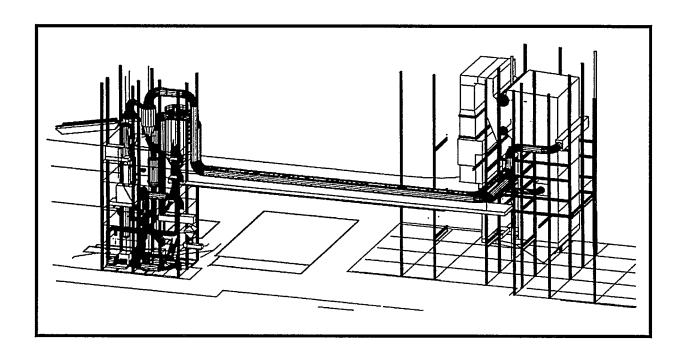
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### **VERMONT GASIFIER PROJECT**

BURLINGTON, VERMONT RECEIVED CONTRACT NO. 2064

NOV 2 1 1995

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### FINAL REPORT - PHASE I July 1995

ZURN /////// NEPCO

MASTER



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### VIA UPS

August 9, 1995

Mr. Milton Farris Future Energy Resources, Inc. 3350 Cumberland Circle, N.W. Suite 1500 Atlanta, GA 30339-3363

Subject:

Final Report - Phase 1

Vermont Gasification Project

### Dear Glenn:

Attached are ten copies of the subject report. The results/minutes of the Safety Meeting were transmitted under separate cover. With the exception of closing out loose ends, this report concludes the Phase 1 effort. Invoice 64008 has been issued, invoicing for all of the Contract Value but \$54,000. The \$54,000 will be invoiced for next month.

Should you have any questions, please advise.

Very truly yours,

Janki & Kany

Joseph J. Sapp Project Manager

JJS/ckw/64-PR

### Attachment

cc:

D. Butynski

J. Rohrer

W. Bell

G. Manry

C. Johnson

B. Slack

### DISCLAIMER

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### **VERMONT GASIFIER PROJECT**

### FINAL REPORT - PHASE 1

### JULY 1995

1.0	ENGINEERING STATUS
2.0	TECHNICAL AREAS OF CONCERN
3.0	ATTACHMENTS

### VERMONT GASIFIER PROJECT BURLINGTON, VERMONT

### FINAL REPORT - PHASE 1

### JULY 1995

### 1.0 ENGINEERING STATUS

### 1.1 General

Phase 1 engineering accomplishments are shown below. Also shown below are engineering activities scheduled for Phase 2. During the July 17th Design Review Meeting the project was re-directed to design and install a scrubber. The scrubber design will be incorporated into Phase 2.

### 1.2 Civil/Structural

The following summarizes the Phase 1 accomplishments:

- 1.2.1 The site survey and geotechnical work has been completed. The geotechnical report prepared by Knight Consulting indicates that steel "H" piles will be required under the gasifier building only. All other foundations will consist of spread footings.
- 1.2.2 The pipe rack foundations between the gasifier building and the McNeil boiler have been completed, but must be verified after the final pipe refractory is selected.
- 1.2.3 The gasifier building foundations, including steel piles, have been designed and checked, but must be verified once building steel is completed and building loads are finalized. The current foundation design did not include the enclosure flare stack on top of the building.
- 1.2.4 The fuel handling foundations have been completed. These foundations will have to be verified once final vendor is selected. The foundation for the infeed fuel hopper has been designed, but put on hold on the drawing awaiting decision on final hopper size.
- 1.2.5 The gasifier building structural steel is in the process of re-design based on the enclosed flare arrangement and based on the latest General Arrangement drawing. A model has been developed to calculate steel member sizes using STAAD III program. Several more iterations with the model will be required before final design is completed. The output of the model will show final member sizes and building loads for foundation design.

- 1.2.6 The utility bridge has been completed, but must be verified after final refractory selection in the product gas and flue gas lines. Based on the expected upgrades in the refractory, there will be approximately one third (1/3) increase in load on the pipe bridge. This will require only a minor modification to the bridge in terms of upgrading a chord size and a vertical member size of the truss.
- 1.2.7 The site plan has been completed.
- 1.2.8 The following has been scheduled for Phase 2:
  - Pipe rack, building and fuel handling foundations to be verified based upon final equipment selection and configuration.
  - Final building steel member sizes to be finalized based on final equipment selection and configuration.
  - Pipe rack steel member size to be verified after final refractory selection.
  - Review vendor and shop drawings.
  - Provide field support as needed for construction.
  - Re-design as necessary for scrubber modification.

### 1.3 <u>Mechanical/Process Design</u>

The following summarizes the Phase 1 accomplishments:

- 1.3.1 The process flow diagrams, including Heat and Mass Balance, have been completed.
- 1.3.2 The P&IDs and line list have been generated. Since these documents continuously evolve through the life of the project, updates will be required as final equipment selection is made.
- 1.3.3 The following equipment has been specified with bid evaluations and requisitions completed:
  - Cyclones
  - Start-up Burners
  - Product Gas Burner
  - Blowers
  - Flare

### 1.3.4 The following is the status of the balance of equipment:

- Sand and MgO Transport System Equipment has been specified with a sand storage tank, MgO tank, and a common dense phase transporter. Due to the fact that it is not clear when and how much MgO will be required, it may make sense to consider using a bag unloading system for MgO with 2,000 lb. bags instead of a 330 cu. ft. tank. This may save capital and operating costs. Vendors have been asked to quote on a bag unloading system.
- Ash Handling System The system was initially bid and evaluated. Continuous developments were made throughout the project life and incorporated into a revised specification. This revised specification was subsequently re-bid and is currently being evaluated. During the July 17th Design Review Meeting, the bottom ash system was deleted.
- <u>Fuel Handling System</u> The system was initially bid and evaluated. Continuous developments were made throughout the project life and incorporated into a revised specification. This revised specification was subsequently re-bid and is currently being evaluated.
- Vessel Fabrication This includes the specification and drawing package for the gasifier vessels. This has been bid and several potential fabricators have been selected. A final release of drawings will be required for an updated bid before final release to the manufacturer. The drawings have been finalized.
- <u>Refractory Specification</u> Refractory to be field installed in the vessels and shop installed in the piping has been specified and initially evaluated. The refractory costs were significantly greater than initially estimated and all the bidders have been asked to rebid. Bids are due on July 13, 1995.
- <u>Rupture Disks</u> An adequate method of design and vent rupture disks has not been established. Pending the safety review, this task has been put on hold.
- <u>HT Dampers</u> The dampers have been specified and bids have been evaluated. A requisition needs to be prepared.
- <u>Expansion Joints</u> The expansion joints have been specified and bids evaluated. Requisition is awaiting final expansion plan configuration to pick up potential modifications in order to minimize change orders after release.

- Prepared preliminary drawings of modifications to the McNeil boiler for the product gas burner and the combustor flue gas penetration. Zurn Energy is to summarize with a final report regarding modifications and impact on boiler performance. Final report has not been completed.
- IGT has conducted a test with a 12 inch L-valve to determine whether an L-valve can adequately transport a heterogeneous mixture of sand and char to the combustor. The test was completed successfully, but we are still awaiting the results and final report.
- 1.3.5 A Project Safety Review was completed during the week of July 17, 1995.
- 1.3.6 Provide permit support.
- 1.3.7 The following activities are scheduled for Phase 2:
  - Prepare requisitions for the following equipment:
    - Sand & MgO Transport System
    - Ash Handling System
    - Fuel Handling System
    - Vessel Fabrication
    - Refractory System
    - HT Dampers
    - Expansion Joints
  - Specify, evaluate bids, and requisition the following:
    - Fire Protection
    - Heating, Ventilation, and Air Conditioning
    - Sump Pump
    - Insulation
  - Update process flow diagrams, P&IDs, line list and equipment list to final equipment configuration.
  - Support safety review(s) and development of operating procedures.
  - Address any design changes or modifications as a result of safety review.
  - Review vendor drawings.
  - Provide field support as needed for construction and start-up.
  - Re-design system to include scrubber.

### 1.4 <u>Electrical Design</u>

The following summarizes the Phase 1 accomplishments:

- 1.4.1 The following equipment has been specified with bid evaluations and requisitions completed:
  - Low Voltage MCCs
  - Medium Voltage Switchgear
  - Auxiliary Transformers
- 1.4.2 The closed circuit television system has been specified and issued for bid. Bid evaluations have not been completed.
- 1.4.3 The cable and raceway list was generated (power cable only).
- 1.4.4 The one-line diagram was generated.
- 1.4.5 The electrical underground layout was completed.
- 1.4.6 The following design activities have been scheduled for Phase 2:
  - Lighting specification
  - Ground resistivity testing specification
  - Heat tracing specification
  - Lighting and fire protection raceway design
  - Instrumentation raceway design
  - Detail wiring diagrams
  - Review vendor drawings
  - Provide field support as needed for construction and start-up
  - Design interface with scrubber system

### 1.5 <u>Instrumentation and Controls</u>

The following summarizes the Phase 1 accomplishments:

- 1.5.1 The following equipment has been specified with bid evaluations and requisitions completed:
  - Combustion Gas Analyzers
  - Steam Conditioning Valves
  - Pilot Tube Flow Elements
  - Gas Chromatograph and Sample System

- 1.5.2 The following equipment has been specified and bids have been evaluated, but final requisitions have not been written. For these items we are awaiting final design configuration in order to minimize change orders after equipment release:
  - Control System
  - Control Valves
  - Air Flow Dampers
  - Intrinsic Safety Barriers
  - Orifice Plates
  - Level Transmitters
  - Pressure Transmitters
  - Pressure Switches
  - Pressure Indicators
  - Thermocouples
  - Thermometers
- 1.5.3 The logic drawings and the control system description have been completed. The instrument location drawings have been generated. Final location drawings will be completed after final piping design in Phase 2.
- 1.5.4 Interfaced control system with existing McNeil Plant.
- 1.5.5 The following activities are scheduled for Phase 2:
  - Final I/O count and DCS requisition
  - Final valve count and control valve requisition
  - Final instrument count and miscellaneous instrument requisitions
  - Instrument installation details
  - Instrument location diagram upgrade
  - Logic diagram upgrade
  - Support safety review and development of operating procedures
  - Review vendor drawings
  - Provide field support as needed for construction and start-up
  - Design interface with scrubber system

### 1.6 <u>Piping/Mechanical Design</u>

The following summarizes the Phase 1 accomplishments:

- 1.6.1 General arrangement drawings have been completed.
- 1.6.2 Vessel drawings have been completed.
- 1.6.3 Refractory lined piping has been designed. The drawings still need a final check before final release.
- 1.6.4 Stiffeners and plate thicknesses for flat duct between vessels and cyclones have been designed, but have not been shown on the final drawings.

- 1.6.5 The utility bridge piping has been completed. Pipe design inside McNeil's building has been completed.
- 1.6.6 Initial routing of large bore piping (steam & water) has been developed, but drawings have not been generated.
- 1.6.7 Refractory lined piping has been stress analyzed. Pipe supports have been designed. Expansion plan has been designed, but final drawing has not been generated.
- 1.6.8 Preliminary stress analysis has been performed on large bore steam piping.
- 1.6.9 Preliminary pipe specification has been generated.
- 1.6.10 The following activities are scheduled for Phase 2:
  - Finalize, check and issue for construction the refractory lined piping drawings.
  - Finalize drawings for duct between vessels and the cyclones.
  - Complete steam and water large bore pipe design, stress analysis, and pipe support design.
  - Design small bore piping.
  - Update general arrangement drawings for final equipment configuration.
  - Check vessel manufacturer shop drawings and calculations.
  - Review vendor drawings.
  - Final pipe specification will be generated.
  - Provide field support as needed for construction and start-up.
  - Design interface for scrubber system.

### 2.0 TECHNICAL AREAS OF CONCERN

### 2.1 Agglomeration in Combustor and Dash Pots

Recent tests at the Battelle process research unit using wood feedstock from Burlington Electric's fuel supply showed ash agglomeration at temperatures above 1840°F which is the operating range of the Vermont unit. Agglomeration stops fluidization and solids circulation. Particles to basketball size were observed and it was necessary to shut down to clean out the combustor. During this short series of tests agglomeration was found to be controlled by adding magnesium oxide at a rate of approximately the wood dry ash rate. The ability to add MgO is being included in the gasifier design. The risk is that the fuel tested is not representative of all fuels. Agglomeration may additionally occur at temperatures lower than observed in the test, agglomeration may not be easily controlled, and the differences in operating dynamics between the process research unit (bubbling bed combustor) and the Vermont unit (entrained bed combustor) may result in severe agglomeration problems.

### 2.2 Nuclear Detectors

To assure that sand seal leg length remains constant between the gasifier and combustor and that the proper quantity of make-up sand is added, it is necessary to measure the level of sand and char in the gasifier and combustor dash pots. These closed vessels operate pressurized and at high temperatures and in the case of the gasifier dash pot, contain flammable gas. It is planned to take the solids level measurements with nuclear detectors. Technically this method is optimum for the application, but requires that Burlington Electric Company obtain nuclear source licenses for selected technicians and provide for training to maintain the licenses. To date Burlington Electric has stated they will consider taking on the licensing, but have not committed themselves.

### 2.3 Interruptible versus Firm Gas Supply

Presently the start-up of the gasifier plant is based upon using interruptible gas supply. This means that there will be periods of gas curtailment when the gasifier can not be brought on-line. This will occur primarily in the winter. From a safety perspective, the pilot for the flare must come from the firm gas supply which is not subject to curtailment.

### 2.4 Char Characteristics and Cyclone Efficiencies

### 2.4.1 Char Characteristics:

Reasonable char sizing distribution was predicted based on expected raw fuel sizing criteria and published char formation algorithms. These sizing predictions were then modified to reflect the anticipated size degradation due to the inherent abrasive environment associated with the gasifier process. An additional weighted factor was applied to the resulting size distribution to emphasize the production of smaller size char particles.

This was done to provide a slightly increased hardship on the cyclones, as smaller particles are harder to remove from a gas stream than larger size particles. In the end, the sizing distribution reflected in the cyclone specification was selected as being representative of what is anticipated at Burlington. However, it must be recognized that there is no existing empirical data upon which this is based and it is largely considered near impossible to attain and measure an actual piece of char. The design risk consideration here is that the char particles could be significantly different than identified in our documentation. This would affect the following items:

- Cyclone performance
- Possible sticking, jamming, or otherwise obstructing valve or other mechanical clearances.
- Possible adverse solid circulation affects. Specific consideration should be given to clogging in the Dip Legs between the cyclones and L-valves.
- Solids circulation ratio may change considerably. Char size and solids circulation ratio is related by virtue of the fact the sand may have to contact more or less char surface area in order to completely transfer an adequate quantity of heat to combust the char.

### 2.4.2 Cyclone Performance:

Cyclone performance is directly related to the char removal as discussed above. Presently, the cyclones being considered have a very high removal efficiency for all particulate loading. I some aspects this is potentially undesirable. An unanticipated quantity of ash is likely to be removed from the Gasifier and Combustor Cyclones. The conceptual design is based on all ash being removed from the system via the Secondary Combustor Cyclone. If significant ash is removed in the Gasifier and Combustor Primary Cyclones, this ash could promote agglomeration in the Dip Legs and L-valves. Sand is the third primary constituent to be removed from the gas streams via the cyclones. Once again, the efficiency is higher than originally expected. This will help minimize the sand loading ultimately deposited in the McNeil Station boiler. However, it should be recognized that a substantial amount will still ultimately find its way to the boiler regardless of increased cyclone efficiency. It is important to note that the sand and ash sizing characteristics were derived in largely the same manner as the char characteristics. Sizes were predicted based on input from other operating experience from conventional wood fired boilers. This is not to suggest that these sizes can't or won't change. The effect of size distribution changes from the anticipated will largely effect those items shown above under the Char <u>Characteristics</u> discussion above. In addition to these items listed above,

the quantity of ash loading exiting the Secondary Combustor Cyclone must be given due consideration if it is outside the operational removal parameters of the ash system presently scoped for that location. All in all, operational problems could occur with low cyclone efficiencies (no char collection, high solids carryover to boiler, high sand make-up rates) and excessively high efficiencies (accumulation of ash in gasifier and combustor).

### 2.5 Particulate Emissions/NOx Emissions Due to Fuel Bound Nitrogen

Safety vent flare - during periods when the safety vent flare is in use it will disperse particles of sand (silica), ash, and char to the atmosphere. Presently it is planned to use the safety vent flare for 80 hours over a 3 month period during plant initial start-up. Subsequently, the vent flare will only be used following gasifier trip for a few minutes following each incident. Note that during the period of facility initial commissioning, the allowed flare emissions are severely curtailed by the air quality permit. Thus, there is limited opportunity for fine tune controls associated with the flare and burner and it is possible that some variance may have to be required from this permit.

During gasifier start-up and normal operations the product gas burner will emit particles of sand, ash, and char into the McNeil boiler furnace. It is anticipated that this particulate will be substantially collected in the pollution control equipment on the back end of the McNeil boiler. Poor cyclone efficiencies, offspec. fuel, sand, char, and ash, as well as off-design performance of the gasifier may lead to higher than expected particulate loadings to the McNeil boiler causing emission non-compliance and/or boiler fouling problems.

NOx emissions due to fuel bound nitrogen - during gasification, a portion of fuel bound nitrogen is expected to be converted to NH3 (ammonia). Battelle's work with the PRU indicates this is approximately 10%. When the ammonia reaches the product gas burner some of it will be converted to NOx. The quantity of ammonia converted to NOx has been predicted by COEN (burner manufacturer) to be approximately 90%. Based on the above assumptions and assuming that emissions from the char combustor will be comparable to typical wood fired CFB NOx emissions (0.18 lb/MMBtu), it is anticipated that total NOx emissions (product gas burner and char combustor) will be no greater than current McNeil allowed emissions. However, if the amount of fuel bound nitrogen converted to ammonia in the gasifier exceeds 10% or the conversion at the burner exceeds 90% or char combustor NOx emissions are greater than expected, the B.E.D. facility may be out of compliance for NOx emissions. The impact of fuel bound nitrogen on NOx emissions has not been addressed in the air permit modifications as the information was not available at the time. Although the net emissions impact should not be affected, the permit information should be straightened out.

### 2.6 Solids Circulation System

Solids circulation concerns include possible agglomeration, the impact of char characteristics on cyclone efficiency both discussed above, and:

- possible difficulties with circulation of sand, char, and ash
- possible loss of sand column seals

The solids in the circulation path from the gasifier cyclone to the dash pot and further through the L-valve to the combustor include sand, char, and ash. Conditions are similar in the circulation path from the combustor to the combustor cyclone through its dash pot and through its L-valve to the gasifier except there is no char. Due to density and size differences, it is possible that during flow the mixture may be stratified. The effect could be most pronounced at the L-valve where partial fluidization occurs.

The sand seal columns between the dash pots and the L-valves serve to isolate the reducing atmosphere in the gasifier from the oxidizing atmosphere in the combustor. The consequence of loss of either sand seal would mean mixing of product gas and combustion air which is expected to result in a rapid burn (deflagration), possibly an explosion (unlikely, but must be investigated), and rapid pressure increase in the system, requiring vessel external venting. Sand seal heights are to be normally maintained by the gasifier control system based on level measurements in the dash pots. Excepting difficulties with the control system, the most likely way of losing sand seals is by blowing them through a sand leg. Again, expert opinions vary, but a pressure differential between the vessels as low as 4 to 5 psi could possibly cause the problem (reference T. Knowlton fax 4/17/95). It should be noted that balancing pressure between the vessels by throttling system valves is an option, but it is limited as the addition of pressure drop results in increased blower pressure requirements and increased horsepower. Results from the L-valve test conducted at IGT will allow a more exact computation and review of the solids system design.

### 2.7 Valve Design and Sealing Problems

Maximum temperature and pressure for valves associated with the combustor and product gas is 1800°F and 15 psig. For valves associated with the combustor and flue gas maximums are 2000°F and 15 psig. These valves are the respective vessel design temperatures and pressures. At these temperatures and pressures allowable stresses for even the most costly high temperature metals are very low and valve design is based on material creep limitations. The most practical approach to valve design is to define the frequency and duration of service at the higher temperature and pressure conditions (it is worth noting that other gasifier designs surveyed do not subject valves to temperature and pressure combinations as difficult as these).

Valve sealing is most challenging for valves associated with the gasifier vessel and product gas lines as product gas leakage will ignite in contact with air so that even a small leakage results in destruction of the seals. Valves in this category include those at the product gas safety vent flare, the product gas shut-off to the product gas burner, and start-up air valves at the gasifier vessel.

To prevent seal leakage, a solution is to use double valves with a higher pressure sealing medium between so that leakage is always from the valve into the product gas. Nitrogen is ideal for a seal gas as it is inert and commercially available. Unfortunately, even very tight clearances result in high consumption of nitrogen. For example, to seal two valves in the 24" inside diameter product gas line at the burner against 2 psig with a disk to seat clearance of .005" requires approximately 220 lb. of nitrogen per hour. If conditions were the same, but valve clearance was .015", the nitrogen requirement would be 650 lb/hr (.005" is approximately the diameter of a human hair). As the product gas line carries sand and a small amount of char in addition to product gas, it will be difficult to assure that these clearances will be maintained, especially in a high temperature, material creep environment. For that reason and as nitrogen costs \$.05/lb, other gases are being investigated. A possibility is the use of steam which has the problem that the source is McNeil Station and following trip it will become unavailable. Another possible problem is that condensed steam may wet refractories with damage occurring when the refractory is heated during start-up.

### 2.8 <u>Deflagration Venting</u>

Should air come in contact with the product gas in the gasifier vessel or product gas lines, the possibility of very rapid burning or deflagration exists. See paragraphs on sand circulation concerns and valve sealing above and the section purging of the gasifier to prevent flame front entry below. In that case, the gasifier system pressures would rise throughout and the product gas safety vent and vessel rupture disks or other overpressure protection provisions could vent the contents of the gasifier vessels into the atmosphere. Some specific fire/safety considerations associated with such venting are given in Battelle's 4/25/95 letter. It appears there are personnel hazards as well as fire hazards to the McNeil Station and surrounding area in the event of a rupture disk relief. Reference Battelle's letter of 4/25/95.

The greatest deflagration of explosion hazard will be from a combustible mixture of air and natural gas that is allowed to build up inside the vessels sufficiently to cause uncontrolled combustion after being exposed to an ignition source. Se Walt Howard's report dated June 21, 1995. Deflagration or explosion venting cannot protect the vessels for pressure rise from this event. Currently there are no pressure relief disks or valves included in this vessel design. Standard industrial practice on boilers and other vessels is to protect overpressure from uncontrolled combustion with a flame safety and burner management system in accordance with NFPA. It must be determined whether this is an acceptable practice for the Burlington gasifier or whether some "other" means (pressure containment, indirect air heating) will be required. Costs have not been included for "other" means of protection.

### 2.9 Combustion and Gasifier Blower Surge Control

Due to characteristics inherent with centrifugal compressors, the gasifier and combustor blowers are capable of a turndown of between 2:1 and 3:1. The factor most limiting to turndown is the onset of the phenomenon known as surge. When the surge threshold is exceeded, flow reversals and pressure transients can cause machine damage. The use of variable inlet vanes to control throughput has the

effect of increasing this turndown, although in the case of the gasifier blower, it is still not sufficient for process requirements. The only way to prevent surge is to ensure suction flow never falls below the valve where surge occurs for a given inlet vane position. This will be accomplished by comparing blower differential pressure to inlet vane position. If differential pressure exceeds the maximum value allowed for the existing vane position, a blow-off valve will open to increase suction flow and decrease differential pressure.

### 2.10 Purging of Gasifier Piping

This is necessary to prevent flame front entry into the system. It is anticipated that purging will be required during gasifier start-up and shutdown to assure that burning does not occur within the gasifier vessel, cyclones, or the product gas piping. In addition to the usual purging to clear possible explosive gases prior to start-up, burner light-off purging will be necessary during:

- gasifier start when the atmosphere within the gasifier vessel changes from oxidizing to reducing.
- gasifier start-up or shutdown when the volume of gas generated is such that a flame front can move from the product gas burner or safety vent flare back down through the piping toward the gasifier vessel.

The gasifier start-up sequence includes burning wood in the gasifier vessel to heat the refractory. When the refractory is sufficiently heated, the excess air provided for combustion will be reduced. As the airflow is reduced, the oxygen for combustion goes from excess to stoichiometric to substoichiometric and instead of being combusted, the wood fuel feed transitions will be gasified. The transition means that air and product gas will exist as a combustible at relatively high temperatures. An explosive mixture may be possible as air is decreased and more product gas is produced. During this period steam will be added to the gasifier vessel both as fluidizing steam through the distribution plate and as dilution steam at the top of the vessel to prevent combustion by dilution of the mixture. The exact quantities of steam must be determined by gas composition calculations (expert assistance will be required with this determination) as details of the start-up procedure are developed.

A somewhat similar situation develops during orderly shutdown or following gasifier trip. Normally gas velocities through the product gas piping to the product gas flare or the product gas burner are sufficient to preclude a flame front from burning from the outside atmosphere (or the oxygen rich boiler furnace in the case of the product gas burner). However, as less gas is generated during shutdown, the possibility exists of a flame front traveling down the piping towards the gasifier entraining its own air supply and potentially causing high pressures, overheating the refractory and possibly explosion/deflagration. To preclude such an occurrence, steam will be added to the gasifier vessel during shutdown and immediately following trip to maintain gas velocities, purge the piping and dilute the product gas. Provision is also being made to add steam to the product gas line near the product gas burner to purge that line back towards

the product gas flare. Details of the necessary controls are to be developed. One area of concern is that following trip of the McNeil Station, the steam supply from the station may not be adequate and the possibility exists that Nitrogen gas may have to be utilized in that situation in lieu of steam.

### 2.11 Char Burnout

Based on tests that Battelle has done with a small (six inch) CFB, complete burnout of char in the combustor will occur at lengths of approximately 10 feet. Since the Burlington char combustor is much different than the test CFB, direct use of the data in terms of complete char burnout cannot be made. The Burlington combustor has 50 ft. of length. This gives a residence time in excess of 1 second in the combustor. Depending on the char size, this may not be adequate for complete combustion. The risk of incomplete burnout is that char overloading could occur, causing excessive or inconsistent combustor temperatures, agglomeration, and carryover through the cyclones. Test ports have been included in the vessel to help determine where char burnout occurs.

### 2.12 Repair of Refractory

The refractory throughout this project will require continuous monitoring and maintenance. The highly abrasive environment coupled with thermal cycling (as the plant is brought off and on-line) will lead to cracks, erosion, and refractory failures with time. Certain areas such as the cyclone target area will be particularly subject to erosion.

### 2.13 On-Line Capabilities

The project direction has been given to delete the on-line capabilities to remove tramp bed material from the vessels. With poor quality fuel this could lead to increased pressure drop across the distributor and lead to increased shutdowns for cleaning.

### 2.14 Retractable Burner

For the retractable burner located inside the vessel the actual flame could cause local hot spots and agglomeration inside the combustor.

### 2.15 Air and Product Gas Mixture

A combustible mixture of air and product gas could enter the fuel system due to equipment or controls malfunction and create a deflagration or explosion situation.

### VERMONT GASIFIER PROJECT FINAL REPORT - PHASE 1 JULY 1994

### **ATTACHMENTS**

A - DRAWING AND SPECIFICATION REGISTER

### ATTACHMENT A DRAWING AND SPECIFICATION REGISTER

DWG STATUS LEGEND : 1 = CONCÈPTUAL ENGINEERING AT 30% COMPLETE

2 = DESIGN AND DRAFTING AT 70% COMPLETE

3 = 95% COMPLETE (FOR PROGRESS PURPOSES) 4 = PHASE 1 ENGINEERING COMPLETE

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COMMENTS	PHASE 1 COMPLETE PHASE 1 COMPLETE NEEDS REQUISITION PHASE 1 COMPLETE PHASE 1 COMPLETE NEEDS REQUISITION PHASE 1 COMPLETE	PHASE 2 PHASE 2 PHASE 2	PHASE 1 COMPLETE NEEDS DRAWINGS CHECKED NEEDS CHECKING PHASE 1 COMPLETE SUBJECT TO SAFETY REVIEW	PHASE 1 COMPLETE PHASE 1 COMPLETE PHASE 1 COMPLETE NEEDS REQUISITION PHASE 1 COMPLETE	PHASE 2 PHASE 1 COMPLETE
IFC/ IFB DATE	01/13/95 03/10/95 01/13/95 03/01/95	03/15/95 03/15/95 03/15/96	07/14/95	03/17/95	02/28/95 01/16/95 03/10/95
IPC/ IFC/ IFC/ UB ITB IFB DATE DATE	01/05/95 12/16/94 12/22/94 12/19/94 11/25/94 04/07/95	03/01/95 02/17/95 02/06/95	04/03/95 04/16/95 03/30/95 04/14/95	02/15/95 02/15/95 01/09/95 11/17/95 11/17/95	12/24/94 12/16/94 01/16/94 11/17/94 02/13/95
IFC! IFB DATE	01/19/95 03/08/95 01/12/95 02/27/95 11/23/94 04/12/95		01/18/95 04/26/95 04/26/95	02/09/95 02/27/95 03/28/95 11/21/94 11/21/94 04/26/95	01/30/94 01/06/95 11/21/94 · 03/06/95
DWG CDST STATUS CODE	4 4S7410 4 4S7340 4 4U7300 4 4S7300 4 4S7370 4 4S7350	457370.2 457370.2 457370.2	4 4K/380 4 4K/380 4 4K/360 4 4S/400 4 4K/380	4 4K7380 4 4K7380 4 4S7340 4 4U7320 4 4S7420	45/420-2 4 4K7340 4 4S7320 4 4L7410 4 4L7410 4 4L7410
LAT EST REV DATE TITLE S	01/19/95 EQUIPMENT LIST 03/08/95 CYCLONE SPECIFICATION 06/12/95 ASH HANDLING SYSTEM 06/12/95 START-UP BURNER 11/23/94 PRODUCT GAS BURNER 04/11/95 SAND AND MAGNESIUM OXIDE TRANSPORT SYSTE 02/09/95 BLOWERS	FIRE PROTECTION ALARM & SPRINKLER SYSTEMS HEATING, VENTILATING & AIR CONDITIONING SUMP FUME	PREL 01/16/95 PIPE SPECIFICATION  A 04/24/95 REFRACTORY LINED PIPE AND DUCT FOR TEMP. SE  STRESS ANALYSIS  A 07/11/95 LINE LIST  RUPTURE DISKS	04/26/95 REFRACTORY LINED EXPANSION JOINTS 07/11/95 DAMPERS FOR HIGH TEMPERATURE SERVICE 03/28/95 VESSEL FABRICATION SPEC. 06/12/95 FUEL HANDLING SYSTEM SPEC. 11/21/94 GENERAL MACHINERY SPEC. 04/20/95 REFRACTORY SPEC.	INSULATION SPEC.  01/25/95 PRODUCT GAS SAFETY VENT STACK & FLARE 01/06/95 NITROGEN GAS GENERATING SYSTEM 11/21/94 ELECTRIC MOTOR SPEC. 06/19/95 LOW VOLTAGE MOTOR CONTROL CENTERS 06/20/95 MEDIUM VOLTAGE CONTROLLER GEAR
LA	~ < m m < < <		PRE) A A	<b>m m &lt; m &lt; &lt;</b>	A A A B
DWG/ SPEC NO.	100.0 101.2.1 102.2 103.3 103.31 107.3	100.6 110.1 111.5	115.1 115.2.1 115.7 115.8 115.9	115.12.1 115.12.2 115.30 117.0 117.11	118.3 17.5 127.5 202.3 203.1

DWG STATUS LEGEND: 1 = CONCÈPTUAL ENGINEERING AT 30% COMPLETE
2 = DESIGN AND DRAFTING AT 70% COMPLETE
3 = 95% COMPLETE (FOR PROGRESS PURPOSES)
4 = PHASE 1 ENGINEERING COMPLETE

COMMENTS	PHASE 1 COMPLETE			PHASE 1 COMPLETE		PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 2	PHASE 1 COMPLETE	PHASE 1 COMPLETE	-	PHASE 1 COMPLETE	_	PHASE 1 COMPLETE	PHASE 1 COMPLETE	_	_	-	PHASE 1 COMPLETE	PHASE 1 COMPLETE	-	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE
ACTUAL PLANNED PHOJCT DEC.  IEC. IEC. IEC.  UB IEB IFB DATE DATE DATE	04/17/95		03/03/95												03/31/95	03/15/95			03/15/95		03/31/95					03/15/95	03/15/95
E PLANNEI IFC! IFB DATE	. 03/06/95 03/06/95			03/16/95	_	04/19/95	05/26/95	26/91/60	03/23/95	26/90/60	01/23/95		01/23/95	01/23/95	02/10/95		03/31/95		02/10/95	02/27/95	02/27/95		02/27/95	02/27/95	02/27/95	02/27/95	02/27/95
ACTUA IFC/ IFB DATE	12/22/94	03/06/95	03/13/95	12/22/94	12/22/94	03/21/95	96/02/92		12/22/94	12/22/94	01/17/95	04/06/95	01/31/95	01/31/95	04/02/95	03/13/95	04/05/95	04/12/95	03/13/95	02/21/95	03/21/95	06/15/95	02/17/95	02/11/95	02/21/95	03/13/95	03/06/95
DWG COST STATUS CODE	4 4L7410 4 4L7410.2	4 4L7410	4 4L7410	4 4L7410	4 4L/410 4 4L7410	4 4L7330	4 4L7410	TEM 4L7410.2	4 4L7410	4 4L7410	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400	4 4M7400
EST DATE THIE	12/22/94 ELECTRICAL GROUNDING INSTALLATION GROUND RESISTIVITY TESTING	06/20/95 MEDIUM VOLTAGE SWITCHGEAR		12/22/94 FURNISHING & INSTALLATION OF ELECTRICAL RA	12/22/94 FURNISHING OF ELECTRICAL WIRE & CABLE 12/22/94 WIRING INSTALLATION METHODS	04/25/95 CABLE AND RACEWAY LIST & LOAD LIST	05/24/95 CLOSED CIRCUIT TELEVISION SYSTEM	INSTALLATION OF ELECTRICAL BEAT TRACING SY	12/22/94 ELECTRICAL FIELD TESTING	12/22/94 ABOVE GROUND ELECTRICAL INSTALLATION	04/04/95 GAS CHROMATOGRAPH	04/04/95 PRIMARY GAS SAMPLING SYSTEM	01/30/95 CONTROL SYSTEM	01/30/95 COMBUSTION GAS ANALYZERS	04/04/95 CONTROL VALVES AND ACTUATORS	03/09/95 STEAM CONDITIONING VALVES	04/04/95 AIR FLOW CONTROL DAMPERS	04/12/95 INTRINSIC SAFETY BARRIERS	03/09/95 FLOW ORIFICE PLATES WITH FLANGES	02/20/94 PITOT TUBE FLOW ELEMENTS	03/07/95 LEVEL TRANSMITTERS	06/15/95 LOAD CELL WEIGHING SYSTEM	02/16/95 PRESSURE TRANSMITTERS	02/15/95 PRESSURE SWITCHES	02/16/95 PRESSURE INDICATORS	03/10/95 THERMOCOUPLES AND THERMOWELLS	03/03/95 DIAL THERMOMETERS AND THERMOWELLS
LAT	∢	В	Д	∢ <	< ∢	7	4		4	4	Ø	4	∢	4	4	4	4	∢	¥	∢	4	4	4	∢	4	4	∢
DWG/ SPEC NO.	206.2	207.1	208.2	209.1	209.5	209.6	210.1	210.2	216.2	220.1	302.4	302.5	304.1	305.1	307.1	307.2	307.5	309.1	310.1	310.7	312.2	313.3	314.1	314.2	315.1	316.1	317.1

DWG STATUS LEGEND: 1 = CONCEPTUAL ENGINEERING AT 30% COMPLETE

2 = DESIGN AND DRAFTING AT 70% COMPLETE

3 = 95% COMPLETE (FOR PROGRESS PURPOSES) 4 = PHASE I ENGINEERING COMPLETE

		HC/	IIC.	FC FC FC		
I AMALA.	DWG COST	IFB DATE	IFB DATE	(FB DATE	GOMMENTS	
UMENT INSTALLATION SPEC		02/08/95	04/12/95		PHASE 1 COMPLETE	
5 INSTRUMENT INDEX/LIST	4 4M7310	01/19/95	03/17/95		PHASE 1 COMPLETE	
94 CONTROL SYSTEM DESCRIPTION	4 4M7320	05/23/95	04/21/95		PHASE 1 COMPLETE	
194 SUBSURFACE INVESTIGATION	4 4C7310	10/12/94			PHASE 1 COMPLETE	
1/95 EARTHWORK SITE IMPROVEMENTS	4 4C7310	03/30/95	03/01/95	03/17/95	PHASE 1 COMPLÉTE	
5/95 CONCRETE SPECIFICATION	4 4F7330	03/16/95	02/01/95	03/17/95	PHASE 1 COMPLETE	
4/95 STRUCTURAL AND MISCELLANEOUS STEEL SPEC.	4 4H7340	02/27/95	02/01/95	02/23/95	PHASE 1 COMPLETE	
METAL BUILDING ENCLOSURE	417300.2		36/10/60	02/23/95	PHASE 2	
ARCHITECTURAL BUILDING FINISHES	417300-2		39/10/60	02/23/95	PHASE 2	
GASIFIER BUILDING ELEVATIONS & DETAILS	417300-2		36/10/60		PHASE2	
GASIFIER BUILDING ELEVATIONS & DETAILS	417300.2		03/01/95		PHASE 2	
17/95 CONTROL BUILDING PLANS AND ELEVATIONS	4 417300	01/17/95	03/01/95		PHASE 1 COMPLETE	
BUILDING WALL DETAILS	417300.2		36/10/60		PHASE 2	
19/95 SITE PLAN	4 4C7300	12/22/94	12/13/94		PHASE 1 COMPLETE	
13/95 UNDERGROUND PIPING PLAN	4 4E7300	02/13/95	02/11/95		PHASE 1 COMPLETE	
20/95 ONE LINE DIAGRAM	4 4L7300	01/19/95	01/09/95		PHASE 1 COMPLETE	
23/95 ELECTRIC UNDERGROUND LAYOUT	4 4L7310	02/21/95	02/06/95	02/20/95	PHASE 1 COMPLETE	
23/95 ELECTRIC UNDERGROUND DETAILS	4 4L7310	02/21/95	02/06/95	02/20/95	PHASE 1 COMPLETE	
LIGHTING & PIRE PROTECTION - LEVELS 1 AND 2	41,7370-2		04/19/95		PHASE2	e i
LIGHTING & FIRE PROTECTION - LEVELS 3 AND 4	41.7370-2		36/61/10		PHASE 2	
LIGHTING & FIRE PROTECTION - LEVELS 5 AND DETAI	LS 4L7370-2		\$6/61/10		PHASE 2	
LIGHTING PANEL SCHEDULES	41,7370-2		26/61/10		PHASE 2	
OVERALL ELECTRICAL LAYOUT	4 4L7320		06/15/95		CONCEPTUAL DESIGN	
25/95 GASIFIER RACEWAY - LEVELS I AND 2	4 4L7320	05/01/95	04/19/95			
25/95 GASIFIER RACEWAY - LEVELS 3 AND 4	4 4L7320	05/01/95	04/19/95		PHASE 1 COMPLETE	
25/95 GASIFIER RACEWAY - LEVELS 5 AND 6	4 4L7320	05/01/95	04/19/95		PHASE 1 COMPLETE	
5/95 GASIFIER RACEWAY - LEVELS 7 AND 8	4 4L7320	05/01/95	04/19/95		-	
5/95 SITE RACEWAY & LIGHTING	4 4L7320	05/01/95	04/19/95		PHASE 1 COMPLETE	
5/95 SITE RACEWAY & LIGHTING	4 4L7320	05/01/95	04/19/95		PHASE 1 COMPLETE	
	ES STE CEVA.  S S STE CEVA.  VELS VELS VELS VELS VELS VELS VELS VELS	TEEL SPEC. 4  TEEL SPEC. 4  TAILS  TAILS  ATIONS  A	- 4 4M7340 02/08/95 4 4M7320 05/23/95 4 4M7320 05/23/95 4 4C7310 10/12/94 4 4C7310 03/30/95 4 4F7330 03/16/95 4 4F7330 03/16/95 4 4F7300 01/17/95 4 4F7300 01/17/95 4 4F7300 01/17/95 4 4F7300 01/19/95 4 4F7310 02/21/95 4 4F7320 05/01/95	4 4M7340 02/08/95 4 4M7320 05/23/95 4 4M7320 05/23/95 4 4C7310 10/12/94 4 4C7310 03/30/95 4 4F7330 03/16/95 4 4F7330 03/16/95 4 4F7300 02/27/95 4 4T7300 01/17/95 4 4T7300 01/19/95 4 4T7310 02/21/95 4 4T7320 05/01/95	- 4 4M7340 02/08/95 04/12/95 4 4M7310 01/19/95 03/17/95 4 4M7320 05/23/95 04/21/95 4 4C7310 10/12/94 4 4C7310 03/30/95 03/01/95 4 4F7330 03/16/95 02/01/95 4 4F7330 03/16/95 02/01/95 4 4F7330 03/16/95 02/01/95 4 4F7340.2 02/27/95 02/01/95 4 4T7300 01/17/95 03/01/95 4 4C7300 12/22/94 12/13/94 4 4C7300 01/17/95 03/01/95 4 4C7310 02/21/95 02/06/95 6 4 4C7310 02/21/95 04/19/95 6 4 4C7320 05/01/95 04/19/95	TEEL SPEC. 4 4M7340 02/08/95 04/12/95 4 4M77310 01/19/95 03/17/95 4 4M77320 05/23/95 04/21/95 4 4C7310 10/12/94 4 4C7310 03/30/95 03/11/95 03/17/95 4 4C7310 03/30/95 02/01/95 03/17/95 4 4F7330 03/16/95 02/01/95 02/23/95 4 4T730.2 01/17/95 03/01/95 4 4T730.2 01/17/95 03/01/95 4 4T730.0 01/17/95 03/01/95 4 4T7310 02/21/95 02/06/95 02/20/95 4 4T7320 05/01/95 04/19/95 6 4 4T7320 05/01/95 04/19/95 6 4 4T7320 05/01/95 04/19/95 7 4 4T7320 05/01/95 04/19/95

DWG STATUS LEGEND: 1 = CONCÈPTUAL ENGINEERING AT 30% COMPLETE

2 = DESIGN AND DRAFTING AT 70% COMPLETE 3 = 95% COMPLETE (FOR PROGRESS PURPOSES) 4 = PHASE 1 ENGINEERING COMPLETE

Ç	LAT EST REV DATE TITLE	DWG COST STATUS CODE	THE THE THE DATE DATE	COMMENTS	
E046,SH.3 E046,SH.4	1 04/25/95 SITE RACEWAY & LIGHTING 1 04/25/95 SITE RACEWAY & LIGHTING CONTROL POOM PACEWAY	4 4L7320 4 4L7320 4 41.7320	95 04/19/95 95 04/19/95 04/19/95		
EOSO-A FOSO-I	480V MCC COVER SHEET FUET RECEIVING HOPPER FEEDER :- WD	41.7380-2	04/19/95	PHASE 2 PHASE 2	
E050-3	FUEL CONVEYOR WD LOCK HOPPER VALYE 1 WD	4L7380-2 4L7380-2	04/19/95 04/19/95	PHASE 2 PHASE 2	
E050-5 E050-6		4L7380.2 4L7380.2	04/19/95 04/19/95	PHASE2 PHASE2	
E050.7	AN 1-WD (COMBUSTOR ST	4L7380-2 (ARELUP) 4L7380-2	04/19/95 04/19/95	PHASE2 PHASE2	
E050-9 5050-10	COMBUSTION AIR FAN 2-WTI (COMBUSTOR AUX COMBUSTION AIR FAN 3-WTI (BOILER)	,	04/19/95 04/19/95	PHASE2 PHASE2	
B050-12 B050-12	LIGHTING TRANSFORMERS LT-1 FEEDER MISC POWER TRANSFORMER DT-1 FEEDER	4L7380-2 4L7380-2	04/19/95 04/19/95	PHASE2 PHASE2	
E050-13 E050-14	UPS POWER FEED CONTROL ROOM HVAC REED	41.7380.2 41.7380.2	04/19/95 04/19/95	PHASE 2	
E050-15 E050-16	BUILDING EXHAUST FANS - WD 480Y WELDING RECEPTACLE PEED	41,7380.2	04/19/95 04/19/95	PHASE2 PHASE2	
E060.A 5060.1	MASC EQUIPMENT WIRING COVER SHEET STARTIP BURNER - WD	41.7340.2 41.7340.2	04/19/95 04/19/95	PHASE2 PHASE2	
E060.2 E060.8	FIRE PROTECTION PANEL. WD ASH SYSTEM WD - SHEET I	41.7340.2 41.7340.2 41.7340.2	04/19/95 04/19/95 04/19/95	PHASE2 PHASE2 PHASE2	
E070-10	AGRICATION WAY STATE A PRODUCT GAS SAMPLER WD INSTRUMENT WIRING COVER SHEET	41,7340-2	04/19/95 04/19/95	PHASE 2 PHASE 2	
E070-1 E070-2	INST. JUNCTION BOX 1 - WIRING INST. JUNCTION BOX 2 - WIRING	41.7340.2	04/19/95 04/19/95	PHASE2 PHASE2	

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4 = PHASE 1 ENGINEERING COMPLETE

	PHASE 2 PHASE 2	PHASE2	PHASE 1 COMPLETE	PHASE 1 COMPLETE	NEEDS FINAL LOADS/	FLARE VERIFICATION	NEEDS FINAL LOADS/	FLARE VERIFICATION	NEEDS FINAL LOADS/	FLARE VERIFICATION	NEEDS FINAL LOADS/	FLARE VERIFICATION .	NEEDS FINAL LOADS/	FLARE VERIFICATION	PHASE 1 COMPLETE	NEEDS FINAL EQUIP. VERIF.	NEEDS FINAL EQUIP. VERIF.	NEEDS FINAL REFRACT. VERIF.	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE '	PHASE 1 COMPLETE
PROJETI IFC/ IFB DATE					05/08/95		05/08/95		05/08/95		05/08/95		05/08/95			05/08/95	05/08/95		03/17/95	03/17/95	03/17/95							
ACTUAL PLANNED PROJECTO JEC/ JEC/ JEC/ JEB JEB JEB DATE DATE DATE	04/19/95	04/19/95	02/01/95	02/01/95	02/24/95		02/24/95		02/24/95		02/24/95		02/24/95			02/28/95	02/28/95	04/19/95	11/18/95	12/05/94	12/05/94	12/05/94		04/03/95	04/03/95	04/03/95	04/03/95	04/03/95
			01/17/95	01/17/95	05/08/95		05/08/95		05/08/95		05/08/95		05/08/95		01/17/95	05/08/95	05/08/95	05/08/95	02/08/95	02/08/95	02/08/95	11/21/94	01/12/95	03/20/95	03/20/95	03/20/95	03/20/95	03/20/95
DWG COST STATUS CODE	41,7340.3	41,7340.2	4 4F7300	4 4F7300	4 4F7340		4 4F7340		4 4F7340		4 4F7340		4 4F7340		4 4F7320	4 4F7350	4 4F7350	4 4F7430	4 4S7390	4 487390	4 487390	4 4S7390	4 487390	4 4K7300	· 4 4K7300	4 4K7300	4 4K7300	4 4K7300
LAT EST REV DATE TITLE	MISC INST. WIRING . 2 MISC. INST. WIRING . 3	MISC. INST. WIRING 4	01/17/95 STRUCTUAL DESIGN NOTES	01/11/95 TYPICAL CONCRETE DETAILS	05/05/95 GASIFIER BUILDING PILE PLAN		05/05/95 GASIFIER BUILDING FOUNDATION PLAN		05/05/95 GASIFIER BUILDING FOUNDATION SECTION & DET		05/05/95 GASIFER BUILDING FOUNDATION SECTIONS & DET		05/05/95 GASIFIER BUILDING SLAB PLAN		01/17/95 CONTROL BLDG. FNDN. PLANS & SECTIONS	05/05/95 FUEL HANDLING FOUNDATION PLAN & SECTIONS	05/05/95 FUEL HANDLING FOUNDATION PLANS, SEC. & DET	05/05/95 UTILITY BRIDGE FOUNDATION	07/07/95 MASS/HEAT BALANCE GEN. DIAGRAM	03/14/95 MASS/HEAT BALANCE 20% MOISTURE CASE	03/14/95 MASS/HEAT BALANCE 45% MOISTURE CASE	11/17/94 FUEL HANDLING FLOW DIAGRAM	01/11/95 ASH HANDLING SYSTEM	06/15/95 GENERAL ARRANGEMENT, LEVEL 1 & 2	. 06/15/95 GENERAL ARRANGEMENT, LEVEL 3 & 4	06/15/95 GENERAL ARRANGEMENT, LEVEL 5 & 6	. 06/15/95 GENERAL ARRANGEMENT, LEVEL 7 & 8	06/15/95 SOUTH GASIFIER BUILDING ELEV.
L			-	-	-		_		-						-	-	-		4	<u>د.</u>	2	-	-	¥	<b>∀</b>	∢	4	∢
DWG/ SPEC NO.	E070-4 E070-5	E070-6	F001	F002	F005,SH.1		F005,SH.2		F005,SH.3		F005,SH.4	•	F005,SH.5		F006	F010,SH.1	F010,SH.2	F015	FD001,SH1	FD001,SH2	FD001,SH3	FD010	FD011	GA01	GA02	GA03	GA04	GA05

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										,			•																
COMMENTS	PHASE 1 COMPLETE	•	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE '	PHASE 1 COMPLETE
ACTUAL PLANNED PHOJCT'D BC BC FC BB FB FB DATE DATE								05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95	05/12/95
PLANNEL IFC/ IFB DATE	04/03/95	04/03/95	04/03/95	04/03/95	04/03/95			04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95	04/12/95
ACTUAL IFC/ IFB DATE	03/20/95	03/20/95	03/20/95	03/20/95	03/20/95	01/17/95	92/08/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95	05/23/95
DWG GOST STATUS GODE	4 4K7300	4 4K7300	4 4K7300	4 4K7300	4 4K7300	, 4 4U7330	4 4U7330	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320	4 4M7320
LAT EST REV DATE TITLE	06/15/95 NORTH GASIFIER BUILDING ELEV.	06/15/95 WEST GASIFIER BLDG. ELEV. (LOWER)	06/15/95 WEST GASIFIER BLDG. ELEV. (UPPER)	06/15/95 EAST GASIFIER BLDG. ELEV. (LOWER)	06/15/95 EAST GASIFIER BLDG. ELEV. (UPPER)	01/13/95 GENERAL ARRANGEMENT CONTROL BUILDING (PL	05/05/95 GENERAL ARRANGEMENT FUEL HANDLING	05/17/95 INDEX - LOGIC DRAWINGS	05/18/95 CONTROL LOGIC LEGEND	05/18/95 STEAM SUPPLY LOGIC	05/18/95 GASIFIER COMBUSTION LOGIC	05/18/95 GASIFIER BURNER COMB. CONTROL	05/18/95 GAS FLOW MEASUREMENT LOGIC	05/18/95 COMBUSTOR COMBUSTION CONTROL	05/18/95 START-UP BURNER COMBUSTION CONTROL	05/18/95 GASIFIER INTERLÓCKS	05/18/95 SOLIDS CIRCULATING CONTROLS	05/18/95 WOOD FUEL HANDLING LOGIC	05/18/95 WOOD FUEL HANDLING LOGIC	05/18/95 COMB. OVERBED BURNER CONTROL	05/18/95 MISC. MOTOR LOGIC	05/18/95 REFRACTORY TEMPERATURES	05/18/95 GASIFIER CONTROLS	05/18/95 COMBUSTOR CONTROLS	05/18/95 COMBUSTOR BLOWER	05/18/95 GASIFIER BLOWER	05/18/95 PRODUCT GAS LOGIC	05/18/95 ANALOG INDICATORS SHEET 1	05/18/95 ANALOG INDICATORS SHEET 2
T.	4	∢	4	4	4	-	<b>-</b>	<b>-</b>	-	-	-	<del></del>		-		-		-	-	<b>-</b>	<b>-</b>	-	-	-	-		-	-	
DWG/ SPEC NO.	GA06	GA07,SH.1	GA07,SH.2	G008,SH.1	G008,SH.2	GA010	GA020	1000	1001	1002	1003	1004	1005	9001	1001	1008	6001	1010	1011	1012	1013	1014	1015	1016	1017	· I018	1020	1021	1022

DWG STATUS LEGEND: 1 = CONCEPTUAL ENGINEERING AT 30% COMPLETE

2 = DESIGN AND DRAFTING AT 70% COMPLETE

3 = 95% COMPLETE (FOR PROGRESS PURPOSES) 4 = PHASE I ENGINEERING COMPLETE

COMMENTS PHASE 1 COMPLETE	PHASE 2
PROJECT D IFC/ IFC/ IFD/ IFD/ DATE 05/12/95 05/12/95 05/12/95 05/12/95 05/12/95 05/12/95 05/12/95 05/12/95 05/12/95 05/12/95 05/12/95 05/15/95 05/15/95 05/15/95	
HCT IFC/ IFC/ IFC/ IFC/ IFC/ IFC/ IFC/ IFC/	04/19/95 04/19/95 04/19/95 04/19/95 04/19/95 04/19/95 04/19/95 04/19/95
	4M7340.2 4M7340.2 4M7340.2 4M7340.2 4M7340.2 4M7340.2 4M7340.2 4M7340.2 4M7340.2 4M7340.2 4M7340.2 4M7340.2
DWG STATUS SQ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	\$4\$\$\$\$\$\$\$\$\$\$\$ 
LAT EST  REV 15ATE  OS/18/95 ASH HANDLING  OS/18/95 DIGITAL INDICATORS SHEET 1  OS/18/95 DIGITAL INDICATORS SHEET 2  OS/18/95 DIGITAL INDICATORS SHEET 2  OS/18/95 DIGITAL INDICATORS SHEET 1  OS/18/95 GASIFIER TRIPS  OS/18/95 GASIFIER TRIPS  OS/18/95 FUEL FEEDER TEMPERATURE  OS/01/95 INSTRUMENT LOCATION DIAGRAM, LEVEL 1 & 2  OS/01/95 INSTRUMENT LOCATION DIAGRAM, LEVEL 3 & 4  OS/01/95 INSTRUMENT LOCATION DIAGRAM, LEVEL 3 & 8  OS/01/95 INSTRUMENT LOCATION DIAGRAM, LEVEL 7 & 8  OS/01/95 INSTRUMENT LOCATION DIAGRAM, FUEL HANDLI	INSTRUMENT INSTALLATION DETAILS INDEX INSTRUMENT INSTALLATION DETAIL
	0 = 2 % 4 % 9 % % % % % % % % % % % % % % % %
DWG SPHG 1025 1026 1037 1030 1033 1034 1100 1101 1101 1103	

DWG STATUS LEGEND: 1 = CONCÈPTUAL ENGINEERING AT 30% COMPLETE

2 = DESIGN AND DRAFTING AT 70% COMPLETE 3 = 95% COMPLETE (FOR PROGRESS PURPOSES) 4 = PHASE 1 ENGINEERING COMPLETE

) Exima		ACTUAL PLA	ACTUAL PLANNED PROJETO	
_	LAT EST REV DATE TITLE	щ		COMMENTS
D90-14		4M7340-2	2	PHASE2
1300-15 1300-16	INSTRUMENT INSTALLATION DETAIL INSTRUMENT INSTALLATION DETAIL	1 4M7340:2 04/1	JA719/95 D4/19/95	HASEZ PHASEZ
D00-17	INSTRUMENT INSTALLATION DEPAIL		04/19/95	PHASES
1300-19	INSTRUMENT INSTALLATION DELAH. INSTRUMENT INSTALLATION DETAH:	1 4M7340.2 04)19/95	04/19/95	FRASE 2. PHASE 2.
1300-20	INSTRUMENT INSTALLATION DETAIL		34/19/95	PHASE2
1300:21	INSTRUMENT INSTALLATION DETAIL		04/19/95	PHASE2
1300.22	INSTRUMENT INSTALLATION DETAIL		04/19/95	PHASE 2 Principle
1300-23 1490-24	INSTRUMENT INSTALLATION DELAIL INSTRUMENT INSTALLATION DELAIL	1 4M/34U52 (4419/93 1 4M/34U2 (4419/95	9992	FEASE S PHASE 2
1300.25	INSTRUMENT INSTALLATION DETAIL		36/8	PHASEZ
M001	A '06/26/95 GASIFIER VESSEL	4 4K7300 03/17/95 03/01/95		
M002,SH.1	A 06/26/95 GASIFIER SECTIONS & DETAILS	03/17/95	_	
M002,SH.2		03/11/95		-
M002,SH.3	A 06/26/95 GASIFIER SECTIONS & DETAILS	03/17/95	_	_
M003		03/17/95	_	<del>-</del>
M004,SH.1		03/17/95		<del>, ,</del>
M004,SH.2	A 06/26/95 COMBUSTOR SECTIONS & DETAILS	4 4K/300 03/17/95 03/01/95	28//L/80 C6/I	PHASET COMPLETE
M004,5H.3	A 00/20/93 COMBUSTOR SECTIONS & DETAILS  Objects of Asserted Average Asserted Assert		105 02/17/06	DE ETE : VENDOB TRAVING
MOOF	ON/1975 COMBUSTOR CYCLONE	03/17/95		DELETE - VENDOR DRAWING
M007	I 03/13/95 SECONDARY CYCLONE	4 4107300 03/11/95 03/01/95		DELETE VENDOR DRAWING
MOOS	2 04/1795 CYCLONE DASH POTS 1 02/17/05 MAYOTTE EAVER HARDED	4 4K7308 03/17/95 03/01/95		DELETE - VENDOR DRAWING DELETE - VENDOR PRAWING
M010	2 04/17/95 MISCELLANEOUS DUCTING	4K7300	1/95 05/12/95	NEEDS ADDITIONAL DESIGN/DRAFTING
M011	A 06/26/95 L-VALVE DETAILS	07/13/95		PHASE 1 COMPLETE
M012 2	2 04/17/95 GASIFIER TO COMBUSTOR PEED LINE			DELETE - NOT APPLICABLE
MOI3	SAND SILO TO COMBUSTOR	4 4K7306 03/01/95	1/95 05/12/95	DELETE: VENDOR DRAWING

DWG STATUS LEGEND: 1 = CONCÉPTUAL ENGINEERING AT 30% COMPLETE

2 = DESIGN AND DRAFTING AT 70% COMPLETE

3 = 95% COMPLETE (FOR PROGRESS PURPOSES) 4 = PHASE I ENGINEERING COMPLETE

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COMMENTS	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	_	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY .	PHASE 1 COMPLETE
ACTUAL PLANNED PROJECTD BECT FCC BB FFB FFB DATE DATE																			06/15/95	06/15/95	06/15/95	06/15/95	06/15/95	06/15/95	06/15/95	06/15/95	06/15/95	06/15/95	05/01/95
L PLANNEI IFC! IFB DATE					04/17/95	04/17/95	04/17/95	04/17/95	04/17/95	04/17/95	04/17/95	04/17/95	04/17/95	04/17/95	04/17/95	04/11/95	04/17/95	04/17/95	04/19/95	04/19/95	04/19/95	04/19/95	04/19/95	04/19/95	04/19/95	04/19/95	04/19/95	04/19/95	04/19/95
ACTUAL IFC/ IFB DATE	03/17/95	03/17/95	03/17/95	03/11/95	01/18/95	01/18/95	01/18/95	01/18/95	01/18/95	01/18/95	07/11/95	01/18/95	01/18/95	01/18/95	01/18/95	01/18/95	01/18/95	07/11/95											05/02/95
DWG COST STATUS CODE	4 4K7300	4 4K7300	4 4K7300	4 4K7300	4 4S7380	4 4S7380	4 4S7380	4 487380	4 4S7380	4 4S7380	4 4S7380	4 4S7380	4 4S7380	4 487380	4 4U7330	4 4U7330	4 4S7380	4 4S7380	4 4K7320	4 4K7320	4 4K7320	4 4K7320	4 4K7320	4 4K7320	4 4K7320	4 4K7320	4 4K7320	4 4K7320	4 4K7320
LAT EST REV DATE TITLE	96/30/92	A 06/30/95 SECTIONS A-A, BB	A 06/30/95 SECTIONS C.C, DD	A 06/30/95 VESSEL SECTIONS E-E, F-F	3 07/07/95 PIPING & INSTRUMENT SYMBOLS	2 07/07/95 PIPING & INSTRUMENT SYMBOLS	3 07/07/95 PIPING STANDARDS P&ID	2 07/07/95 PIPING STANDARDS P&ID	3 03/16/95 COMBUSTER AIR AND NATURAL GAS P&ID	3 03/16/95 GASIFIER AND COMBUSTER P&ID	1 07/07/94 GASIFIER AND COMBUSTER P&ID	3 07/07/95 PRODUCT GAS BURNER P&ID	3 07/07/95 SEAL STEAM P&ID	3 07/07/95 INSTRUMENT & SERVICE AIR P&ID	3 07/07/95 ASH SYSTEM P&ID	3 03/16/95 FUEL HANDLING P&ID	3 03/16/95 SERVICE SYSTEMS P&ID	1 07/07/95 INERT GAS P&ID	PIPING PLAN - LOWER LEVEL & LEVEL 2	PIPING PLAN - LEVEL 3 & 4	PIPING PLAN - LEVEL 5 & 6	PIPING ELEVATION - FRONT	PIPING ELEVATION - RIGHT SIDE	PIPING ELEVATION - LEFT SIDE	PIPING ELEVATION - REAR	PIPING SECTIONS & DETAILS	PIPING SECTIONS & DETAILS	PIPING SECTIONS & DETAILS	1 05/02/95 PIPING PLAN - UTILITY BRIDGE
1		•	•	4	ന	64	m	7	e.	. 3	1	m	m	m	m	m	m	-											_
DWG/ SPEC NO.	M020	M023	M024	M025	P001,SH1	P001,SH2	P002,SH1	P002,SH2	P003	P004,SH.1	P004,SH.1	P005	P006	P007	P008	P009	P010	P011	P100	P101	P102	P103	P104	P105	P106	P107	P108	P109	P110

DWG STATUS LEGEND: 1 = CONCÉPTUAL ENGINEERING AT 30% COMPLETE 2 = DESIGN AND DRAFTING AT 70% COMPLETE

3 = 95% COMPLETE (FOR PROGRESS PURPOSES) 4 = PHASE I ENGINEERING COMPLETE

	PHASE 1 COMPLETE PHASE 1 COMPLETE	PHASE 1 COMPLETE	PRELIM ROUTING ONLY	PRELIM ROUTING ONLY	NEEDS FINAL DRAFTING	-	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	_	•	~	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	•	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	DELETE - NOT APPLICABLE	DELETE - NOT APPLICABLE	DELETE - NOT APPLICABLE
ACTUAL PLANNED PHOIGT'D LECT LECT FOU THE TER FEB DATE DATE DATE	05/01/95	05/01/95	06/15/95	06/15/95	06/15/95																					07/15/95	07/15/95	07/15/95
C. PLANNEI IPC/ IFB DATE	04/19/95	_	04/19/95	04/19/95	02/01/95	01/06/95	01/06/95	01/06/95	01/06/95	01/06/95	01/06/95	01/06/95	01/06/95	01/06/95	01/06/95	01/06/95	01/06/95	96/90/10	01/06/95	01/06/95	96/90/10	01/06/95	01/06/95	01/06/95	01/06/95	04/19/95	04/19/95	04/19/95
ACTUA IFC/ IFB DATE	05/02/95	05/02/95				01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95	01/09/95			
DWG COST STATUS CODE	4 4K7320 4 4K7320	4 4K7320	4 4K7320	4 4K7320	4 4K7320	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	4 4K7370	1.487370	1 487370	1 4K7370
LAT EST REV DATE TITLE	1 05/02/95 BLR. BLDG. PIPING PLAN GROUND FLOOR TO EL. 14	1 05/02/95 BLR, BLDG, PIPING PLAN EL 141'-0" AND UP - NORT	. PIPING SECTIONS & DETAILS	PIPING SECTIONS & DETAILS	VESSEL ASSEMBLY - EXPANSION RECORD	A 01/09/95 PIPING STANDARDS INDEX	A 01/09/95 PIPE SUPPORTS SCOPE	A 01/09/95 PIPE SUPPORTS SCOPE	A 01/09/95 PIPE SUPPORTS SCOPE	A 01/09/95 PIPE SUPPORTS SPACING TABLE	A 01/09/95 PIPE SUPPORT CALL-OUT	A 01/09/95 PIPE SUPPORT ADJ. CLEVIS HANGER	A 01/09/95 PIPE SUPPORT MED. CLAMP WITH T.B.	A 01/09/95 PIPE SUPPORT DOUBLE BOLT CLAMP WITH T.B.	A 01/09/95 PIPING SUPPORT LUG ATTACHMENT WITH T.B.	A 01/09/95 WEAR SHOE FOR UNINSULATED PIPE	A 01/09/95 WEAR SHOE FOR UNINSULATED PIPE (4" MAX. INS	A 01/09/95 WEAR SHOE FOR UNINSULATED PIPE (6" MAX. INS	A 01/09/95 RIGID PIPE STANCHION TO FLOOR	A 01/09/95 ADJUSTABLE GLIDING SUPPORT	A 01/09/95 HOSE STATION COLUMN MOUNTED	A 01/09/95 SAFETY VALVE DRIP PAN ASSEMBLY	A 01/09/95 SAFETY VALVE DRIP PAN ASSEMBLY FOR CON. 270	A 01/09/95 PERSONNEL PROTECTION LAGGING	A 01/09/95 PERSONNEL PROTECTION PERFORATED METAL GU	PIE SUPPORT DETAIL	PIPE SUPPORT DETAIL	PIPE SUPPORT DETAIL
DWG/ SPEC NO.	P112,SH.1	P112.SH.3	P115	P116	P120	PDS-00	PDS-10.1.1	PDS-10.1.2	PDS-10.1.3	PDS-10.2	PDS-10.3	PDS-10.4.01	PDS-10.4.02	PDS-10.4.03	PDS-10.4.04	PDS-10.4.20	PDS-10.4.21	PDS-10.4.22	PDS-10.4.40	PDS-10.4.41	PDS-11	PDS-13.1	PDS-13.2	PDS-15.1	PDS-15.2	PS300	P\$301	PS302

DWG STATUS LEGEND : 1 = CONCEPTUAL ENGINEERING AT 30% COMPLETE 2 = DESIGN AND DRAFTING AT 70% COMPLETE

3 = 95% COMPLETE (FOR PROGRESS PURPOSES) 4 = PHASE 1 ENGINEERING COMPLETE

JTD COMMENTS	95 DELETE - NOT APPLICABLE		95 DELETE - NOT APPLICABLE	DELETE		DELETE	DELETE				95 DELETE - NOT APPLICABLE			NEEDS ADDITIONAL ANALYSIS	NEEDS ADDITIONAL ANALYSIS	NEEDS ADDITIONAL ANALYSIS	NEEDS CHECK FINAL CONFIG.	NEEDS FINAL ROUTING	NEEDS CHECK FINAL CONFIG.	NEEDS ADDITIONAL ANALYSIS	NEEDS ADDITIONAL ANALYSIS	NEEDS ADDITIONAL ANALYSIS	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE	PHASE 1 COMPLETE.	PHASE 1 COMPLETE	PHASE 1 COMPLETE .	PHASE 1 COMPLETE
ACTUAL PLANNED PHOJCT'D  FC ECT FC  DWG COST FFB FFB FFB  STATUS CODE DATE DATE	1 4K7370 04/19/95 07/16/95	04/19/95		04/19/95		04/19/95	04/19/95	04/19/95		04/19/95	1 4K7370 04/19/95 07/15/95	1 4K7370 04/19/95 07/15/95	1 4K7370 04/19/95 07/15/95	4 4K7370 07/13/95	4 4K7370	4 4K7370 07/13/95	4 4H7300 01/17/95 01/10/95	4 4H7310 01/17/95 01/10/95	4 4H7310 01/17/95 01/10/95	4 4H7310 01/17/95 01/10/95	4 4H7310 01/17/95 01/10/95	4 4H7310 01/17/95 01/10/95	4 4H7310 01/17/95						
LAT EST REV DATE TITLE	PIPE SUPPORT DETAIL	PIPE SUPPORT DETAIL	PIRE SUPPORT DETAIL	PIPE SUPPORT DETAIL	PIPE SUPPORT DET ALL	PIPE SUPPORT DETAIL	PIPE SUPPORT DETAIL	PIPE SUPPORT DETAIL	PREL 06/25/95 PIPE SUPPORT DETAIL LOG	PIPE SUPPORT DETAIL LOG	PREL 06/25/95 PIPE SUPPORT DETAIL LOG	PREL 05/25/95 PIPE SUPPORT DETAIL LOG	PREL 07/15/95 PIPE SUPPORT DETAIL LOG	PREL 05/25/95 PIPE SUPPORT DETAIL LOG	PREL 06/25/95 PIPE SUPPORT DETAIL LOG	PREL.06/25/95 PIPE SUPPORT DETAIL LOG	PREL 06/25/95 PIPE SUPPORT DETAIL LOG	1 01/17/95 STANDARD STEEL DETAILS	1 01/17/95 STANDARD GRATING DETAILS	1 01/17/95 STANDARD FLOORPLATE DETAILS	1 01/17/95 STANDARD LADDER DETAILS	1 01/17/95 STANDARD LADDER DETAILS	1 01/17/95 STANDARD HANDRAIL DETAILS	1 01/17/95 STANDARD HANDRAIL DETAILS					
DWG/ SPEC NO.	PS303	PS304	PS305	P8306	PS307	PS308	PS309	PS310	PS311	PS312	PS313	PS314	PS315	PSCA002	PSCA003	PSCA005	PSFG003	PSLPS001	PSPG002	PSPG004	PSSC001	PSSC002	2001	2002	S003	S004,SH.1	S004,SH.2	S005,SH.1	S005,SH.2

DWG STATUS LEGEND: 1 = CONCÉPTUAL ENGINEERING AT 30% COMPLETE 2 = DESIGN AND DRAFTING AT 70% COMPLETE

3 = 95% COMPLETE (FOR PROGRESS PURPOSES) 4 = PHASE 1 ENGINEERING COMPLETE

0		*****	PHASE 1 COMPLETE	PHASE 1 COMPLETE	NEEDS FINAL CALC. & CHECK	NEEDS FINAL CALC. & CHECK	NEEDS FINAL CALC, & CHECK	NEEDS FINAL CALC, & CHECK	NEEDS FINAL CALC, & CHECK	NEEDS FINAL CALC. & CHECK	NEEDS FINAL CALC. & CHECK	NEEDS FINAL CALC. & CHECK	NEEDS FINAL CALC, & CHECK	NEEDS FINAL CALC, & CHECK	NEEDS FINAL CALC, & CHECK ·	NEEDS FINAL CALC, & CHECK	NEEDS FINAL CALC, & CHECK	NEEDS FINAL CALC. & CHECK	NEEDS FINAL CALC. & CHECK	NEEDS REFRACTORY VERIF.	NEEDS REFRACTORY VERIF.	NEEDS REFRACTORY VERIF.	NEEDS REFRACTORY VERIF.
PROJECT	<u> </u>	DATE			04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95
ACTUAL PLANNED	IFC/	DATE DATE	01/10/95	01/17/95	03/24/95	03/24/95	03/24/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	04/14/95	02/24/95	02/24/95	02/24/95	02/24/95
	DWG COST	ž2	4 4H7310	4 4H7310	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340	4 4H7340
	LAT EST	REV DATE TITLE	1 01/17/95 STANDARD STAIR DETAILS	1 01/17/95 STANDARD STAIR DETAILS	1 04/17/95 ROOF PLAN	1 04/17/95 FRAMING PLAN T.O.S. EL. 215'-0"	1 · 04/17/95 FRAMING TOS EL. 203'-6"/203'-2"	1 04/17/95 FRAMING PLAN TOS EL. 189'-5 1/2"	1 04/17/95 FRAMING PLAN TOS EL. 177'-4 3/4"	1 04/17/95 PLAN TOS EL. 166'-4 1/2" & 163'-9 1/2"	1 04/17/95 PLAN FRAMING TOS EL. 151'-7 3/4"	1 04/17/95 FRAMING PLAN TOS EL. 142'-7 3/4"	1 04/17/95 FRAMING PLAN TOS EL. 130'-11 3/4"	1 04/17/95 ELEVATION COL. LINE B, E & 1	1 04/17/95 ELEVATION COL. LINE 4, 5, C.3,3 & F	1 04/17/95 STAIR SECTIONS	1 04/17/95 SECTIONS COL, LINES C AND D	1 04/17/95 SECTIONS COL, LINES 2 AND 3"	1 04/17/95 TRUSS, SWAY BRACE AND MISC. DETAILS	1 04/21/95 UTILITY BRIDGE PLANS	1 04/21/95 UTILITY BRIDGE SECTIONS AND DETAILS	1 04/21/95 UTILITY BRIDGE SECTIONS AND DETAILS	1 04/21/95 UTILITY BRIDGE SECTIONS AND DETAILS
			-:	7.	<b>∹</b>	7		4.	'n.	9.	7	∞.	o:	10	Ξ	12	13	14	15	Ξ.	۲.	i.	4
	DWG/ SPEC	ÖX.	S006,SH.1	S006,SH.2	S010,SH.1	S010,SH.2	S010,SH.3	S010,SH.4	S010,SH.5	S010,SH.6	S010,SH.7	S010,SH.8	S010,SH.9	S010,SH10	S010,SH11	S010,SH12	S010,SH13	S010,SH14	S010,SH15	S019,SH.1	S019,SH.2	S019,SH.3	S019,SH.4