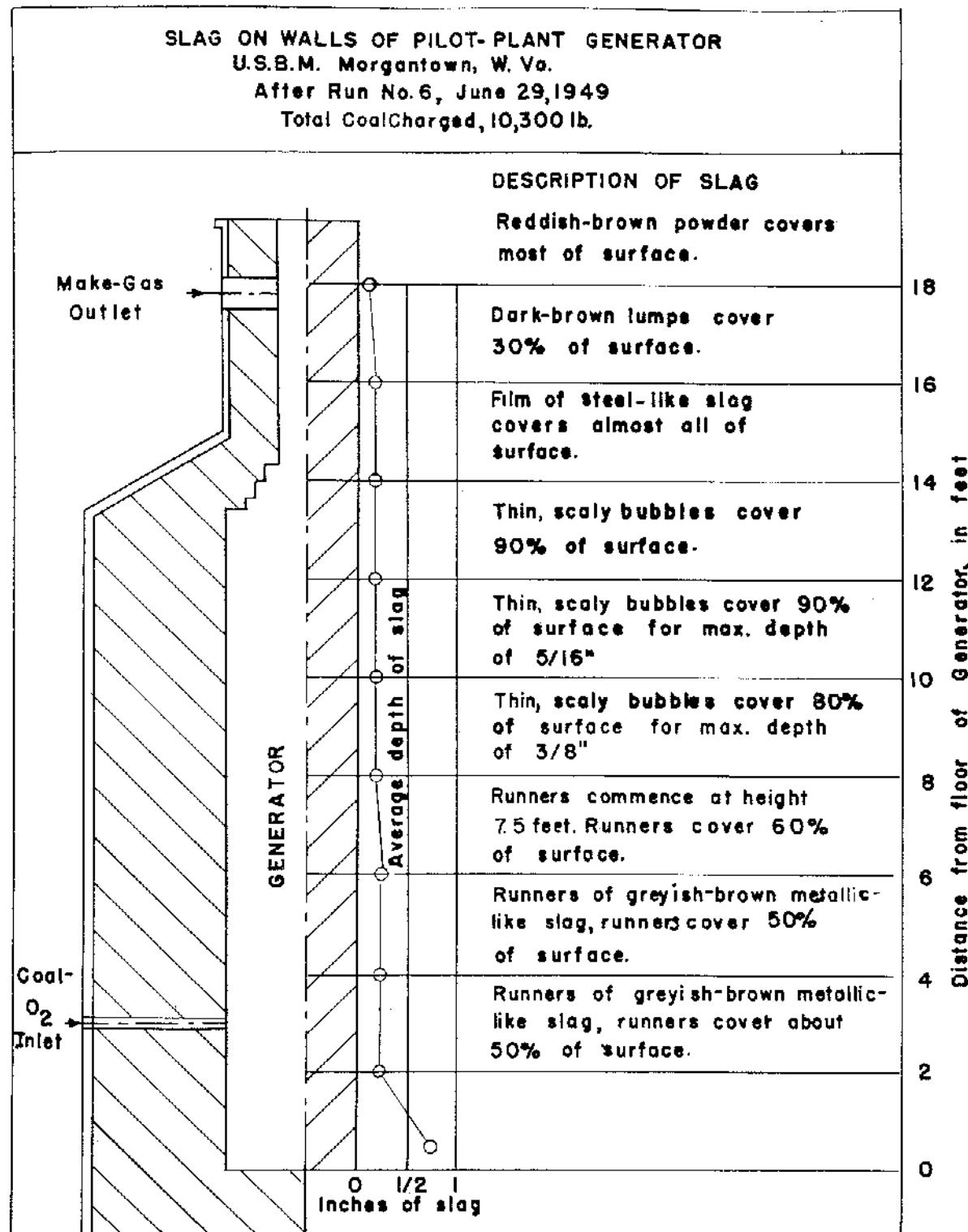


Figure 25. - Typical slag distribution in gas generator.