

ChevronTexaco provides no warranties, either express or implied, as to the accuracy or validity of any of the work in this report. Anyone accessing or using the reports indemnifies and holds ChevronTexaco harmless against any liability that comes from using or relying on the information contained therein.

PERSONAL AND CONFIDENTIAL

HYDROCARBON SYNTHESIS

2001-2-P

11-8-55

THE TEXAS COMPANY

RESEARCH AND TECHNICAL DEPARTMENT



REPORT ON

HYDROCARBON SYNTHESIS

EFFECT OF REDUCTION TEMPERATURE ON SYNTHESIS CATALYST

RUNS 63, 64, 65, AND 66

NOTICE

The information herein contained is not public but belongs to The Texas Company which has provided it solely for an expressly restricted private use. All persons, firms or corporations who receive such information shall be deemed by their act of receiving the same to have agreed to make no duplication or other disclosure or use whatsoever of any or all of such information except such restricted use as is expressly authorized in writing by The Texas Company.

Laboratory Montebello

Report No. 2001-2-P

Date November 8, 1955

PERSONAL AND CONFIDENTIAL

BRIEF OF PARTIAL REPORT

Laboratory Montebello

Date Approved November 8, 1955

Date Work Completed February 4, 1952

Experiment No. 2001

Partial Report No. 2

Subject: Hydrocarbon
Synthesis

Subject: Hydrocarbon Synthesis: Effect of Reduction Temperature on Synthesis Catalyst

Object: (1) To determine whether the poor yields at the Carthage Hydrocol, Inc., plant at Brownsville, Texas, were due in part to methods of catalyst preparation.
(2) To determine whether high reduction temperature could be used to speed the preparation of catalyst without affecting catalyst quality.

History: The yields at the Carthage Hydrocol, Inc., plant had never reached design level nor had they ever been as high as those obtained in pilot plants. It was desired to increase the capacity of the catalyst reduction facilities and one possibility was to use higher reduction temperatures.

Experimental Work: A run was made with the Montebello hydrocarbon synthesis reactor evaluating Bethlehem mill scale catalyst promoted, sized, and reduced at Brownsville. Three additional runs were made using Bethlehem mill scale catalysts reduced at different temperatures. During part of one run the effects of recycle/fresh feed ratio were investigated. Near the end of another run, an attempt was made to increase the promoter on the catalyst by the addition of anhydrous potassium carbonate.

Conclusions: 1. The mill scale catalyst treated and reduced at Brownsville exhibited no difference from mill scale catalysts prepared at Montebello.
2. Variation of the catalyst reduction temperature in the range of 650°F to 800°F had no effect on the quality of the catalyst.
3. Increasing the recycle/fresh feed ratio in the range of 0.06/1 to 2.0/1 increased the yields of saleable liquid products and suppressed the yields of methane and CO₂.
4. The addition of anhydrous potassium carbonate to the catalyst bed during a run had no effect on the synthesis reaction.

WIS-EW

(WEK-WAMcM)-WJC(2)-RWH-HDM(2)-RLSr(2)-duBE(2)
WMS-RP-CEL-GK-FHH-~~XXXX~~ JCW

NOTICE

The information herein contained is not public but belongs to The Texas Company which has provided it solely for an expressly restricted private use. All persons, firms or corporations who receive such information shall be deemed by their act of receiving the same to have agreed to make no duplication or other disclosure or use whatsoever of any or all of such information except such restricted use as is expressly authorized in writing by The Texas Company.

PERSONAL AND CONFIDENTIAL

HYDROCARBON SYNTHESIS

PARTIAL REPORT NO. 2

Montebello Research Laboratory

Experiment No. 2001

Work Completed: February 4, 1952

Report Approved: Nov. 8, 1955

EFFECT OF REDUCTION TEMPERATURE ON SYNTHESIS CATALYST

RUNS 63, 64, 65, AND 66

INDEX

	<u>Page</u>
I. INTRODUCTION	1
II. EQUIPMENT AND MATERIALS	2
III. OPERATIONS	4
IV. RESULTS AND DISCUSSION	7
V. CONCLUSIONS	10
VI. APPENDIX	12

INDEX TO FIGURES

1	HYDROCARBON AND CHEMICALS YIELDS VS. CATALYST AGE	5
2	YIELDS OF WATER AND CO ₂	6

INDEX TO TABLES

I.	SUMMARY OF DATA AND OPERATING CONDITIONS	3
II.	EFFECT OF RECYCLE RATIO ON PRODUCT DISTRIBUTION	8

NOTICE

The information herein contained is not public but belongs to The Texas Company which has purchased it solely for an expressly restricted private use. All persons, firms or organizations who receive such information shall be deemed to have agreed to make no duplication or other disclosure or use whatsoever of any or all of such information except such restricted use as is expressly authorized in writing by The Texas Company.

PERSONAL AND CONFIDENTIAL

HYDROCARBON SYNTHESIS

PARTIAL REPORT NO. 2

Montebello Research Laboratory
Work Completed: February 4, 1952

Experiment No. 2001
Report Approved: Nov. 8, 1955

EFFECT OF REDUCTION TEMPERATURE ON SYNTHESIS CATALYST
RUNS 63, 64, 65, AND 66

I. INTRODUCTION

Production at the Carthage Hydrocol, Inc., synthetic fuels plant at Brownsville, Texas, had not reached the design yield level, nor had it reached the levels obtained by various pilot units using the same catalyst base stock. It was believed possible that the method of catalyst preparation at Brownsville was at least partially responsible for the poor yields.

For this reason Montebello Laboratory made a run with a hydrocarbon synthesis reactor, evaluating Bethlehem mill scale catalyst promoted, sized, and reduced at Brownsville. All treatment prior to the synthesis operations was the same as at Brownsville.

It was desired to increase the capacity of the catalyst reduction facilities at Brownsville, and one possibility was to use higher reduction temperatures. In order to ascertain the time advantage to be gained by higher temperatures and also to determine any deleterious effects on catalyst activity, Montebello Laboratory made three runs with a synthesis reactor using catalysts reduced at different temperatures.¹

¹ Detailed data on the catalyst reduction rate were presented in TDC 802-45-P.

NOTICE

The information herein contained is not public but belongs to The Texas Company which has provided it solely for an expressly restricted private use. All persons, firms or corporations who receive such information shall be deemed by their act of receiving the same to have agreed to make no duplication or other disclosure or use whatsoever of any or all of such information except such restricted use as is expressly authorized in writing by The Texas Company.

During the latter part of one of the runs, the effect of recycle/fresh feed ratio was investigated by doubling the flow rate of recycle gas. The data were compared with other data from a run in which the recycle rate had been reduced to practically nothing. Extensive investigation of the effect of recycle/fresh feed ratio had not been made at Montebello because the facilities at the commercial plant at Brownsville were not flexible enough, anyhow, to allow much deviation from the design recycle ratio.

This report concerns Runs 63, 64, 65, and 66 made between October 19, 1951, and February 2, 1952.

II. EQUIPMENT AND MATERIALS

Runs 63, 64, 65, and 66 were made in Reactor No. 5S¹, a vessel 12.5 inches in diameter by 30 feet tall with a sparger at the bottom for better inlet gas distribution. For comparison purposes, some data are included from Run 55^a made in Reactor No. 5C. That reactor was the same as No. 5S except that it had a 60-degree cone instead of a sparger at the bottom.

The synthesis gas feed was obtained by using the Texaco Synthesis Gas Generation Process with natural gas and oxygen in a 2-cubic-foot generator. A water-wash tower was used on the synthesis gas in all runs except No. 55.

The catalyst used in Run 63 was Bethlehem mill scale, sized, promoted, and reduced at Brownsville. It was shipped to

¹For description and drawing, see TDC 802-50-P.
^aIbid.

TABLE I

SUMMARY OF DATA AND OPERATING CONDITIONS

Period	Hours on Stream	Average Catalyst Age, Hours	Fresh Feed Rate, ¹ MSCFH	Recycle Ratio	Bed Depth, Feet	Space Velocity v/hr/v	Inlet Pressure psig	Conversion H ₂ + CO Per Cent	Selectivity C ₃ +C ₄ + Per Cent	Activity Index ²	Yield C ₃ + lbs/MCF ³ H ₂ +CO	BPD Brownsville Basis
63-0	0-96	48	15.7	0.97	20.6	1118	414	86.16	79.77	28.73	9.18	7221
-1	96-216	156	16.0	0.96	20.6	1152	413	84.87	78.05	27.84	8.73	6737
-2	216-336	276	16.2	0.99	19.3	1237	406	80.39	76.30	24.90	8.13	6148
64-0	0-106	53	15.2	1.05	18.2	1229	416	84.00	80.18	27.90	8.90	6930
-1	106-194	150	15.7	1.02	18.9	1226	416	82.40	78.56	26.41	8.51	6518
-2	194-290	242	15.5	1.08	19.7	1156	414	80.56	77.44	24.18	8.11	6148
-3	290-386	338	15.6	1.07	19.8	1156	413	79.15	76.29	23.15	7.84	5866
65-0	0-112	56	15.8	1.02	18.3	1281	416	85.10	78.44	29.59	8.80	6836
-1	112-232	172	15.5	1.05	18.8	1214	414	82.77	77.37	26.61	8.43	6446
-2	232-326	279	15.4	1.04	18.7	1222	410	79.05	75.67	23.73	7.80	5871
66-0	0-94	47	16.4	0.95	19.0	1272	404	83.06	80.04	27.50	8.81	6823
-1	94-207	150	15.7	0.97	18.7	1241	403	81.73	77.71	26.01	8.33	6310
-2	207-296	252	15.0	1.03	18.7	1179	403	80.59	75.40	24.45	8.10	6122
-3	296-416	356	14.3	1.07	18.6	1125	401	79.78	75.50	23.28	8.02	6003
-4	416-500	458	15.2	1.05	16.3	1369	398	72.84	74.83	20.94	7.03	5212
-5	500-619	560	15.0	2.09	8.2	2668	404	72.28	79.56	28.79	7.72	5819

¹MSCFH = thousand standard cubic feet per hour, based on 60°F and 14.73 psia.

²Activity Index = $\sqrt{v/h/v} \log \left(\frac{100}{100 - \text{conversion}} \right)$

Montebello in sealed, stainless steel drums and loaded into the reactor in air-tight cans pressured with cylinder nitrogen. The nitrogen was obtained from Air Reduction Company.

The catalysts used in Runs 64, 65, and 66 also were received from Brownsville, but in the unreduced state. They were reduced in the Montebello reactor at, respectively, 730°F, 800°F, and 650°F average bed temperature.¹ Linde cylinder hydrogen was used for reducing the catalyst.

III. OPERATIONS

The average operating conditions are summarized in Table I, opposite.²

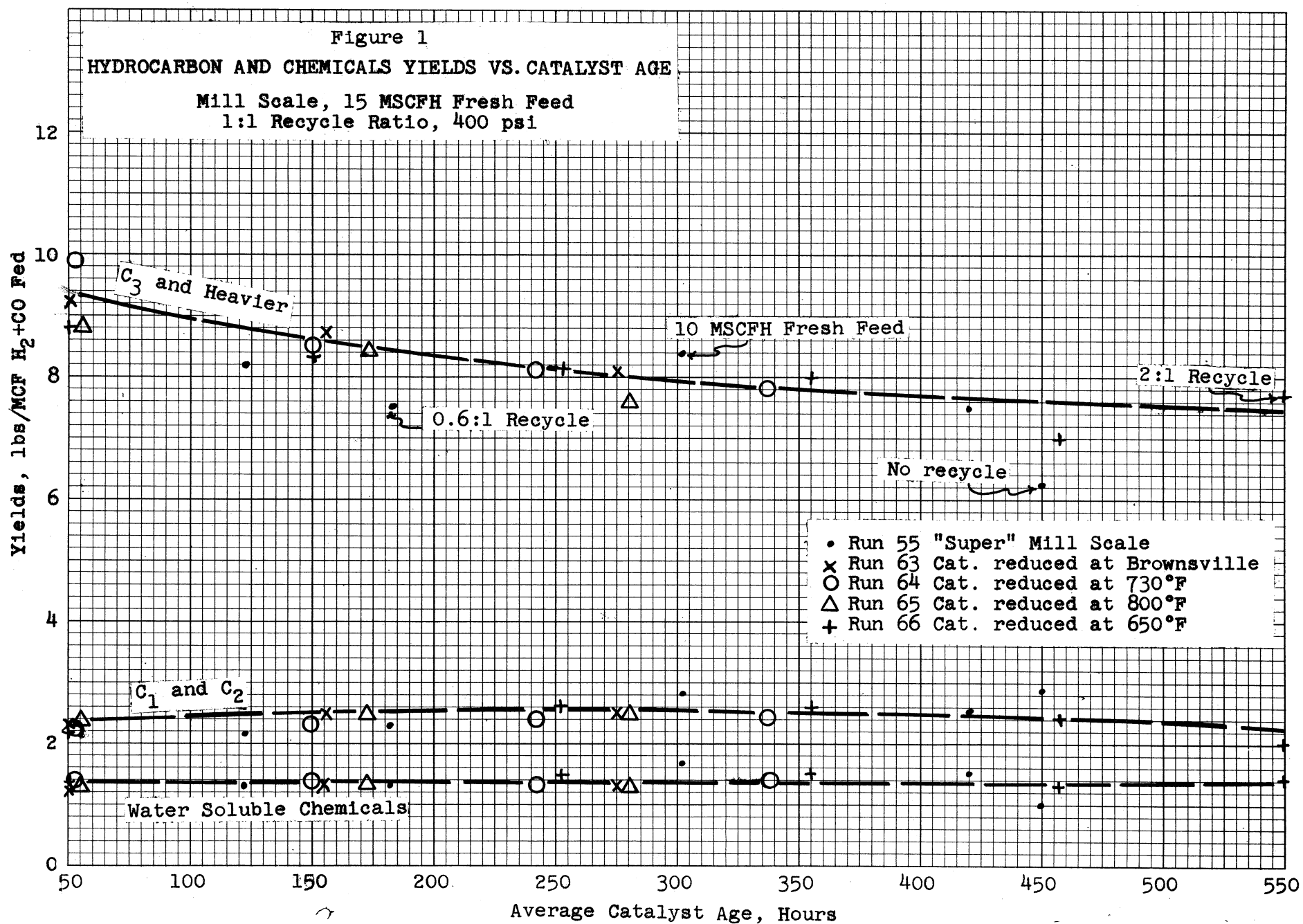
Run 63

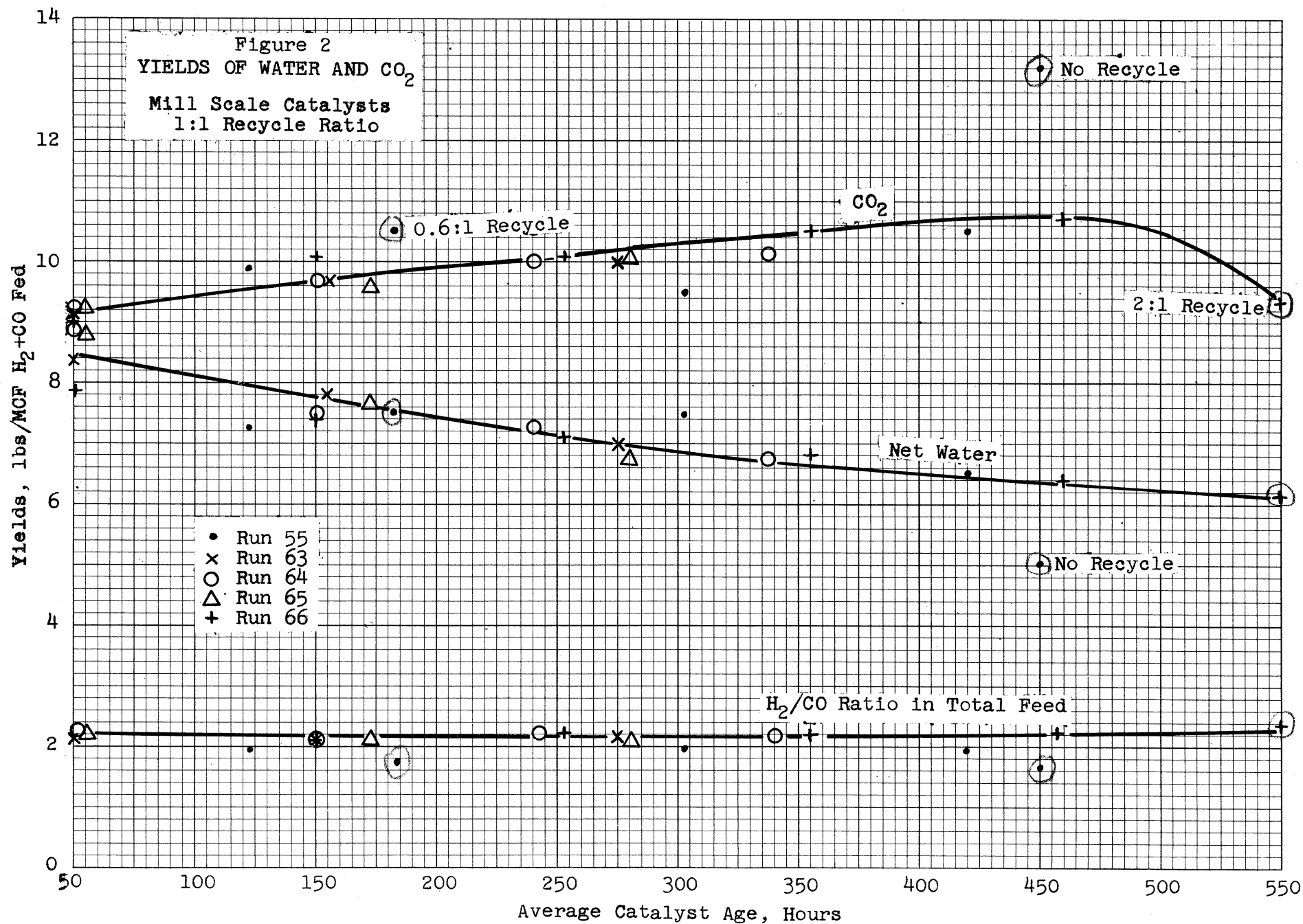
The reduced catalyst for Run 63 was transferred from the stainless steel drums in which it was received from Brownsville to the reactor in 50-pound batches, using sealed cans pressured slightly with cylinder nitrogen. During the loading into the reactor, natural gas was circulated at 500°F and 75 psig. Analysis of the circulated gas at the beginning of the loading showed 0.11 per cent free oxygen. After the loading, the oxygen content was too low to be detected.

After 18 hours the reactor pressure was increased to 120 psi with natural gas and then to 215 psi with hydrogen. The circulated mixture was maintained at approximately 45 per cent hydrogen at 700°F for 24 hours before the fresh feed was cut in. This

¹Reduction data are summarized in Tables IV, V, and VI in the Appendix. Analyses of catalysts are in the Appendix, Table III.

²Further details of the operating conditions are given in the daily average data sheets in the Appendix.





procedure was followed in order to duplicate as much as possible the Brownsville start-up practice.

The initial load of 2000 pounds of catalyst resulted in a 22-foot depth, which gradually declined to 19 feet during the run. The fresh feed rate was 16 MSCFH with a recycle-to-fresh-feed ratio of 1:1.

Runs 64, 65, and 66

These runs were made with catalyst base stock shipped from Brownsville but the reduction was carried out at various temperatures in the Montebello reactor. The general operating conditions were similar to those of Run 63. No make-up catalyst was added during any of the runs.

Between Runs 64 and 65 the line between the feed heater and the reactor was changed from carbon steel to 18-8 stainless steel to allow higher reduction temperatures.

Near the end of the Run 65, period J, 20 pounds of potassium carbonate was added to the approximately 2000 pounds of catalyst in the reactor in an effort to increase the yield.

During the terminal 119 hours of Run 66 the recycle/fresh feed ratio was increased from 1/1 to 2/1.

IV. RESULTS AND DISCUSSION

Effect of Catalyst Reduction Conditions

The yields of hydrocarbons and water-soluble chemicals have been plotted as a function of average catalyst age in Figure 1, page 5. The yields of carbon dioxide and water are shown similarly in Figure 2, opposite. It is evident that the yield structures were the same for Runs 63 through 66 when the only variables were the catalyst reduction conditions previously discussed.

H₂/CO in Effluent
H₂/CO in Combined Feed
H₂/CO in F.F.

5.628
1.654
1.604

TABLE II

EFFECT OF RECYCLE RATIO ON PRODUCT DISTRIBUTION

Run No.	55-2	55-3	55-4	55-5	66-3	66-4	66-5
Periods	L-Q	R-Z	AA-FF	GG-KK	P-T	U-X	Y-CC
Hours	235-379	379-570	570-714	714-834	296-416	416-500	500-619
Recycle Ratio	0.63	0.96	1.01	0.06	1.07	1.05	2.09
Fresh Feed, SCFH	14111	9922	14581	14776	14293	15232	15014
CO ₂ in Total Feed, mol % ^{mol/hr.}	6.23	8.22	11.74	1.57	12.39	11.37	19.78
Space Velocity, v/hr/v	1097	720	1021	1069	1125	1369	2668
Conversion of H ₂ +CO, %	73.03	83.47	76.06	73.64	79.78	72.84	72.28
Selectivity, C ₃ +C ₁ +, %	76.51	75.06	74.86	69.12	75.50	74.83	79.56
Yield of C ₁ +, lbs/MCF H ₂ +CO	9.82	11.19	10.07	8.96	10.63	9.39	9.71
Product Distribution, ^{7.5% in total gas} mol %	7.65	10.67	8.35	8.26	8.48	6.96	6.36
Weight Per Cent of C ₁ +	23.79 3.1%	27.61 2.8%	27.59 3.2%	28.42 3.4%	28.56 3.4%	24.84 3.6%	22.80 3.6%
CH ₄	12.93	12.94	12.86	18.00	13.02	13.87	10.73
C ₂ H ₄	6.32	5.95	6.83	7.64	6.28	6.37	6.06
C ₂ H ₆	4.23	6.05	5.45	5.24	5.20	4.93	3.65
C ₁ +C ₂	23.48	24.94	25.14	30.88	24.50	25.17	20.44
C ₃ H ₆	12.46	12.65	11.93	11.91	11.87	11.49	10.37
C ₃ H ₈	1.90	1.70	1.50	1.23	1.32	1.31	1.09
C ₄ H ₈	8.73	8.97	9.53	8.62	9.13	8.75	9.12
C ₄ H ₁₀	4.80	2.51	2.83	3.20	2.81	2.85	2.85
C ₅ + Recovered Oil	34.81	34.42	34.36	33.17	36.43	36.32	41.46
C ₃ +	62.70	60.25	60.15	58.13	61.56	60.72	64.89
Alcohols	10.67	11.59	11.11	9.22	10.52	10.66	10.37
Acids	3.15	3.22	3.60	1.77	3.42	3.45	4.30
Water Soluble Chemicals	13.82	14.81	14.71	10.99	13.94	14.11	14.67
Yield Basis Brownsville Design Feed Rate, 9488 MCFH H ₂ +CO BPD							
Liquid Hydrocarbons	4336	5051	4480	3814	4988	4301	4854
Alcohols	731	915	772	582	766	688	682
Acids	215	254	250	112	249	223	283
Total Liquid	5282	6220	5502	4508	6003	5212	5819

Effect of Recycle/Fresh Feed Ratio

The data from Run 55 also have been shown in Figures 1 and 2. During this run there were two periods of low recycle ratio, Periods 55-2 with 0.4/1 ratio and Period 55-5 with no recycle gas except the bleed gas through the pressure taps. This flow corresponds to a 0.06/1 ratio. Otherwise the conditions were similar to those of Run 63 through 66, made with a recycle ratio of 1/1 except for Period 66-5, made with 2/1 recycle ratio.

It can be seen in Figure 2 that the H_2/CO ratio in the total feed stream tended to be constant at about 2.2/1. Since the H_2/CO ratio in the fresh feed was fixed at about 1.65 to 1, the composition of recycle gas changed sufficiently, when the recycle ratio was raised from 1/1 to 2/1, to maintain the constant H_2/CO ratio in the total feed. A similar change in the opposite direction took place when the recycle ratio was decreased. Of course, when the recycle flow was practically stopped, then the total feed composition became almost the same as the fresh feed.

The period of lower recycle ratio in Run 55 showed lower yields of C_3 and heavier hydrocarbons, lower yields of water-soluble chemicals, lower yields of water, higher yields of C_1 and C_2 hydrocarbons, and higher yields of CO_2 . The effect of raising the recycle ratio in Run 66 was to increase the yields of C_3 and heavier hydrocarbons (even though the catalyst volume was less). The yields of CO_2 were decreased, but there was only a slight effect on the yield of other products.

Additional data on the effects of recycle ratio are shown in Table II, opposite. The tabulated data shown in more detail the same effects of recycle ratio shown graphically in Figures 1 and 2.

In summary, higher recycle/fresh feed ratio was beneficial in the range of 0.06/1 to 2.0/1. The yields of useful liquid product increased with recycle ratio, and the yields of methane and CO_2 were suppressed. Since the selectivity and conversion decrease with catalyst age, and the CO_2 yields increase, the beneficial effects of increasing the recycle ratio may be more pronounced as the catalyst gets older.

Effect of Addition of Potassium Carbonate

The addition of anhydrous potassium carbonate during period 65-J had no apparent effect on the synthesis reaction.

V. CONCLUSIONS

1. The mill scale catalyst treated and reduced at Browns-ville exhibited no difference from mill scale catalysts prepared at Montebello.
2. Variation of the catalyst reduction temperature in the range of 650°F to 800°F had no effect on the quality of the catalyst.
3. Increasing the recycle/fresh feed ratio in the range of 0.06/1 to 2.0/1 increased the yields of saleable liquid products and suppressed the yields of methane and CO_2 .
4. The addition of anhydrous potassium carbonate during a run had no effect on the synthesis reaction.

REPORT PREPARED BY Signed: W. L. Slater

WLS-EW

REPORT APPROVED BY Signed: duBois Eastman

(WEK-WAMcm)-WJC(2)-RWH-HDM(2)
~~RLSr(2)-duBE(2)~~
 WMS-RP-CEL-GK-Jcw

WORK DONE BY

duBois Eastman
R. A. Beck
W.L. Slater

Director of Research
Supervisor
Chemical Engineer

Clyde Potter
James Elliott
Lawrence Estabrook
Gerald Scott
Willard Herrick
Charles Turbyfill
Lowell Bell
Roy Gothard
John Klein
Harvey Rupp
James Stanchfield
John Hughes
Cecil Mitchell
Ernest Brown

Operator
Operator
Operator
Operator
Operator
Operator
Assistant Operator
Assistant Operator
Assistant Operator
Assistant Operator
Assistant Operator
Assistant Operator
Assistant Operator

REPORT WRITTEN BY

W. L. Slater

Chemical Engineer

(WEK-WAMcM)-WJC(2)-RWH-HDM(2)-RLSr(2)-duBE(2)

WMS
RP
CEL
GK
Jcw

VI. APPENDIX

INDEX TO APPENDIX

<u>Table No.</u>		<u>Page</u>
III	ANALYSES OF CATALYSTS	14
IV	MONTEBELLO RUN 64 REDUCTION	15
V	MONTEBELLO RUN 65 REDUCTION	16
VI	MONTEBELLO RUN 66 REDUCTION	17
	RUN 63 AVERAGE DATA SHEETS	18
	RUN 64 AVERAGE DATA SHEETS	34
	RUN 65 AVERAGE DATA SHEETS	62
	RUN 66 AVERAGE DATA SHEETS	85

TABLE III
ANALYSES OF CATALYSTS

Run	63 S.D.*	64, 65, 66 Raw*	64 A *	64 S.D.**	65 Red.*	65 A *	65 S.D.*	66 A	66 C	66 D *	66 S.D.*
Screen Analysis, Weight Per Cent On U.S. No.											
40 (420 microns)	2.0	0.6	1.2	0.4	1.0			0.8	1.0	0.5	1.0
100 (150 microns)	48.3	45.3	53.4		52.7			63.8	68.4	58.1	70.6
150 (105 microns)	23.4	16.9	19.0	20.3	19.2			21.0	19.2	21.4	25.2
200 (74 microns)	14.8	12.1	11.0	71.5	12.7			9.6	7.8	13.0	2.0
250 (62 microns)	5.1	3.4	5.4	2.2	1.4			4.0	2.6	2.6	0.4
325 (44 microns)	4.3	10.4	7.6	5.7	8.1			0.4	0.6	3.8	0.2
Through 325	2.1	11.3	2.4	2.0	4.9			0.4	0.4	0.6	0.6
50 Per Cent Point, microns	150	140	150	95	150			180	190	170	190
Bulk Density, lbs/cu. ft.											
Aerated	151		157	131	139	139	133	146	140		120
Settled	156		159	132	140	140	135	148	141		121
Compacted	172		187	159	174	186	160	180	174		128
Specific Gravity	4.93		5.90	3.98	6.44	5.35	3.74	4.98	3.66		4.82
Per Cent Iron				78.2	97.7		77.6				74.4
Per Cent Oil Soluble in CCl ₄	1.8			0.15							
Per Cent Carbon after extraction with CCl ₄				11.2							
Per Cent K ₂ O basis Fe					1.17						

*S.D.=catalyst sampled after reactor shutdown; Raw = catalyst before reduction;
Red.:catalyst sampled after reduction but before cutting in feed gas.

TABLE IV

MONTEBELLO RUN 64 REDUCTION
BETHLEHEM MILL SCALE

Loaded 2200#

Hours above 600°F.	Water Production					Temperature - °F			Recycle		Total H ₂ m/hr.	H ₂ Conv. %	Carry-over		H ₂ Flow		
	lbs.		% of Total	lbs./hr.	m/hr.	Heater	Meter		psig.	lbs.			Total	Recycle SCFH	Bleed SCFH	Total SCFH	
	Spot	Total					Bed	Run									√h
1	16	16	2.6	16	0.888		628	90	5.8	251	52.35	0.848	18	18	18122	1746	19868
4	14½	30½	4.9	4.83	0.268		668	93	6.23	226	54.77	0.489	20½	38½	19007	1780	20787
7	35½	66	10.6	11.83	0.657		689	91	5.93	226	52.67	1.247	43½	82	18289	1698	19987
9	33	99	15.9	16.5	0.916		702	88	5.60	236	50.70	1.807	34	116	17602	1637	19239
11	49	148	23.8	24.5	1.360		719	88	5.75	231	52.38	2.597	32	148	18177	1703	19880
13	53	201	32.3	26.5	1.471		714	96	5.95	229	49.96	2.944	22½	170½	17254	1705	18959
15	36½	237½	38.1	18.25	1.013		718	100	5.65	226	48.67	2.081	13½	184	16866	1604	18470
17	55½	293	47.0	27.75	1.540		730	96	5.65	230	48.85	3.153	12½	196½	16908	1630	18538
19	48½	341½	54.8	24.25	1.346		733	90	5.60	225	48.28	2.788	6½	203	16725	1598	18323
21	59	400½	64.3	29.5	1.637		741	90	5.55	228	49.92	3.279	8	211	17344	1599	18943
23	48½	449	72.1	24.25	1.346		747	92	5.70	229	48.78	2.759	8	219	16870	1640	18511
25	46	495	79.5	23.0	1.277		750	90	5.60	226	48.44	2.636	7½	226½	16779	1603	18382
27	42	537	86.2	21.0	1.166		752	88	5.60	226	48.54	2.402	6	232½	16814	1606	18420
29	35	572	91.8	17.5	0.971		756	88	5.60	216	47.60	2.040	5	237½	16844	1575	18063
31	26½	598½	96.1	13.25	0.735		768	88	5.75	225	49.09	1.497	5½	243	16986	1644	18630
33	6	604½	97.0	3.0	0.167		788	87	5.50	229	48.82	0.341	5	248	16937	1589	18528
35	11½	616	98.9	5.75	0.319		731	94	5.95	226	51.23	0.623	5½	253½	17744	1698	19442
39	2	618	99.2	0.50	0.028		785	93	6.03	234	52.18	0.053	8½	262	18044	1755	19800
46	1½	619½	99.5	0.21	0.012		778	91	7.39	230	51.14	0.023	11	273	17232	2175	19408
57	3½	623		0.32	0.018		800	88	7.4	230	51.14	0.035			17232	2175	19408
Average 7-27					1.3072		730			228.7	49.452	2.643					

$$\text{Flow Rate} = \frac{(49.45)(379.5)}{3600} \left(\frac{14.7}{244.7} \right) \left(\frac{1191}{520} \right) = 0.7172 \text{ CFS} \quad V = 1.08 \text{ ft./sec.}$$

$$\text{Average Inventory} = 2200\# @ 160\#/\text{CF} = 13.75 \text{ CF} @ 67\% V = 9.213 \text{ CF}$$

$$t = 9.213/0.7172 = 12.84 \text{ sec.}$$

TABLE V

MONTEBELLO RUN 65 REDUCTION
BETHLEHEM MILL SCALE

Loaded 2445#

Hours above 600°F	Water Production					Temperature - °F			Recycle			Bleed		Total Feed		Hydrogen	Carry-over		Density	Depth
	lbs. Spot	Total	% of Total	lbs/hr	m/hr	Heater	Bed	Meter Run	ψh	Press. psig.	Rate SCFH	ψh	Rate SCFH	SCFH	m/hr	Conv. %	lbs. Spot	Total	#/CF	Ft.
3	56	56	9.1	18.67	1.036	1140	739	62	4.01	235	19032	6.2	1860	20892	55.05	1.88	91	91	167	20.9
5	82	138	22.5	41.0	2.276	1140	809	60	3.94	236	18754	5.3	1595	20349	53.62	4.14	68	159	165	19.9
7	92	230	37.4	46.0	2.553	1090	815	61	3.85	231	18122	5.0	1488	19610	51.67	4.94	43	202		
9	86½	316½	51.5	43.25	2.401	1095	802	59	3.95	223	18333	5.0	1471	19804	52.18	4.60	29	231	165	17.8
11	75	391½	63.7	37.5	2.081	1085	800	54	3.75	224	17523	4.9	1449	18972	49.99	4.17	17	248	162	17.4
7AM 12	52	443½	72.2	52.0	2.886	1080	800	53	3.63	225	17012	4.9	1450	18462	48.65	5.92	10	258		
13	24½	468	76.2	24.5	1.360	1085	784	55	3.55	220	16432	6.5	1925	18357	48.37	2.81	4½	262½	161	16.6
14	37½	505½	82.3	37.5	2.081	1095	786	62	3.55	215	16152	6.5	1870	18022	47.49	4.40	5	267½	156	16.8
15	24½	530	86.2	24.5	1.360	1085	792	65	3.65	225	16908	6.5	1910	18818	49.59	2.74	4	271½	155	16.6
16	28½	558½	90.9	28.5	1.582	1040	800	66	4.00	225	18530	6.5	1905	20435	53.85	2.94	4½	276	160	15.8
17	26	584½	95.1	26.0	1.443	1020	794	70	4.00	225	18442	6.0	1750	20192	53.21	2.72	6½	282½	159	15.7
18	18½	603	98.1	18.5		1005	794	72	4.30	220		6.2					6½	289	158	15.5
19	5	608	98.9	5.0		934	793	75		226		6.2					4	293	159	15.4
20	2	610	99.3	2.0		950	790	74		230		6.4					3	296	160	15.2
23	4½	614½		1.5													7½	303½	164	14.8
Average 3-15					2.125		799			225					50.195	4.23			161	17.6

$$\text{Flow Rate} = \frac{(50.195)(379.5)}{3600} \left(\frac{14.7}{229.7} \right) \left(\frac{1259}{520} \right) = 0.820 \text{ CFS} = 1.24 \text{ ft/sec.}$$

$$\text{Average Inventory} = 2445$$

$$\frac{1590}{2017} / 160 = 12.60 \text{ CF @ } 67\% \text{ V} = 8.442 / 0.820 = 10.30 \text{ sec.}$$

TABLE VI

MONTEBELLO RUN 66 REDUCTION
BETHLEHEM MILL SCALE

Loaded 2883#

Hours above 600°F.	Water Production					Temperature - °F.			Recycle		Bleed		Total Feed		Hydrogen Conv.	Carry-over		
	Spot	Total	% of Total	lbs./hr.	m/hr.	Heater	Bed	Meter Run	Yh	Press. psig.	Rate SCFH	Yh	Rate SCFH	SCFH	m/hr.	%	Spot	Total
4	27	27	4.75	6.75		800	633	54	6.0	226		8.5						
6	12	39	6.86	6.0		790	649	50	5.9	238		7.9					75	75
8	20	59	10.38	10.0		795	654	50	5.9	245		7.05					61	136
10	29	88	15.5	14.5		790	657	46	5.9	232		6.7					58½	194½
12	33½	121½	21.4	16.65		788	657	45	5.95	235		6.8					34	228½
14	34	155½	27.4	17.0		782	653	45	5.98	235		6.95					26	254½
16	38½	194	34.1	19.25		786	656	46	6.0	235		7.2					24	278½
18	31½	225½	39.7	15.75		780	652	52	6.0	232		7.25					18½	297
19	28	253½	44.6	28.0		780	653	65	6.0	230		7.2					16½	313½
21	33	286½	50.4	16.5		780	653	72	6.0	232		7.3					12½	326
23	43½	330	58.0	21.75		785	652	73	6.0	222		6.7					11½	337½
25	36	366	64.4	18.0		751	650	64	5.95	232		6.7					10	347½
27	31	397	69.8	15.5		750	630	60	5.95	240		6.9					6½	354
29	30	427	75.1	15.0		761	647	53	5.98	235		6.5					5½	359½
31	29	456	80.2	14.5		760	649	49	5.98	230		6.8					5	364½
33	27	483	85.0	18.5		760	652	48	5.98	235		6.8					6	370½
35	25	508	89.4	12.5		760	654	45	5.9	225		6.7					5½	376
37	21	529	93.0	10.5		760	657	45	6.0	235		6.5					6	382
39	15	544	95.7	7.5		755	659	42	5.95	227		6.0					4	386
41	11½	555½	97.7	5.75		750	655	45	6.05	235		6.5					5½	391½
43	7	562½	98.9	3.5		752	657	56	6.08	231		6.7					4½	396
45	4	566½	99.6	2.0		752	663	69	6.02	225		6.7					4	400
47	2	568½		1.0		740	653	72	6.05	225		6.5					3	403
Average 8-33 25 hours	424			16.96	0.9413		651	55	5.97	233	28472	6.9	2080	30555	80.51	1.17		

Recycle Flow = (79.31)(3.7854)(5.97)(V250)(1.0048) = 28472

Bleed Flow = (5.02)(3.7854)(6.9)(15.81)(1.0048) = 2083

$$\frac{(30555)}{3600} \left(\frac{14.7}{250} \right) \left(\frac{1111}{520} \right) = 1.066 \text{ Cu. Ft./sec.} = 1.61 \text{ ft./sec.}$$

Average Inventory = 2420# @160#/CF = 15.13 Cu. Ft. @67% Void = 10.14 CF Void

 $t = 10.14/1.066 = 9.51 \text{ sec.}$

[illegible]

Form ML-11

$$R/NCM = 16.91 \times \# / MCF$$
$$*9488 \text{ MCFH } H_2 + CO, \text{ Bbl/Day} = 5421.6 \times \text{gal/MCF}$$

RUN NO. 63-1(F-J)
HOURS 96-216
CATALYST Bethlehem MS

THE TEXAS COMPANY — MONTEBELLO LABORATORY
YIELD CALCULATIONS

[illegible]

Form ML-11

$$g/NCM = 16.91 \times \delta / MC$$
99488 MCFH $H_2 + CO$ Bbl/Day 1421.6 X gal/MCF

RUN NO. 63-2(K-0)
HOURS 216-336
CATALYST Bethlehem MS

THE TEXAS COMPANY — MONTEBELLO LABORATORY
YIELD CALCULATIONS

[illegible]

Form M-11

1993年 4月 20日 / 星期三

[illegible]

$$g/NCM = 16.91 \times \# / MCF \quad 89488 \text{ MCFH } H_2 + CO, \text{ Bbl/Day} = 5421.6 \times \text{gal} / MCF$$

OPERATING CONDITIONS				PRODUCT TESTS			CATALYST DATA						
PRESSURES PSIG		RATES SCFH		OIL	WATER	INVENTORY DATA		PARTICLE SIZE					
Oxygen	439	Fresh Feed	15,272	*API	50.7	10.8	In Reactor at Start of Period			Screen Analysis			Sedimentation
Natural Gas	435	Recycle	15,102	Neut. No.	39.7	32.5	Fresh Catalyst Added	Mesh	Micros	%	Micros	%	
Generator Outlet	417	Combined Feed	30,374	Sap. No.	46.8	36.7	Total	On 40	419+		80+		
Reactor Inlet	415	Wet Gas—Measured	3,815	Hydrox. No.			Catalyst Recovered	58	100	150	40—80		
Condenser Inlet		Adjusted	4,729	Bromine No.	75		In Reactor at End of Period	150	105		20—40		
Product Accumulator	360	Loss	914	Poor °F.				200	74		10—20		
				Chemicals, % by K ₂ CO ₃	7.5		REACTOR d-p. Inches H ₂ O	250	62		0—20		
							No. Height	325	44				
TEMPERATURES —°F.		Recycle/Fresh Feed	0.99				0 0-21 3/8	-	<325				
Oxygen	419	Inlet Velocity—ft./sec.	0.94				1 21 5/8-52 3/4	75	CATALYST				
Natural Gas	761	Fresh Feed Rate—SCFH.	14797	HEMPEL DIST. %		*API	2 52 5/4-84	76	Bulk Density, Lbs./Cu.Ft.				
Generator		per Cu.Ft. Dense Bed	1039	205 °F.			3 84-115 3/8	83	Aerated				
Quench Accumulator	154	per Lb. Catalyst	6.75	400	76	55.4	4 115 3/8-353 1/8	375	Settled				
Reactor Inlet	381	per Sq. Ft.	22405	400-550	14	34.7	Total	609	Compacted				
Condenser Inlet	578			550+	10				Particle Density, gm./cc.				
Product Accumulator	89	Heat Transfer Calculations					CALCULATED FROM dp		NH ₃ Value, ml./gm.				
Catalyst No.	Height	Steam Rate = 221 #/hr.	A. S. T. M. DIST. ON				Density, Lbs./Cu.Ft.	154	N ₂ Surface, m ² /gm.				
1	0'0"	@707 psia & 505°F	Naphtha °F.				Inventory, Lbs.	2191					
2	0'9"	= 1201 Btu/#	IRP	96			Bed Depth, Ft.	21.56	CHEMICAL ANALYSIS				
3	1'9"	Water in @60° P = 28 Btu/#	10%	137			Vol. Cu. Ft.	14.23	Fe				
4	4'5"	= 1173 Btu	50%	225					C				
5	7'10"	(1173)(221) = 259,233 Btu/hr.	90%	350					O				
6	12'3"	Ave. Bed Temp. = 653°F	EP	396					H				
7	17'5"	dT = 653-505 = 148°F	Rec.	96					K ₂ O, W+, % basis Fe				
8	20'0"	Tube Area = 37.8 sq. ft.							X-Ray Analysis—				
9	22'7"	K = (259,233 / (37.8 * 148)) = 46.3 Btu/°F/sq. ft.							Fe ₂ O ₃				
10	25'2"								Fe ₂ O ₄				
11	26'11"								Fe				

[illegible]

Form ML-21 **Included in Reactor Effluent Total g/NCM = 16.91 X #/MCF *9488 MCFH H₂ + CO, Bbl/Day = 3421.6 X gal/MCF

GAS ANALYSES				GENERATOR BALANCE										WEIGHT BALANCE			
HOUR	LOAD	AVERAGE	M/HR	C	H	O		Mol %	M/HR	C	H	O	#/hr Measured	At Wt. Balance			
FRESH FEED																	
CO ₂ 2.010	36.89	36.89	15.343	15.343		15.343	CO ₂ 2.010	0.18	10.237			20.520	WET GAS	251.41	316.43		
H ₂ 2.010							H ₂ 2.010	1.40	0.183	0.183		0.366	OIL	66.92	66.92		
CO ₂ 2.010	60.25	60.25	25.055		50.130		N ₂ 2.010	1.25	0.163				WATER	141.83	141.83		
CO ₂ 2.010	2.08	2.08	0.865	0.865		1.730	CH ₄ 2.010	82.63	10.775	10.775	43.100		TOTAL	460.16	525.18		
N ₂ 2.010	0.31	0.31	0.129				C ₂ H ₆ 2.010	6.73	0.378	1.756	5.268		FRESH FEED	525.18			
CH ₄ 1.242	0.48	0.48	0.200	0.200	0.800		C ₂ H ₄ 2.010	5.40	0.704	2.112	5.632		WEIGHT BALANCE	87.62			
		M. W	12.62399				C ₂ H ₂ 2.010	1.67	0.218	0.872	2.180						
		H ₂ O 2.010			7.020	3.510	C ₂ H ₂ 2.010	0.74	0.097	0.485	1.164		WET GAS FACTOR	1258621			
				16.408	57.950	20.683	W. =	20.1885614					INDICATED LOSS - S C F H	1028			
		BALANCE		101.39	101.06	98.55	TOTAL			16.183	57.344	20.886					
WET GAS			GAS FLOW RATES										LIQUID PRODUCT RATES				Base 11 hours
CO ₂ 2.010	6.81	6.81		V.R	PRESSURE	TEMP.	M. W.	S. C. F. H.	M/HR							#	#/GAL HR
H ₂ 2.010					414	80	2299252										
CO ₂ 2.010	37.44	37.44	FRESH FEED														
N ₂ 2.010	31.19	79.31	6.470	20.705	0.9813	1.514	15.768	41.602		OIL	711-3/4	378.77	71	0.9956	377.10	50.7	2436.33
CH ₄ 1.642	11.18	11.18	159.44	5.750	4.025	0.9874	3.977	10.480			516"	282.57	71	1.0015	293.01	6.466	1894.60
H ₂ 2.010	2.46				115	129	1.0985				214-3/4	127.74	72	0.9941	126.99		821.12
C ₂ H ₆ 2.010	1.70	1.70	79.31	8.530	20.681	0.9404	1.0985	14.453	38.084		1108"	99.28	72	0.9941	97.70		631.73
C ₂ H ₄ 2.010	2.89																
C ₂ H ₂ 2.010	0.26	0.26	5.02	9.220	20.681	1.0000	1.0985	1.051	2.769								
C ₂ H ₂ 2.010	2.17	2.17	NATURAL GAS		437	199	1435978										
H ₂ 2.010	0.76	0.76	28.43	7.700	21.253	0.8883	1.1975	4.949	13.041								
CO ₂ 2.010	1.01	1.01	OXYGEN		440	85											
C ₂ H ₆ 2.010	0.31	0.31	27.07	6.890	21.324	0.9758	3.885	10.237									
C ₂ H ₄ 2.010	0.31	0.31	STEAM														
		M. W	23.98948	215.7	3.540	0.3004	229	#/hr.									

CATALYST Mill Scale Red.

CATALYST Mill Scale Red.

at Brownsville

FRESH FEED										WET GAS				RECYCLE	COMBINED RECYCLE	EFFLUENT		NET CHANGE		YIELD BASIS H ₂ +CO FED										
		%	m/hr	#/hr	%	At Wt. Balance														CONDENSATE										
		%	m/hr	#/hr	%	m/hr		#/hr		m/hr		#/hr		m/hr		#/hr		#/MCF		#/gal		gal/MCF		YIELDS		BASIS		BROWNVILLE DESIGN FEED RATE		
CO	28.310	37.043	15.338	429.61	6.587	0.834	23.36	2.535	17.873	3.369	-14.504	-406.25																		
H ₂	28.310	59.197	24.512	49.42	35.937	4.695	9.47	14.264	38.776	18.959	-19.817	-59.95												400 EP	79	7.973	98.0	7.716		
CH ₄	28.310	2.373	0.983	43.26	32.304	4.221	185.77	12.023	13.806	17.044	5.238	142.51	9.423										400-550	10	0.997	91.4	0.911			
N ₂	28.310	0.020	0.091	2.55	1.513	0.198	5.55	0.601	0.692	0.799													550 +	11	1.096	114.6	1.256			
CH ₃	28.310	1.167	0.483	7.75	10.923	1.427	22.89	4.336	4.619	5.763	0.944	15.14	1.001																	
C ₂ H ₆	28.310				2.633	0.344	9.65	1.045	1.045	1.589	0.344	9.65	0.638																	
C ₃ H ₈	28.310				1.937	0.253	7.61	0.769	0.769	1.022	0.253	7.61	0.503																	
C ₄ + C ₅	28.310																													
C ₆ H ₁₄	28.310																													
C ₇ H ₁₆	28.310																													
C ₈ H ₁₈	28.310																													
C ₉ H ₂₀	28.310																													
C ₁₀ H ₂₂	28.310																													
C ₁₁ H ₂₄	28.310																													
C ₁₂ H ₂₆	28.310																													
C ₁₃ H ₂₈	28.310																													
C ₁₄ H ₃₀	28.310																													
C ₁₅ H ₃₂	28.310																													

Form ML-21

**Included in Reactor Effluent Total

$$f/NCM = 16.91 \times f/MCF$$
$$0.9488 \text{ MCFH H}_2 + \text{CO, Bbl/D}_{\text{AY}} = 5421.6 \times \text{gal/MCF}$$

OPERATING CONDITIONS				PRODUCT TESTS			CATALYST DATA				
PRESSURES PSIG		RATES SCFH		OIL		WATER		INVENTORY DATA		PARTICLE SIZE	
Oxygen	439	Fresh Feed	15,714	*API	52.2	10.7	In Reactor at Start of Period		Screen Analysis Sedimentation		
Natural Gas	442	Recycle	15,064	Neut. No.	40.0	31.9	Fresh Catalyst Added		Mesh	Microns %	
Generator Outlet	417	Combined Feed	30,778	Sap. No.	47.7	35.0	Total		On 40 419+	80+	
Reactor Inlet	412	Wet Gas—Measured	4,045	Hydrox. No.			Catalyst Recovered		33	100 150 40—80	
Condenser Inlet		Adjusted	4,958	Bromine No.	82		In Reactor at End of Period		150 105	20—40	
Product Accumulator	361	Loss	913	Pour °F.					200 74	10—20	
				Chemicals, % by K_2CO_3		10.0	REACTOR d-p. Inches H_2O		250 62	0—20	
							No. Height		325 44		
TEMPERATURES—°F.		Recycle/Fresh Feed	0.96				0 See Period A		-	<325	
Oxygen	478	Inlet Velocity—ft./sec.	0.96				1		76	CATALYST	
Natural Gas	747	Fresh Feed Rate—SCFH	15123	HEMPEL DIST. %		0 API	2		75	Bulk Density, Lbs./Cu.Ft.	
Generator	2068	per Cu.Ft. Dense Bed	1085	205 °F.			3		81	Aerated	
Quench Accumulator	151	per Lb. Catalyst	7.09	400		78	55.2		4	360 Settled	
Reactor Inlet	357	per Sq. Ft.	22914	400-550		10	30.2		Total	592 Compacted	
Condenser Inlet	577			550+		12				Particle Density, gm./cc.	
Product Accumulator	92	Heat Transfer Calculations					CALCULATED FROM dp			NH_3 Value, ml./gm.	
Catalyst No.	Height	Steam Rate = 237 #/hr.		A. S. T. M. DIST. ON			Density, Lbs./Cu.Ft.		153	N_2 Surface, m ² /gm.	
1	See Period A	@705 psia & 506°F =		Naphtha °F.			Inventory, Lbs.		2133		
2	658	1201 Btu/#		IRP		107	Bed Depth, Ft.		21,12	CHEMICAL ANALYSIS	
3	651	Water in @63°F = 31 Btu/#		10%		134	Vol., Cu. Ft.		13.94	Fe	
4	650	Net Heat Trans./# steam =		50%		221				C	
5	664	1170 Btu		90%		350				O	
6	662	(1170)(237) = 277,290 Btu		EP		411				H	
7	650	Ave. Bed Temp. = 656°F		Rec.						K_2O W +, % basis Fe	
8	641	dT = 655-506 = 149°F								X-Ray Analysis—	
9	634	Tube Area = 37.6 sq. ft.								Fe_2O_3	
10	629	K = (37.6)(149) = 49.5 Btu/°F.sq.ft.								Fe_2O_3	
11										Fe	

GAS ANALYSES					GENERATOR BALANCE										WEIGHT BALANCE									
HOUR	1400	2200	0600	AVERAGE	M/HR	C	H	O		Mol %	M/Hr	C	H	O		#/hr Measured	At Wt. Balance							
FRESH FEED																								
CO ₂ 18-010	37.02	36.15	37.96	37.043	15.338	15.338		15.338	CO ₂ 18-010	0.23	10.364			20.788		WET GAS	263.51							
H ₂ 20-016	60.08	58.38	59.13	59.197	24.612		49.024		N ₂ 18-016	0.42	0.186	0.186		0.372		OIL	63.91							
CO ₂ 24-010	2.05	2.41	2.66	2.373	0.983	0.983		1.966	CH ₄ 18-016	83.32	10.914	43.656				WATER	145.68							
N ₂ 20-016	0.19	0.27	0.20	0.220	0.091				C ₂ H ₆ 20-016	7.13	0.934	1.868	5.804			TOTAL	473.10							
CH ₄ 18-016	0.66	2.79	0.05	1.167	0.483	0.483	1.932		C ₂ H ₄ 20-016	5.29	0.693	2.079	5.544			FRESH FEED	532.59							
			M.O.E.	12.862388					C ₂ H ₂ 20-016	1.58	0.204	0.816	2.040			WEIGHT BALANCE	89.83							
			H ₂ O 19-016					6.926	3.463	C ₂ H ₂ 20-016	0.63	0.083	0.415	0.995			WET GAS FACTOR	1225759						
						16.804	57.882	20.767	MM =	20.0202							INDICATED LOSS - S.C.F.H.	913						
			BALANCE			103.23	100.07	99.80	TOTAL			16.278	57.840	20.788										
WET GAS					GAS FLOW RATES										LIQUID PRODUCT RATES									
CO ₂ 18-010	6.31	6.17	6.68	6.387	V-R	PRESSURE	TEMP.	M.W.	S.C.F.H.	M/HR	HOUR	GAGE	GAL	"F	FACTOR	GAL AT 67°	# APP #GAL	#	Base 19 hours # HR GAL HR					
H ₂ 20-016	36.55	35.32	35.44	35.937	FRESH FEED	418.3	72	2250753				OIL	6'0"	320.94	54	1.0030	321.90	52.2	2064.34					
CH ₄ 18-016	29.71	33.33	33.87	32.304	79.31	6.464	20.664	0.8887	1.5003	15.714	41.407		2'6"	135.80	68	0.9961	135.27	6.413	867.49					
N ₂ 20-016	1.42	1.63	1.49	1.513	WET GAS	1.50	66	1171044																
CH ₄ 18-016	12.40	10.25	10.12	10.923	158.44	5.895	4.025	0.9943	1.0821	4.045	10.659													
H ₂ 20-016	2.79	2.62	2.59	2.633	RECYCLE	411.6	127																	
C ₂ H ₆ 20-016	1.96	1.93	1.92	1.937	79.31	8.482	20.647	0.9412	1.0821	14.146	37.275													
C ₂ H ₄ 20-016	3.45	3.12	3.25	3.273	BLEED																			
C ₂ H ₂ 20-016	0.41	0.28	0.37	0.353	5.02	8.182	20.647	1.0000	1.0821	918	2.419		WATER	7'3"	384.23	74	0.99846	383.64	10.7	3179.22				
C ₂ H ₆ 20-016	2.49	2.30	2.17	2.320	NATURAL GAS	442.3	201	1446052						1'11"	102.69	73	0.99858	102.74	8.287	851.41				
C ₂ H ₄ 20-016	0.72	0.89	0.86	0.787	28.43	7.668	21.378	0.8770	1.2025	4.971	13.099			2'6"	133.50	68	0.99942	133.42		1105.65				
C ₂ H ₂ 20-016	1.18	1.12	0.98	1.093	OXYGEN	458.7	93							1'6"	80.37	68	0.99920	80.31		665.53				
C ₂ H ₆ 20-016	0.26	0.25	0.16	0.223	27.07	6.909	21.893	0.9877		5.933	10.364													
C ₂ H ₄ 20-016	0.35	0.39	0.30	0.347	38.0																			
			M.W.	34.70135	215.7	3.759	0.93017		237.40/-															

THICKENED	gal/hr	TREATING	gal/hr
-----------	--------	----------	--------

GAS ANALYSES					GENERATOR BALANCE										WEIGHT BALANCE					
HOUR	1400	2200	0600	AVERAGE	M/Hr	C	H	O		Mol %	M/hr	C	H	O	#/hr Measured	At Wt. Balance				
FRESH FEED																				
CO ₂ 29.00	36.94	37.02	37.17	37.043	15.511	15.511		15.511		O ₂ 20.00	0.21	10.532 0.028			21.100	WET GAS 280.63 319.00				
H ₂ 2.64										CO ₂ 44.30	1.44	0.191	0.191		0.382	OIL 64.52 64.52				
N ₂ 44.30	60.19	60.37	60.15	60.237	25.224		50.448			N ₂ 20.00	1.79	0.237				WATER 148.23 148.23				
CH ₄ 16.44	2.27	2.29	2.24	2.500	0.953	0.953		1.926		CH ₄ 16.44	82.53	10.918	10.918	45.672		TOTAL 493.58 531.75				
	0.25	0.21	0.27	0.243	0.102					C ₂ H ₆ 30.24	6.80	0.902	1.804	5.412		FRESH FEED 531.75				
CH ₄ 16.44	0.35	0.11	0.07	0.177	0.074	0.074	0.295			C ₂ H ₆ 14.07	5.28	0.700	2.100	5.600		WEIGHT BALANCE 92.62				
				M.W.	16.998825					C ₃ H ₈ 0.820	1.55	0.206	0.824	2.060						
				H ₂ O 15.00						CH ₄ 72.164	0.60	0.080	0.400	0.960		WET GAS FACTOR 1135918				
							7.525	3.763								INDICATED LOSS—S.C.F.H. 596				
						16.548	58.269	21.800		WT =	20.116332									
				BALANCE		101.92	100.98	98.69		THL		16.237	57.704	21.482						
WET GAS					GAS FLOW RATES								LIQUID PRODUCT RATES							
CO ₂ 29.00	6.49	6.29	6.82	6.530	✓T	PRESSURE	TEMP.	M.W.	S.C.F.H.	M/Hr		HOUR	GAGE	GAL	°F	FACTOR GAL AT 66 °F	#	#/HR GAL HR		
H ₂ 2.16	36.04	35.26	37.53	36.277	FRESH FEED		415	70°	28797938			OIL	7'13"	386.41	65	0.9975	385.44	52.8	2453.73	
CO ₂ 29.00	32.01	32.21	27.33	30.750	79.31	6.463	20.729	0.9905	1.5099	15.891	41.874		6'10"	320.24	64	1.0030	321.80	6.392	2057.58	
N ₂ 44.30	1.49	1.29	1.78	1.520	WET GAS		1.51	64	1191989				4'4"	231.47	53	1.0055	232.28		1484.73	
CH ₄ 16.44	11.65	11.04	11.61	11.800	168.44	6.325	4.026	0.9962	1.0918	4.388	11.563		1'13"	57.39	72	0.9941	57.05		364.66	
H ₂ 2.64	2.65	2.73	2.72	2.687	RECYCLE		415.3	118								+3.48	+22.25	64.52		
C ₂ H ₆ 30.24	1.99	2.15	2.38	2.173	79.31	8.479	20.736	0.9485	1.0918	14.440	38.050					242.25	1549.47	10.09		
C ₂ H ₆ 14.07	3.57	3.57	3.93	3.690	BLEED															
C ₃ H ₈ 0.820	0.61	0.27	0.28	0.328	5.02	8.900	20.736	1.0000	1.0918	1.000	2.635		WATER 7'11"	401.69	76	0.99819	400.96	10.8	3320.75	
CH ₄ 16.44	2.12	2.30	2.70	2.373	NATURAL GAS		445	191	1459129					2'6"	135.50	66	0.99948	135.48	8.282	1104.98
C ₂ H ₆ 30.24	0.55	0.65	0.95	0.720	28.43	7.700	21.441	0.8938	1.1996	5.033	13.282			4'56"	239.01	66	0.99948	237.87		1970.04
C ₂ H ₆ 14.07	0.79	1.00	1.17	0.987	OXYGEN		442.6	70°						1'56"	75.97	74	0.99846	75.85		628.10 149.82
CH ₄ 16.44	0.18	0.26	0.29	0.243	27.07	6.963	21.385	0.9905		3.993	10.622					489.56	3557.62	17.89		
C ₂ H ₆ 30.24	0.17	0.27	0.31	0.250			30.1													
				M.W.	24.28715	215.7	3.354	4.7		211 #/hr.										
				STEAM			0.920													

OPERATING CONDITIONS				PRODUCT TESTS			CATALYST DATA							
PRESSURES PSIG		RATES S.C.F.H.			OIL	WATER	INVENTORY DATA		PARTICLE SIZE					
Oxygen	441	Fresh Feed	15,846	*API	55.4	10.8	In Reactor at Start of Period			Screen Analysis		Sedimentation		
Natural Gas	445	Recycle	15,272	Neut. No.	43.0	33.2	Fresh Catalyst Added			Mesh	Microns	%	Microns	%
Generator Outlet	417	Combined Feed	31,118	Sap. No.	56.7	36.2	Total			On 40	419+		80+	
Reactor Inlet	414	Wet Gas—Measured	4,300	Hydrox. No.			Catalyst Recovered		42	100	150		40—80	
Condenser Inlet		Adjusted	4,752	Bromine No.	96		In Reactor at End of Period			150	105		20—40	
Product Accumulator	362	Loss	452	Pour °F.						200	74		10—20	
				Chemicals, % by K ₂ CO ₃		11.5	REACTOR d-p, Inches H ₂ O			250	62		0—20	
							No. Height			325	44			
TEMPERATURES—°F.		Recycle/Fresh Feed	0.96				0 Period A		-	<325				
Oxygen	502	Inlet Velocity—ft./sec.	0.96				1		75	CATALYST				
Natural Gas	792	Fresh Feed Rates— $\frac{\text{S.C.F.H.}}{\text{H}_2 + \text{CO}}$	15439	HEMPEL DIST. %	°API	2			79	Bulk Density, Lbs./Cu.Ft.				
Generator	2259	per Cu.Ft. Dense Bed	1084	205 °F.		3			83	Aerated				
Quench Accumulator	137	per Lb. Catalyst	6.95	400	90.0	55.9	4		390	Settled				
Reactor Inlet	331	per Sq. Ft.	23392	400-550	11.2	35.4	Total		617	Compacted				
Condenser Inlet	578			550+	8.8					Particle Density, gm./cc.				
Product Accumulator	88						CALCULATED FROM dp			NH ₃ Value, ml./gm.				
Catalyst No.	Height			A. S. T. M. DIST. ON			Density, Lbs./Cu.Ft.		156	N ₂ Surface, m ² /gm.				
1	567			Naphtha °F.			Inventory, Lbs.		2221					
2	659			IBP	83		Bed Depth, Ft.		21.57	CHEMICAL ANALYSIS				
3	654			10%	124		Vol., Cu. Ft.		14.24	Fe				
4	659			50%	201					C				
5	665			90%	325					O				
6	661			EP	384					H				
7	650			Rec.	97.5					K ₂ O, W+, % basis Fe				
8	643									X-Ray Analysis—				
9	637									Fe ₂ O ₃				
10	632									Fe ₂ O ₄				
11	517									Fe				

[illegible]

FRESH FEED				WET GAS		RECYCLE		COMBINED FEED		EFFLUENT		NET CHANGE		YIELD BASIS H ₂ + CO FEED								
	%	m/hr		%	At B/L Balance	m/hr	m/hr	m/hr	m/hr	m/hr	#/hr	#/MCF	#/gal	gal/hr	gal/MCF	CONDENSATE				YIELDS BASIS BROWNFIELD DESIGN FEED RATE*		
	37.20%	15.777	441.89	7.810	1.052	29.47	3.137	19.914	4.189	-14.725	-12.42						CORRECTED RECOVERY, %	gal/hr	RECOVERY, %	gal/hr		
CO	37.20%	15.777	441.89	7.810	1.052	29.47	3.137	19.914	4.189	-14.725	-12.42											
H ₂	60.417	26.621	51.64	36.584	4.929	9.94	14.693	40.314	19.622	-20.692	-41.70						400 EP	83.0	7.732	98.0		
C ₂ H ₄	2.140	0.908	39.96	31.410	4.232	186.25	12.615	13.623	16.847	3.324	146.29	9.311					400-550	10.6	0.988	91.4		
N ₂	0.160	0.098	1.91	1.710	0.320	6.44	0.687	0.755	0.917								550 +	5.4	0.596	114.6		
CH ₄	0.080	0.034	0.55	0.640	1.299	20.84	3.872	3.906	5.171	1.265	20.29	1.291								0.683		
C ₂ H ₆				2.553	0.344	0.65	1.025	1.025	1.369	0.344	9.65	0.614										
C ₃ H ₈				1.973	0.266	8.00	0.792	1.058	0.266	8.00	0.509											
C ₄ +																						
C ₂ H ₂				3.447	0.464	19.52	1.394	1.394	1.048	0.464	19.52	1.242	4.32	4.519	0.288		PROPYLENE	44.4	8.67			
C ₂ H ₆				0.313	0.042	1.85	0.126	0.126	0.168	0.042	1.85	0.118	4.24	0.436	0.028		C ₂ POLY GAS	87.5	7.59	1.269		
C ₃ H ₈				2.373	0.320	17.95	0.953	0.953	1.273	0.320	17.95	1.143	5.00	5.990	0.229		C ₃ POLY GAS	12.5	1.08	0.143		
C ₄ H ₁₀				0.613	0.083	4.82	0.246	0.246	0.329	0.083	4.82	0.307	4.86	0.992	0.063							
C ₅ H ₁₂				1.077	0.145	10.17	0.433	0.433	0.578	0.145	10.17	0.647	4.43	1.866	0.119		C ₄ POLY GAS	5.98	14.76	2.468		
C ₆ H ₁₄				0.187	0.025	1.80	0.075	0.075	0.100	0.025	1.80	0.115	5.28	0.633	0.022		C ₅ GAS	4.86	4.82	0.992		
C ₇ H ₁₆				0.310	0.042	3.53	0.125	0.125	0.167	0.042	3.53	0.225	5.54	0.547	0.041		C ₆ FREE GAS			11.692		
C ₈ +																	C ₇ POLY TAR	7.53	2.11	0.280		
C ₂ +																						
TOTAL	42.408	535.95		13.473	330.23	40.163	82.571	61.606														
H ₂ +CO	97.520	41.398	15711	SCFH	5.981		17.630	59.228	23.811	-35.417												
H ₂ /CO		1.82	Factor	636496	4.68		4.68	2.13	4.68	1.41												
Weight Recovery, %	92.47		Analyst	Age, hrs.	144		Space Velocity, vhr	1114		RECOVERED	59.61	3.794		9.436	0.593		10% WET GAS GASOLINE	15.366	0.9782	5303		
Pressure, psig	416		Inlet Velocity, Ft/sec	0.97	Analyst	Vol, CP	14.10		TOTAL OIL	119.25	7.591		21.699	1.385			FUEL OIL	0.683	0.0435	236		
Temperature, °F	656		Bed Depth, Ft	21.37	Weight, g	8200			0.290pc	15.40	0.980		1.939	0.123			POLY TAR	0.423	0.0269	146		
Reycle Ratio	0.95		Bed Density, CP	156	Balance (H ₂ /CO)	10.88				13.46	8.571		23.638	1.506			TOTAL	17.377	1.1061	5997		
			Shift Ratio (H ₂ /CO)																			
FRESH FEED CONVERSION - %				TOTAL FEED CONVERSION - %				SELECTIVITY				NET WATER				W. S. CHEM.						
Contraction	CO	H ₂	H ₂ +CO	CO	H ₂	CO+H ₂	C ₂ + C ₃ +	GROSS WATER HYDROCARBON TOTAL (L+G)														
68.23	93.33	80.76	85.55	77.85	51.33	59.80	78.02															

$$*9488 \text{ MCFH H}_2 + \text{CO, Bbl/Day} = 3421.6 \times \text{gal/MCF}$$

OPERATING CONDITIONS				PRODUCT TESTS			CATALYST DATA						
PRESSURES PSIG		RATES S.C.F.H.		OIL		WATER	INVENTORY DATA		PARTICLE SIZE				
Oxygen	446	Fresh Feed	16,094	*API	52.6	10.7	In Reactor at Start of Period		Screen Analysis		Sedimentation		
Natural Gas	452	Recycle	15,242	Neut. No.	45.9	34.6	Fresh Catalyst Added		Mesh	Micros	%	Micros	%
Generator Outlet	422	Combined Feed	31,336	Sap. No.	55.0	36.6	Total		On 40	419+		80+	
Reactor Inlet	416	Wet Gas—Measured	4,488	Hydrox. No.			Catalyst Recovered		38	100	150	40—80	
Condenser Inlet		Adjusted	5,113	Bromine No.	86		In Reactor at End of Period			150	105	20—40	
Product Accumulator	367	Loss	625	Pour °F.						200	74	10—20	
				Chemicals, % by K ₂ CO ₃		11.0	REACTOR d-p. Inches H ₂ O			250	62	0—20	
							No. Height			325	44		
TEMPERATURES—°F.		Recycle/Fresh Feed	0.95				See Period A			<325			
Oxygen	469	Inlet Velocity—ft./sec.	0.97				1	76	CATALYST				
Natural Gas	785	Fresh Feed Rate— $\frac{\text{S.C.F.H.}}{\text{H}_2 + \text{CO}}$	18711	HEMPEL DIST. %		*API	2	80	Bulk Density, Lbs./Cu.Ft.				
Generator	2293	per Cu.Ft. Dense Bed	1114	206 °F.			3	80	Aerated				
Quench Accumulator	152	per Lb. Catalyst	7.14	400		82.0	55.3	4	375	Settled			
Reactor Inlet	386	per Sq. Ft.	23805	400-550	10.6	33.3	Total		611	Compacted			
Condenser Inlet	584			550+	7.4				Particle Density, gm./cc.				
Product Accumulator	95	Heat Transfer Calculations					CALCULATED FROM dp		NH ₃ Value, ml./gm.				
Catalyst No.	Height	Steam Rate = 160#/hr.		A. S. T. M. DIST. ON			Density, Lbs./Cu.Ft.		186	N ₂ Surface, m ² /gm.			
1	See Period A	@705 psia & 506°P. =		Naphtha °F.			Inventory, Lbs.		2200				
2	655	1201 Btu/#		IBP		98	Bed Depth, Ft.		21.37	CHEMICAL ANALYSIS			
3	651	Water in @60°P. = 28 Btu/#		106		128	Vol., Cu. Ft.		14.10	Fe			
4	658	Net Heat Transferred/# steam = 506		213						C			
5	662	1173 Btu		906		343				O			
6	661	(1173)(160) = 187,680 Btu/hr.		EP		386				H			
7	654	Ave. Bed Temp. = 656°P.		Rec.		97.0				K ₂ O, W+%, % basis Fe			
8	649	dT = 656-506 = 150°P.								X-Ray Analysis—			
9	641	Tube Area = 37.7 sq. ft.								Fe ₂ O ₃			
10	637	K = $\frac{187,680}{(37.7)(150)}$ 33.2 Btu/°F./sq. ft.								Fe ₂ O ₄			
11	523									Fe			

[illegible]

GAS ANALYSES					GENERATOR BALANCE										WEIGHT BALANCE				
HOURL	1400	2200	0600	AVERAGE	M/HR	C	H	O		Mol %	M/Hr	C	H	O		#/hr Measured	At Wt. Balance		
FRESH FEED																			
CO _{28.000}	37.24	37.03	37.34	37.203	15.684	15.684		15.684		0.27	0.540			21.168		294.25	330.05		
CO _{28.010}										0.36	0.720	0.179		0.358		56.76	56.76		
H _{22.016}	60.37	60.42	60.23	60.340	25.438		50.876			0.83	0.110					146.66	146.66		
CH _{40.010}	2.00	2.30	2.14	2.147	0.905	0.905		1.810		83.02	10.955	10.955	43.820			497.97	533.47		
N _{278.016}	0.17	0.20	0.19	0.187	0.079					6.90	0.911	1.882	5.466			533.47			
CH _{40.002}	0.22	0.05	0.10	0.123	0.052	0.052	0.208			5.45	0.719	2.187	5.752						
										1.56	0.206	0.824	2.060						
			M. W. 18.016	12.65403						1.61	0.61	0.080	0.400	0.960					
							7.503	3.752								1121665			
						16.641	58.587	21.246		MW = 20.06012						INDICATED LOSS - S C F H	560		
						101.86	100.91	99.77		TOTAL		16.337	58.058	21.510					
			BALANCE																
WET GAS					GAS FLOW RATES										LIQUID PRODUCT RATES				
CO _{28.000}	7.39	7.47	7.53	7.460		V. R.	PRESSURE	TEMP.		M. W.	S. C. F. H	M/Hr		HOURL	GAGE	GAL.	"F		
H _{22.016}	37.23	37.12	36.44	36.930	FRESH FEED		414.9	70		2287806				OIL	713.8"	386.41	70		
CO _{28.010}	30.81	31.47	32.17	31.484	79.31	6.496	20.727	-0.9905		1.5126	15.999	42.158			510"	266.38	52		
N _{278.016}	1.64	1.62	1.79	1.650			1.51	68		1192358					7"	1.0039	287.42		
CH _{40.002}	10.43	9.93	9.70	10.020	158.44	6.654	4.026	0.9924	1.0919	4.599	12.119				313"	169.79	52		
C ₂ H _{60.008}	2.53	2.65	2.49	2.554			414.8	126							1'5.8"	77.06	72		
C ₃ H _{80.004}	1.80	1.95	1.91	1.920	79.31	8.070	20.724	0.9420	1.0919	14.370	37.866								
C ₄ H _{100.002}	3.44	3.49	3.15	3.360															
C ₅ H _{120.001}	5.31	0.29	0.28	0.293	5.02	8.821	20.724	1.0000	1.0919	1.002	2.640								
C ₆ H _{140.001}	2.25	2.18	2.15	2.193	NATURAL GAS		449.9	804		1443162									
C ₇ H _{160.001}	0.70	0.54	0.51	0.717	28.43	7.698	21.555	0.9849	1.2013	5.008	13.185								
C ₈ H _{180.001}	0.97	0.91	0.95	0.943	OXYGEN		443.5	74											
C ₉ H _{200.001}	0.23	0.15	0.26	0.213	27.07	8.995	21.406	0.9868		4.000	10.540								
C ₁₀ H _{220.001}	0.28	0.23	0.28	0.283	STEAM														
			M. W. 18.016	24.28001	215.7	2.471													

FRESH FEED										WET GAS		RECYCLE	COMBINED FEED	EFFLUENT		NET CHANGE		YIELD BASIS H ₂ + C ₆ P ₂									
			%	m/hr	#/hr	%	At Wet Balance		m/hr	m/hr	m/hr	m/hr	m/hr	#/hr	#/hr	#/MCF	CONDENSATE			YIELDS BASIS BROWNSVILLE DESIGN FEED RATE*							
			%	m/hr	#/hr	%	m/hr		m/hr	m/hr	m/hr	m/hr	m/hr	#/hr	#/hr	#/MCF	gal/hr			CORRECTED			THERMAL RECOVERY				
			%	m/hr	#/hr	%	m/hr		m/hr	m/hr	m/hr	m/hr	m/hr	#/hr	#/hr	#/MCF	gal/hr			gal/hr			gal/hr				
CO	28.00	37.337	15.891	445.11	7.587	1.070	29.37	3.060	18.951	4.130	-14.881	-115.14															
H ₂	60.383	25.674	61.76	37.974	5.355	10.80	15.316	40.990	20.671	-20.319	-40.96									400 EP	82.0	7.047	98.0	6.905			
CO ₂	1.987	0.846	37.23	30.707	4.331	190.60	12.596	13.232	16.717	3.485	153.37	9.723							400-550	11.2	0.962	91.4	0.879				
N ₂	0.210	0.069	2.49	1.780	0.251	7.03	0.718	0.807	0.969										550 +	6.8	0.584	114.6	0.669				
CH ₄	0.143	0.081	0.98	9.360	1.320	21.18	3.775	3.836	5.095	1.259	20.20	1.281															
C ₂ H ₆					2.630	0.371	10.41	1.061	1.432	0.371	10.41	0.660															
C ₃ H ₈					1.833	0.259	7.79	0.739	0.739	0.998	0.259	7.79	0.434														
C ₄ + C ₅																											
C ₆ H ₁₄					3.083	0.435	18.30	1.244	1.244	1.679	0.435	18.30	1.160	4.32	4.236	0.269											
C ₇ H ₁₆					0.250	0.035	1.54	0.101	0.101	0.136	0.036	1.54	0.098	4.24	0.363	0.023											
C ₈ H ₁₈					0.280	0.322	18.07	0.920	0.920	1.242	0.322	18.07	1.146	5.00	3.514	0.229											
C ₉ H ₂₀					0.753	0.106	6.16	0.304	0.304	0.410	0.106	6.16	0.391	4.86	1.287	0.080											
C ₁₀ H ₂₂					1.113	0.157	11.01	0.449	0.449	0.606	0.157	11.01	0.698	5.48	2.020	0.128											
C ₁₁ H ₂₄					0.823	0.031	2.24	0.090	0.090	0.121	0.031	2.24	0.128	5.28	0.487	0.027											
C ₁₂ H ₂₆					0.427	0.060	5.05	0.172	0.172	0.232	0.060	5.05	0.320	5.54	0.912	0.058											
C ₁₃ + C ₁₄																											
TOTAL		42.561	537.57		14.103	340.15	40.335	82.996	62.124					62.37	3.955	12.839	0.814										
H ₂ + CO	97.680	41.565	15774	SCFH	6.425		18.376	59.941	24.801	-35.140																	
H ₂ /CO	1.62			Factor	633954	5.01	5.01	2.16	5.01	1.37																	
Weight Recovery, %	92.20			Catalyst Age, hrs	192		Space Velocity, vhr	1126					RECOVERED OIL	0.3940%	55.25	3.503	8.593	0.545									
Pressure, psig	412			Inlet Velocity, Ft/sec	0.98		Catalyst Vol., CF	14.01					WATER	117.68	7.458	21.432	1.359										
Temperature, °F	658			Bed Depth, Ft	21.23		Weight, #	2158					TOTAL LIQUOR	0.3080%	16.34	1.036	2.060	0.131									
Recycle Ratio	0.95			Bed Density, #/CF	154		Effluent (H ₂ /CO) Sulf Ratio (H ₂ /CO)	11.98					PRODUCED LIQ		133.96	8.494	23.492	1.490									
FRESH FEED CONVERSION - %								TOTAL FEED CONVERSION - %								SELECTIVITY											
Conversion	CO	H ₂	H ₂ + CO	CO	H ₂	CO + H ₂	C ₆ + C ₇ + C ₈	WATER					NET WATER	6.984%	125.83	7.977	15.106	0.958									
								GREY WATER							148.17	9.013	17.166	1.088									
								HYDROCARBON WASH - C ₆ + C ₇							59.68	77.72											
Form ML-11	66.86	93.27	79.14	84.51	78.21	49.57	55.68	172.3610	0.329																		

OPERATING CONDITIONS				PRODUCT TESTS			CATALYST DATA							
PRESSURES PSIG		RATES SCFH.		OIL		WATER	INVENTORY DATA		PARTICLE SIZE					
Oxygen	440	Fresh Feed	16,192	*API	51.7	10.8	In Reactor at Start of Period			Screen Analysis		Sedimentation		
Natural Gas	448	Recycle	15,307	Neut. No.	44.8	34.6	Fresh Catalyst Added			Mesh	Micros	%	Micros	%
Generator Outlet	416	Combined Feed	31,459	Sap. No.	55.6	35.6	Total			On 49	419+		80+	
Reactor Inlet	412	Wet Gas—Measured	4,692	Hydrox. No.			Catalyst Recovered	20.5		100	150		40—80	
Condenser Inlet		Adjusted	5,352	Bromine No.	86		In Reactor at End of Period			150	105		20—40	
Product Accumulator	360	Loss	660	Four °F.						200	74		10—20	
				Chemicals. > by K ₂ CO ₃		12.0	REACTOR d.p., Inches H ₂ O			250	62		0—20	
							No. Height			325	44			
TEMPERATURES—°F.		Recycle/Fresh Feed		0.95			0 See Period A	-	<325					
Oxygen	488	Inlet Velocity—ft./sec.		0.98			1	73	CATALYST					
Natural Gas	790	Fresh Feed Rate $\frac{H_2}{SCFH} \frac{CO}{CO}$		15/74	HEMPEL DIST. %	*API	2	87	Bulk Density, Lbs./Cu.Ft.					
Generator	2283	per Cu.Ft. Dense Bed		1126	205 °F.		3	74	Aerated					
Quench Accumulator	150	per Lb. Catalyst		7.31	400	81.0	54.2	4	365	Settled				
Reactor Inlet	343	per Sq. Ft.		23900	400-550	11.2	35.6	Total	599	Compacted				
Condenser Inlet	586				550*	7.8				Particle Density, gm./cc.				
Product Accumulator	96	Heat Transfer Calculations						CALCULATED FROM dp		NH ₃ , Value, ml./gm.				
Catalyst No.	Height	Steam Rate = 414 #/hr.		A.S.T.M. DIST. ON			Density, Lbs./Cu.Ft.	154	N ₂ Surface, m ² /gm.					
1	See Period A	@705 psia & 506°F. =		Naphtha °F.			Inventory, Lbs.	2158						
2	658	= 1201 Btu/#		IRP	104		Bed Depth, Ft.	21.53	CHEMICAL ANALYSIS					
3	650	Water in @ 70°F. = 38°F.		10%	129			Vol., Cu. Ft.	14.01	Fe				
4	660	Net Heat Transferred/# steam = 50%		221						C				
5	665	= 1163 Btu		90%	338					O				
6	665	(1163)(414) = 481,482 Btu/hr.		EP	590					H				
7	659	Ave. Bed Temp. = 658°F.		Rec.	97.5					K ₂ O, W + , % basis Fe				
8	652	dT = 658-506 = 152°F.								X-Ray Analysis—				
9	644	Tube Area = 37.7 sq. ft.								Fe ₂ O ₃				
10	640	481,482 K = $\frac{481,482}{152}$								Fe ₃ O ₄				
11	524	= 84.0 Btu/°F./sq. ft.								Fe				

[illegible]

FRESH FEED												WET GAS		RECYCLE		COMBINED FEED		EFFLUENT		NET CHANGE		YIELD BASIS H ₂ + CO FED									
	%	m/hr	\$/hr	%	AS Wt. Balance	m/hr	m/hr	m/hr	m/hr	m/hr	m/hr	m/hr	m/hr	m/hr	#/MCF	CONDENSATE	CONDENSATE	YIELDS	BASIS BROWNVILLE	DESIGN FEED RATE*											
CO																gal/hr	gal/MCF														
CO	37.800	15.878	444.72	8.150	1.204	35.72	13.942	19.220	4.546	-14.674	-411.00																				
H ₂	59.747	25.095	50.59	38.803	5.732	11.56	15.840	41.006	21.542	-19.364	-39.03							400 EP	84.2	6.698	98.0										
N ₂	2.113	0.988	39.09	50.520	4.511	198.58	12.514	13.402	17.025	3.623	159.44	10.253						400-550	11.2	0.891	91.4										
CO	0.207	0.087	2.44	1.466	0.217	6.08	0.901	0.688	0.818									550 +	4.6	0.366	114.6										
CH ₄	0.133	0.056	0.90	9.366	1.384	22.20	3.640	3.896	5.224	1.328	21.30	1.370																			
C ₂ H ₆				2.580	0.381	10.69	1.058	1.058	1.439	0.381	10.69	0.687																			
C ₃ H ₈				1.797	0.265	7.97	0.737	0.737	1.002	0.265	7.97	0.513																			
C ₄ + C ₅																															
C ₆ H ₁₄				3.037	0.449	18.89	1.245	1.245	1.694	0.449	18.89	1.215	4.32	4.373	0.281																
C ₇ H ₁₆				0.287	0.042	1.85	0.118	0.118	0.160	0.042	1.85	0.119	1.24	0.436	0.028																
C ₈ H ₁₈				2.017	0.288	16.72	0.827	0.827	1.125	0.288	16.72	1.075	5.00	3.344	0.215																
C ₉ H ₂₀				0.570	0.084	4.88	0.234	0.234	0.313	0.084	4.88	0.314	1.86	1.004	0.065																
C ₁₀ H ₂₂				0.900	0.133	9.33	0.369	0.369	0.502	0.133	9.33	0.600	8.45	2.712	0.110																
C ₁₁ H ₂₄				0.247	0.036	2.60	0.101	0.101	0.137	0.036	2.60	0.167	8.28	0.495	0.032																
C ₁₂ H ₂₆				0.260	0.038	3.20	0.107	0.107	0.145	0.038	3.20	0.206	5.54	0.578	0.037																
C ₁₃ H ₂₈																															
TOTAL	42.005	537.73		14.774	348.21	41.003	83.068	65.294																							
H ₂ + CO	97.547	40.974	15550	SCFH	6.936		19.282	60.226	26.188	-34.039																					
H ₂ /CO	1.58			Factor	643086	4.76	4.76	2.13	4.76	1.32																					
Weight Recovery, %	90.63			Catalyst Age, hrs.	216		Space Velocity, vhr	1112					RECOVERED OIL	0.36684	51.30	3.299	7.955	0.51													

##Included in Resactor Effluent Total

 $\eta/\text{NCM} = 16.91 \text{ g/g MCF}$
$$20484 \text{ MCFH H}_2 + \text{CO Bbl/DAY} = 3421.6 \times \text{gal/MCF}$$

OPERATING CONDITIONS				PRODUCT TESTS			CATALYST DATA						
PRESSURES PSIG		RATES SCFH			OIL	WATER	INVENTORY DATA		PARTICLE SIZE				
Oxygen	429	Fresh Feed	15941	* API	51.2	10.8	In Reactor at Start of Period		Screen Analysis		Sedimentation		
Natural Gas	447	Recycle	15561	Neut. No.	49.2	36.4	Fresh Catalyst Added		Mesh	Microns	%	Microns	%
Generator Outlet	414	Combined Feed	31502	Sap. No.	61.0	40.2	Total		On 40	419+		80+	
Reactor Inlet	409	Wet Gas—Measured	4795	Hydrox. No.			Catalyst Recovered		35	100	150	40—80	
Condenser Inlet		Adjusted	5607	Bromine No.	82		In Reactor at End of Period			150	105	20—40	
Product Accumulator	360	Loss	812	Pour °F.						200	74	10—20	
				Chemicals, % by K ₂ CO ₃		12.0	REACTOR d-p. Inches H ₂ O			250	62	0—20	
							No. Height			325	44		
TEMPERATURES—°F.				Recycle/Fresh Feed		0.98	0 See Period A			<325			
Oxygen	500	Inlet Velocity—ft./sec.	0.99				1		74		CATALYST		
Natural Gas	791	Fresh Feed Rate—SCFH.	15550	HEMPEL, DIST. %	0 API		2		88	Bulk Density, Lbs./Cu.Ft.			
Generator	2270	per Cu.Ft. Dense Bed	1112	205 °F.			3		68	Aerated			
Quench Accumulator	147	per Lb. Catalyst	7.31	400	83.2	53.0	4		360	Settled			
Reactor Inlet	342	per Sq. Ft.	23561	400-550	11.2	53.8	Total		590	Compacted			
Condenser Inlet	590			350*	5.6					Particle Density, gm./cc.			
Product Accumulator	97	Heat Transfer Calculations					CALCULATED FROM dp			NH ₃ Value, ml./gm.			
Catalyst No.	Height	Steam Rate = 407#/hr.		A. S. T. M. DIST. ON			Density, Lbs./Cu.Ft.		152	N ₂ Surface, m ² /gm.			
1	See Period A	@705 psia & 506°P =		Naphtha °F.			Inventory, Lbs.		2126				
2	658	1201 Btu/#		IBP		102	Bed Depth, Ft.		21.19	CHEMICAL ANALYSIS			
3	650	Water in @65°P = 37 Btu/#		10%		132	Vol., Cu. Ft.		13.99	Fe			
4	660	Net Heat Trans./#Steam		50%		218				C			
5	665	1164 Btu		90%		339				O			
6	665	(1164)(407) = 473,748 Btu/hr.		EP		389				H			
7	660	Ave. Bed Temp. = 658°P.		Rec.		97.0				K ₂ O W.-% basis Fe			
8	650	dT = 658-506 = 152°P								X-Ray Analysis—			
9	646	Tube Area = 37.8 sq. ft.								Fe ₂ O ₃			
10	642	K = (37.8)(152) =								Fe ₂ O ₃			
11	526	82.5 Btu/°Cp/sq. ft.								Fe			

GAS ANALYSES					GENERATOR BALANCE										WEIGHT BALANCE						
HOURL	1400	2200	0600	AVERAGE	M/HR	C	H	O		Mol %	M/Hr	C	H	O		#/hr Measured	At Wt. Balance				
FRESH FEED																					
CO ₂ 25.00	37.77	37.74	37.89	37.800	15.878	15.878		15.878	CO ₂ 25.00	0.86	10.472				21.012	WET GAS	297.80	348.21			
H ₂ 24.00	59.70	59.77	59.77	59.747	25.096	50.192			H ₂ 24.00	1.36	0.034	0.180			0.360	OIL	51.30	51.30			
CO ₂ 25.00	2.08	2.17	2.19	2.113	0.888	0.888		1.776	CH ₄ 12.00	82.76	10.927	10.927	43.708			WATER	487.32	138.22			
N ₂ 24.00	0.23	0.20	0.19	0.207	0.087				C ₂ H ₆ 3.00	6.79	0.897	1.794	5.382			FRESH FEED	537.73	537.73			
CH ₄ 12.00	0.22	0.12	0.06	0.133	0.056	0.056	0.224		C ₂ H ₄ 2.00	5.34	0.705	2.115	5.640			WEIGHT BALANCE	90.63				
				M. W	12.80154																
				H ₂ O 18.016							1.61	0.213	0.852	2.150							
							7.510	3.755			0.72	0.095	0.475	1.140		WET GAS FACTOR	1169274				
						16.822	57.926	21.409	MW =	20.13450						INDICATED LOSS-C F H	812				
				BALANCE					TOTAL			16.343	58.000	21.372							
					102.93	99.87	100.17														
WET GAS					GAS FLOW RATES										LIQUID PRODUCT RATES						
CO ₂ 25.00	7.86	8.20	8.39	8.150		V/R	PRESSURE	TEMP.	M. W.	S. C. F. H.	M/HR		OIL	GAGE	GAL.	"F	FACTOR	GAL. AT 64	API°	#	#/HR GAL. HR
H ₂ 24.00	38.81	38.83	38.77	38.803	FRESH FEED		408.8	71	2261446					7'14"	390.78	63	0.9985	390.19	51.2		
CO ₂ 25.00	30.22	30.62	30.72	30.520	79.31	6.563	20.579	0.9896	1.5038	15.941	42.005			6'10"	365.68	60	1.0000	365.68	6.448		
N ₂ 24.00	1.49	1.45	1.46	1.466	WET GAS		1.51	71	1228269					3'14"	179.09	60	1.0000	179.09			
CH ₄ 12.00	9.54	0.39	0.97	0.386	158.44	6.854	4.026	0.9896	1.1083	4.795	12.635			0'14"	17.70	68	0.9961	17.63			
C ₂ H ₆ 3.00	2.63	2.57	2.64	2.580	RECYCLE		410.8	126										4.96	+32.00	51.30	
C ₂ H ₄ 2.00	1.86	1.79	1.75	1.787	79.31	8.829	20.628	0.9404	1.1083	14.543	38.321							190.93		1831.12	7.955
C ₂ H ₂ 0.74	3.14	2.98	2.99	3.037	BLEED																
O ₂ 21.00	0.29	0.29	0.28	0.287	5.02	8.867	20.628	1.0000	1.1083	1.018	2.682		WATER	7'14"	386.41	74	0.99846	385.81	10.8		
C ₂ H ₂ 0.74	2.13	1.94	1.98	2.017	NATURAL GAS		446.9	200	1437830					6'14"	336.22	75	0.99832	335.66	8.282		
C ₂ H ₂ 0.74	0.87	0.87	0.87	0.870	28.43	7.708	21.486	0.8876	1.1991	5.011	15.204			7'14"	377.68	77	0.99804	376.94			
C ₂ H ₂ 0.74	0.96	0.87	0.87	0.900	OXYGEN		439.3	74						1'8"	90.37	69	0.99907	90.79			
C ₂ H ₂ 0.74	0.26	0.24	0.25	0.247	27.07	6.993	21.307	0.9868		3.974	10.472			2'2'3"	115.92	76	0.99819	115.71			
C ₂ H ₂ 0.74	0.26	0.26	0.26	0.260	STeam		88.7	47						1'0"	62.00	64	0.99963	61.98			
				M. W.	23.569744	215.7	6.579	0.2886		407 #/M.								400.53		3317.19	16.682

[illegible]
$$c/NCM = 16.91 \times F/MCF \quad {}^{80}9488 MCFH H_2 + CO, BH/D_{AV} = 1421.6 \times g_{41}/MCF$$

OPERATING CONDITIONS				PRODUCT TESTS			CATALYST DATA							
PRESSURES PSIG		RATES S.C.F.H.			OIL	WATER	INVENTORY DATA		PARTICLE SIZE					
Oxygen	438	Fresh Feed	16,078	*API	51.3	10.7	In Reactor at Start of Period		Screen Analysis					
Natural Gas	450	Recycle	15,891	Neut. No.	49.3	35.2	Fresh Catalyst Added		Mesh	Microns	%	Microns	%	
Generator Outlet	414	Combined Feed	31,967	Sap. No.	61.0	39.0	Total		On 40	419+		80+		
Reactor Inlet	409	Wet Gas—Measured	4,941	Hydrox. No.			Catalyst Recovered		39.5	100	150	40—80		
Condenser Inlet		Adjusted	5,560	Bromine No.	78		In Reactor at End of Period		150	105		20—40		
Product Accumulator	359	Loss	619	Pour °F.					200	74		10—20		
				Chemicals, % by K ₂ CO ₃		11.0	REACTOR d.p. Inches H ₂ O		250	62		0—20		
							No. Height		325	44				
TEMPERATURES—°F.		Recycle/Fresh Feed	0.99				0 See Period A		<325					
Oxygen	481	Inlet Velocity—ft./sec.	1.01				1		72	CATALYST				
Natural Gas	797	Fresh Feed Rate—S.C.F.H. $\frac{100}{100} \times 40$	15701	HEMPEL DIST. %		°API	2		87	Bulk Density, Lbs./Cu.Ft.				
Generator	2294	per Cu.Ft. Dense Bed	1133	205 °F.			3		68	Aerated				
Quench Accumulator	124	per Lb. Catalyst	7.55	400	84.0	53.5	4		350	Settled				
Reactor Inlet	359	per Sq. Ft.	23789	400-550	10.4	34.0	Total		577	Compacted				
Condenser Inlet	593			550+	5.6				Particle Density, gm. cc.					
Product Accumulator	95	Heat Transfer Calculations					CALCULATED FROM dp		NH ₃ Value, ml./gm.					
Catalyst No.	Height	Steam Rate = 404#/hr.			A. S. T. M. DIST. ON		Density, Lbs./Cu.Ft.		150	N ₂ Surface, m ² /gm.				
1	See Period A	@705 psia & 506° P.			Naphtha °F.		Inventory, Lbs.		2079					
2	660	1201 Btu/#			IBP		98	Bed Depth, Ft.		21.00	CHEMICAL ANALYSIS			
3	652	Water in @68°P = 30 Btu/#			10%		130	Vol., Cu. Ft.		13.86	Fe			
4	662	Net Heat Trans./# steam =			50%		220				C			
5	668	1171 Btu			90%		334				O			
6	667	(1171)(404) = 473,084 Btu/hr.			EP		394				H			
7	662	Ave. Bed Temp. = 661°P.			Rec.		37.4				K ₂ O Wt., % basis Fe			
8	656	dT = 661-506 = 155°P.									X-Ray Analysis—			
9	650	Tube Area = 37.6 sq. ft.									Fe ₂ Co			
10	646	$K = \frac{473,084}{(37.6)(155)}$									Fe ₂ O ₃			
11	598	81.2 Btu/Cp/sq.ft.									Fe			

[illegible]

CATALYST _____

$$r/\text{NCM} = 16.91 \times 4 / \text{MCF} \quad 80488 \text{ MCFH H}^- + \text{CO}_2 \text{ Bbl/D} = 5421.6 \times \text{gal/MCF}$$

GAS ANALYSES					GENERATOR BALANCE											WEIGHT BALANCE				
HOUR	1400	2200	0600	AVERAGE	M/HR	C	H	O		Mol %	M/Hr	C	H	O	# hr Measured	At Wt. Balance				
FRESH FEED																				
CO _{18.00}	37.12	37.44	36.95	37.170	15.763	15.763		15.763	O _{28.00}	0.23	10.472 0.031			21.006	WET GAS	305.35 345.83				
H _{28.00}	60.55	60.41	60.85	60.604	25.701		51.402		CO _{4.00}	1.19	0.160	0.160		0.320	OIL	50.02 50.02				
CO _{28.00}	1.78	1.81	1.78	1.790	0.079	0.759		1.518	N _{28.00}	1.39	0.188				WATER	133.74 133.74				
N _{28.00}	0.14	0.19	0.19	0.173	0.073				CH _{418.00}	82.49	11.052	11.052	44.248		TOTAL	489.12 530.59				
CH _{418.00}	0.41	0.15	0.23	0.263	0.112	0.112	0.448		C _{2H₆30.00}	7.35	0.986	1.972	5.916		FRESH FEED	530.59				
									C _{3H₈4.00}	5.34	0.716	2.148	5.728		WEIGHT BALANCE	92.18				
									C _{4H₁₀8.00}	1.48	0.198	0.792	1.980							
									C _{5H₁₂7.00}	0.53	0.071	0.355	0.852		WET GAS FACTOR	1135806				
									MM = 20.026955						INDICATED LOSS - SCFH	701				
									TOTAL			16.489	58.784	21.326						
BALANCE						100.88	101.04	98.57												
WET GAS					GAS FLOW RATES											LIQUID PRODUCT RATES				
CO _{28.00}	9.76	8.62	8.98	9.120		V/R	PRESSURE	TEMP.	M.W.	S.C.F.H	M/HR	HOUR	GAGE	GAL	'F	FACTOR	GAL AT 60°	APP. # GAL	#	# HR GAL HR
H _{28.00}	40.62	40.93	41.91	41.153	FRESH FEED		407.9	65°	2313885											
CO _{4.00}	27.21	28.32	27.60	27.710	79.31	6.521	20.557	0.9952	1.5211	16.094	42.40B									
N _{28.00}	1.26	1.71	1.51	1.493	WET GAS		1.57	66	1298803											
CH _{418.00}	9.84	9.12	9.98	9.313	158.44	7.150	4.034	0.9943	1.1353	5.159	13.594									
C _{2H₆30.00}	2.39	2.38	2.48	2.417	RECYCLE		407.9	183°												
C _{3H₈4.00}	1.76	1.78	1.79	1.767	79.31	8.546	20.557	0.9444	1.1353	14.939	39.365									
C _{4H₁₀8.00}	2.75	2.83	2.79	2.790	BLEED															
C _{5H₁₂7.00}	0.27	0.29	0.30	0.287	5.02	8.338	20.557	1.0000	1.1353	.977	2.574	WATER	357.50	76	0.99819	386.80	10.7			
C _{6H₁₄6.00}	1.94	1.90	1.75	0.863	NATURAL GAS		458.5	202°	1445551											
C _{7H₁₆5.00}	0.78	0.77	0.67	0.740	28.45	7.721	21.755	0.9863	1.2023	5.089	13.410									
C _{8H₁₈4.00}	0.89	0.85	0.75	0.830	OXYGEN		455.3	87°												
C _{9H₂₀3.00}	0.26	0.26	0.28	0.260	27.07	6.963	21.225	0.9933		3.974	10.472									
C _{10H₂₂2.00}	0.27	0.27	0.23	0.287	STEAM		29.5													
					M.W.	22.46269	215.7	6.392	0.897	399 #/hr.										