

Appendix A
Fischer-Tropsch Wax Characterization Raw Data

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Appendix

FT Wax Solvent Extraction Procedure

1. Melt about 4 grams of wax and disperse into 1 liter of warm reagent grade acetone.
2. Agitate using ultrasonic vibration for about 15 minutes at 50°C.
3. Let solution stand for 16 hours and decant solubles through a standard 3 micron fluoropore membrane filtration unit.
4. Wash filter and insoluble wax again with an additional 500 cc of acetone and allow solution to stand for about 4 hours.
5. Decant solubles through filter, rewash filter with acetone and add to acetone solubles.
6. Remove acetone with a nitrogen stream while gently warming the wax on the hot plate from both fractions (using a vacuum enhances the procedure).
7. Weigh solubles and insolubles.
8. Melt insolubles and disperse into 250-800 cc of cyclohexane dependent on the amount remaining after the removal of the acetone.
9. Repeat steps 2-7 above for separating the cyclohexane into soluble and insoluble portions.
10. Continue weighing procedure until no weight loss is observed, recovery is between 97-100%.

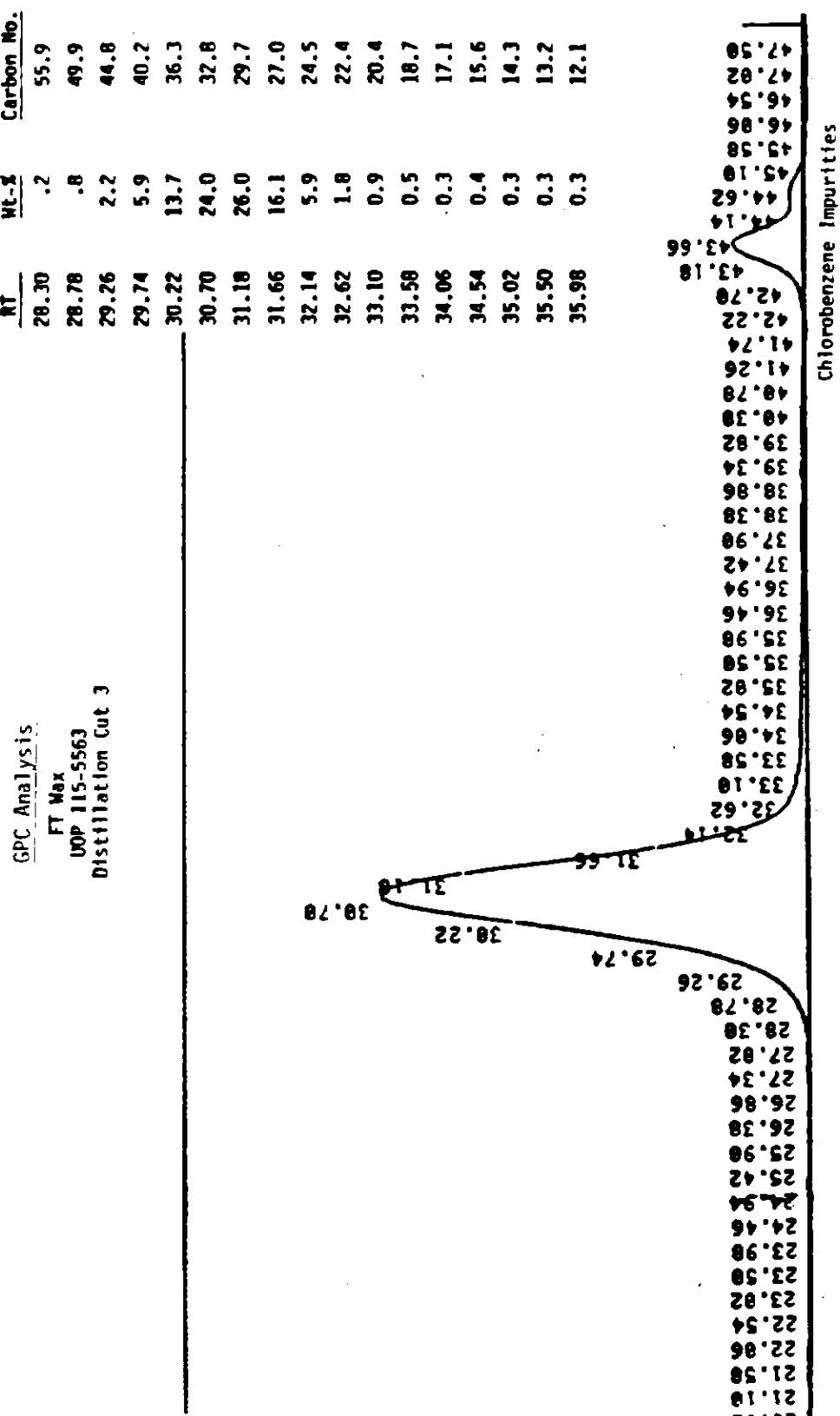
Standard Analytical Methods

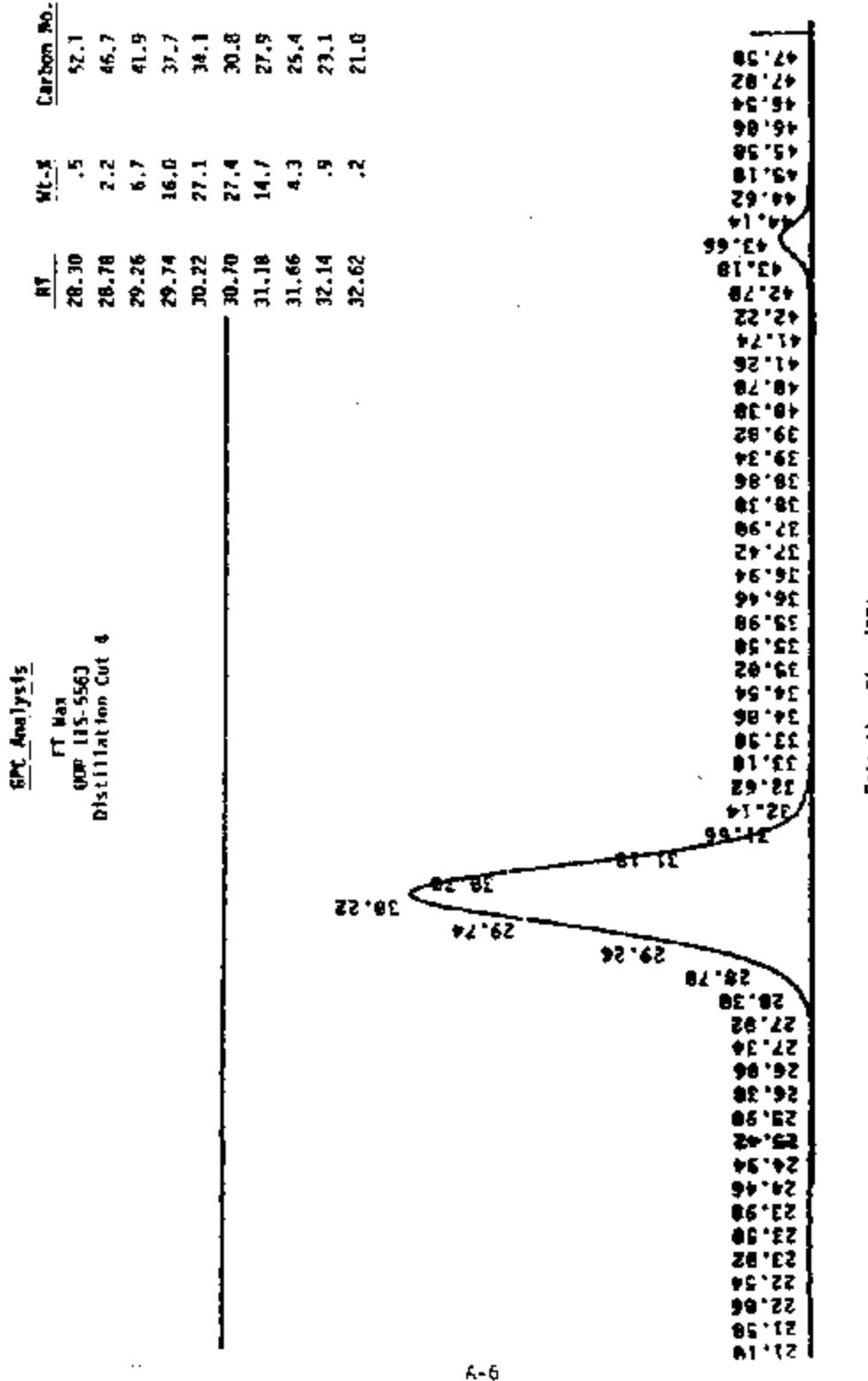
<u>Method Title</u>	<u>ASTM Method No.*</u>
API Gravity	D-1298
Specific Gravity	D-4052
IBP, °F	D-1160
Carbon and Hydrogen	
Oxygen, Total, in Organic Materials	
Trace Sulfur (Micro Coulometric Titration)	
Trace Nitrogen (Micro Coulometric Method)	D-3431
Aniline and Mixed Aniline Point	D-611-82
Melting Point of Petroleum Wax	D-87-77
Viscosity, Kinematic	D-445
Conradson Carbon Residue of Petroleum Products	D-189
Heptane Insolubles - Membrane Filtration	
Metals by Wet Ash Emmision	

* "1987 Annual Book ASTM Standards," American Society for Testing and Material, Philadelphia, PA 1987.

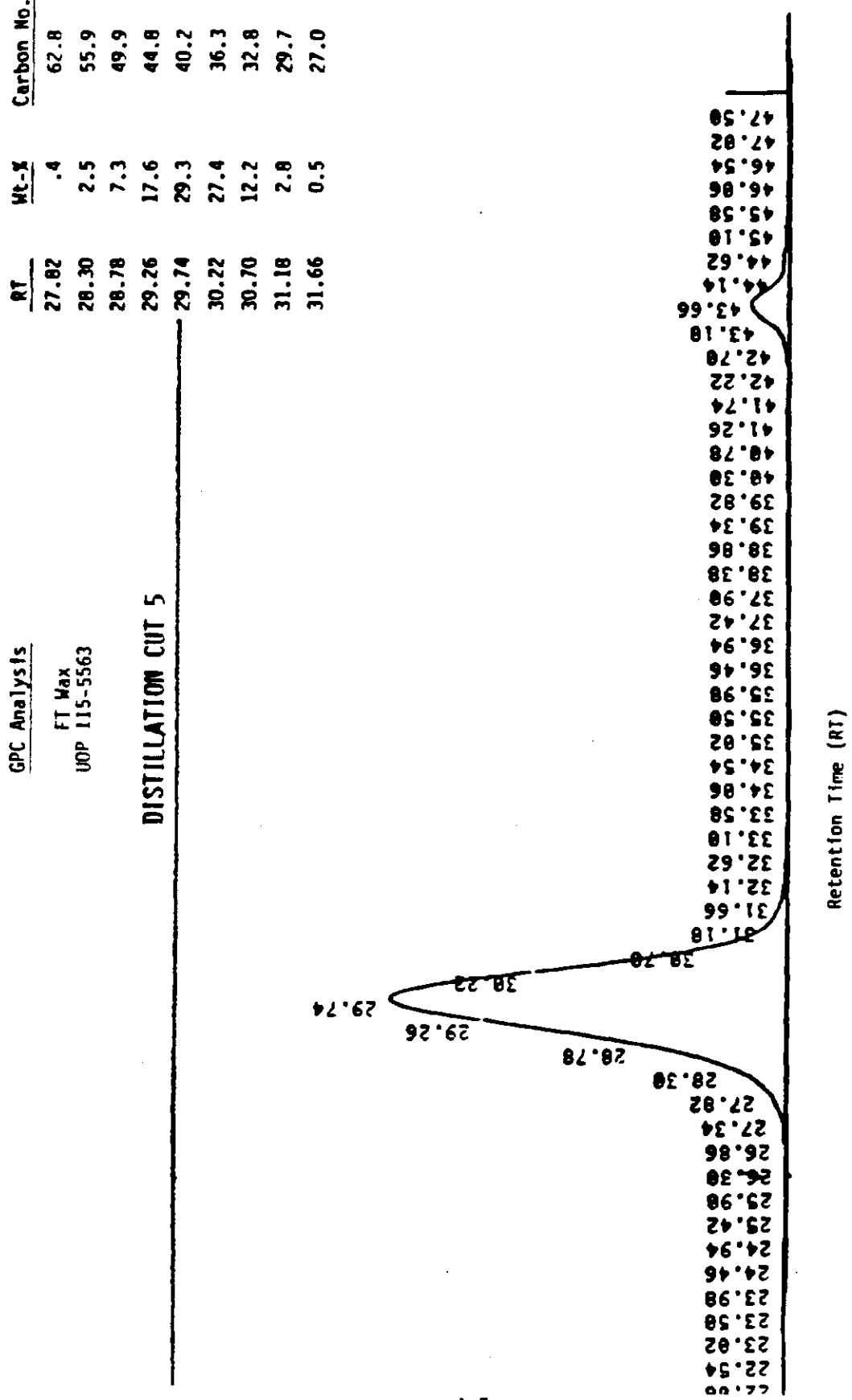
Gas Chromatography Analyses

	<u>Distillation</u>	
	<u>Cut 1</u>	<u>Cut 2</u>
C ₁₁	0.1	
C ₁₂	0.7	
C ₁₃	1.5	
C ₁₄	2.4	
C ₁₅	3.5	
C ₁₆	4.8	
C ₁₇	6.4	0.1
C ₁₈	8.3	0.4
C ₁₉	10.2	1.0
C ₂₀	11.7	2.4
C ₂₁	12.3	4.7
C ₂₂	11.2	7.6
C ₂₃	9.3	10.8
C ₂₄	6.8	12.5
C ₂₅	4.5	13.0
C ₂₆	2.8	11.8
C ₂₇	1.6	9.8
C ₂₈	0.9	7.5
C ₂₉	0.5	5.5
C ₃₀	0.3	3.9
C ₃₁	0.1	2.8
C ₃₂	0.1	1.9
C ₃₃		1.3
C ₃₄		0.9
C ₃₅		0.6
C ₃₆		0.5
C ₃₇		0.3
C ₃₈		0.2
C ₃₉		0.2
C ₄₀₊	—	<u>0.3</u>
Total	100.0 Area %	100.0 Area %

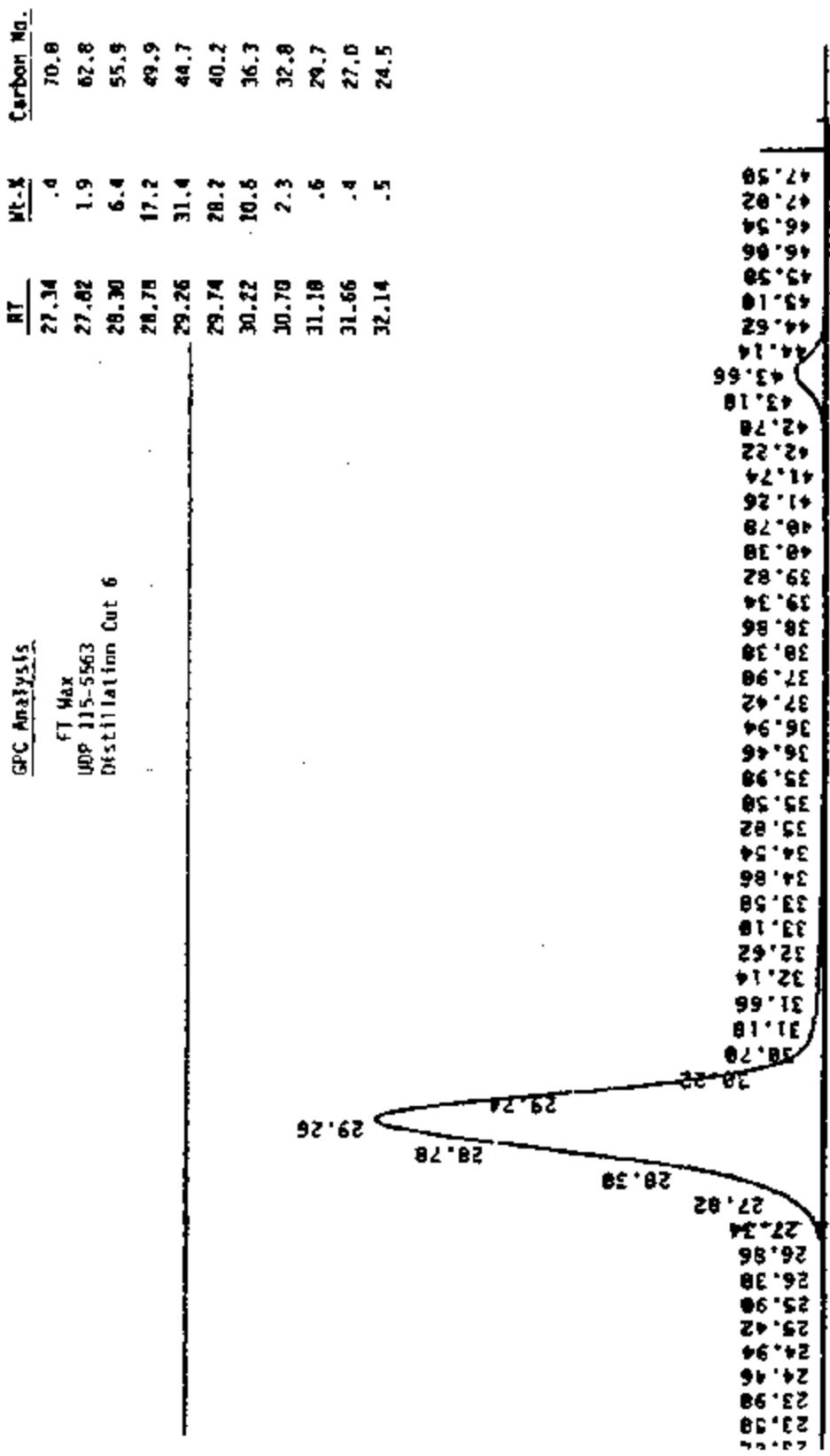




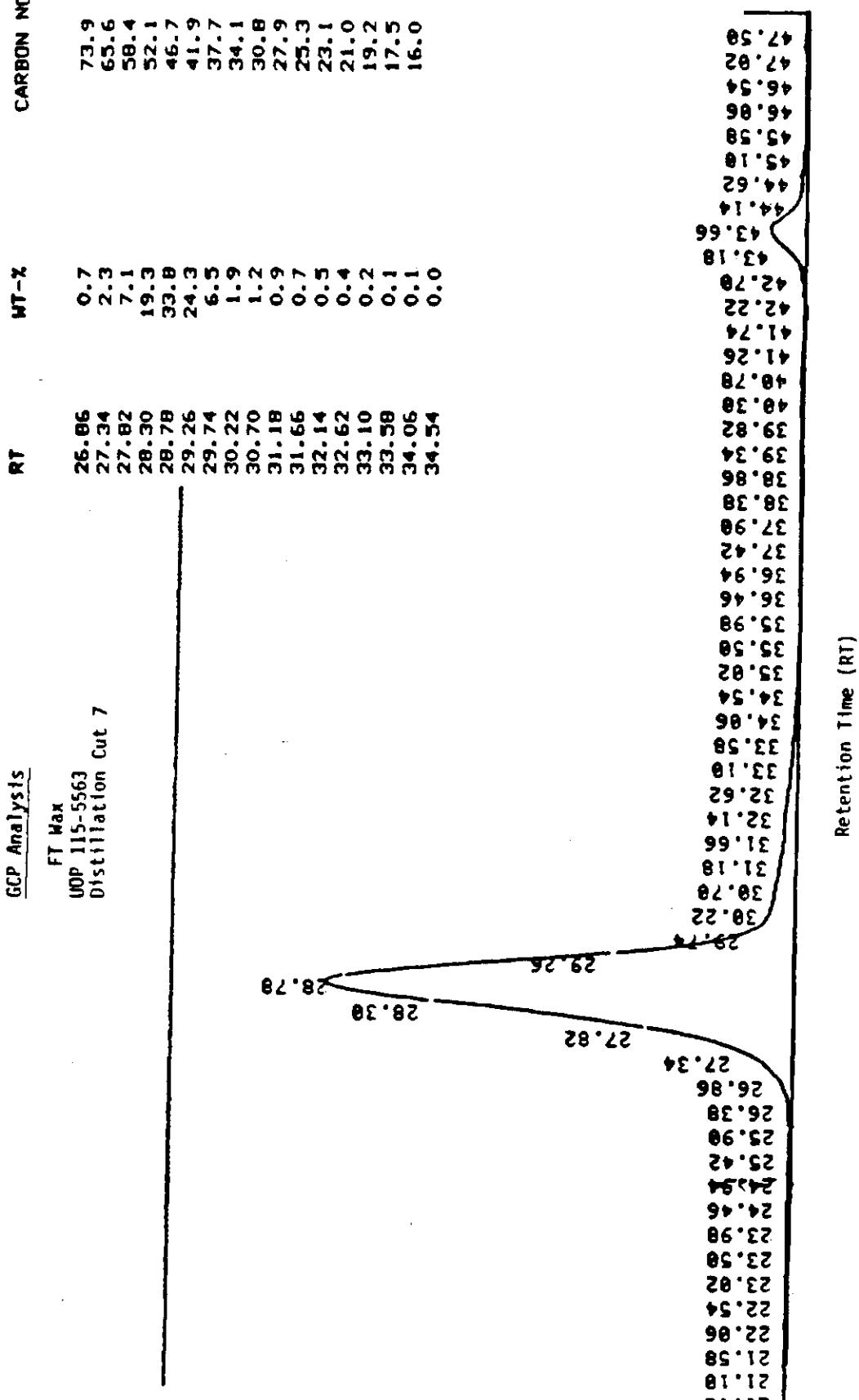
A-6

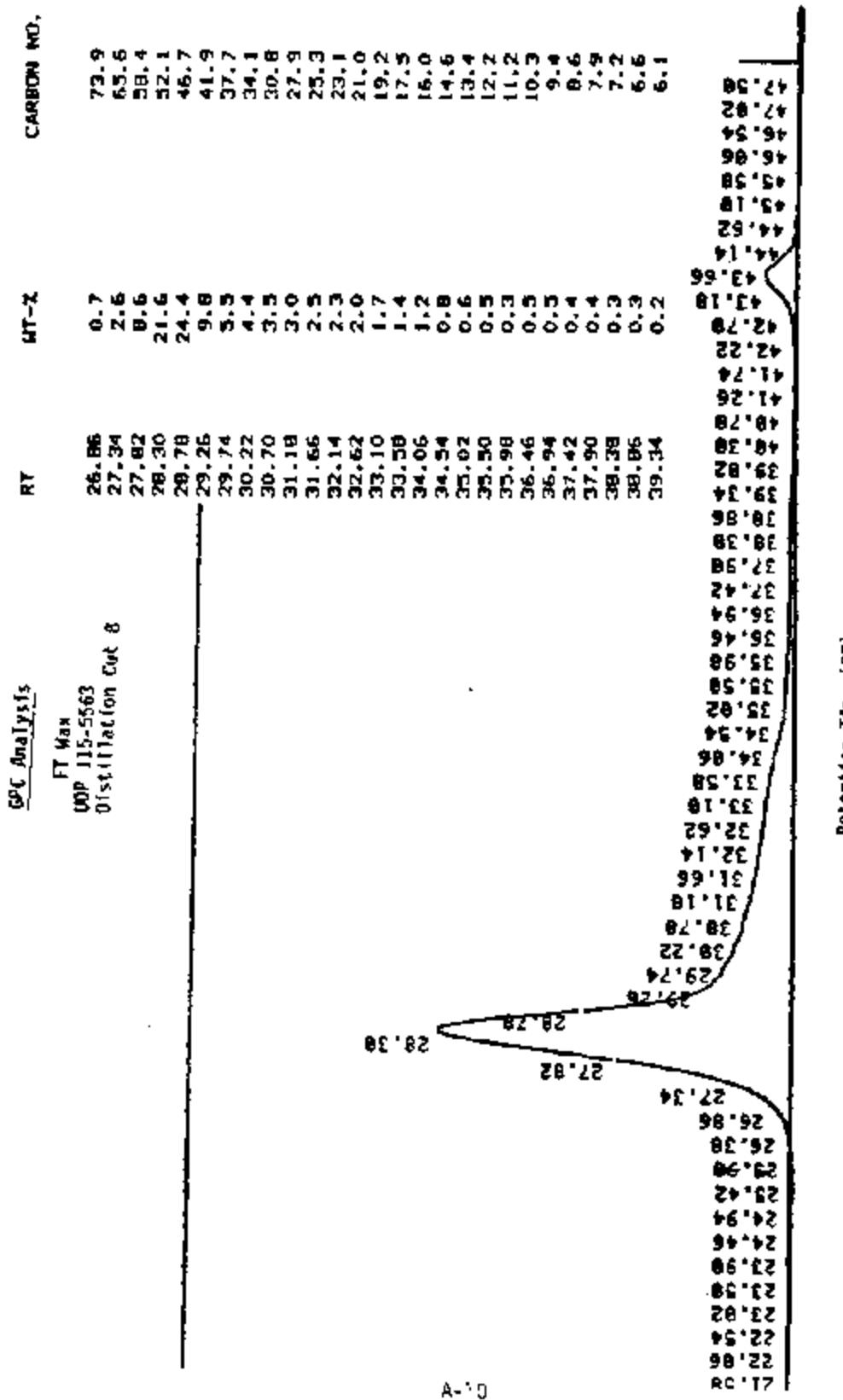


Retention Time (RT)

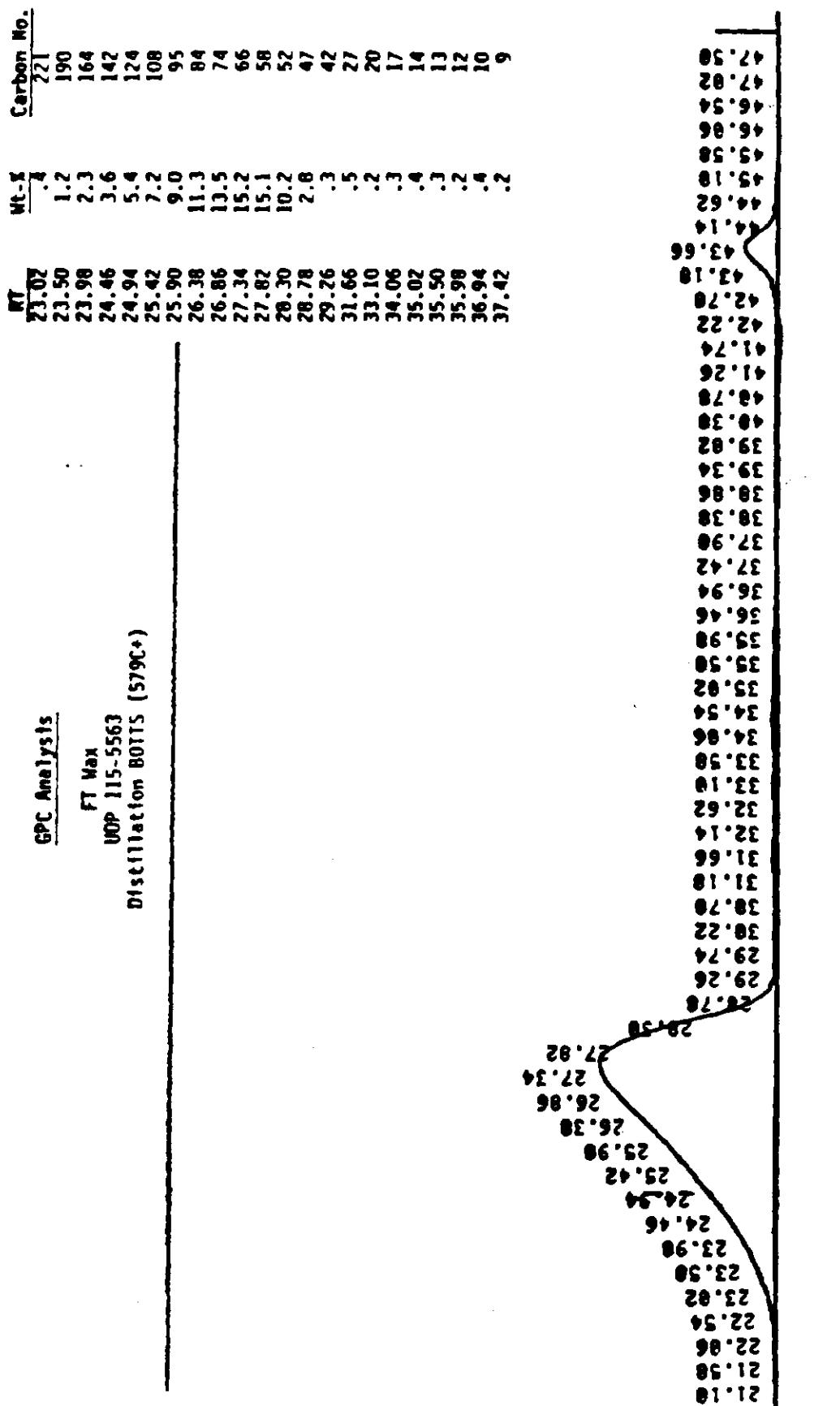


A-B

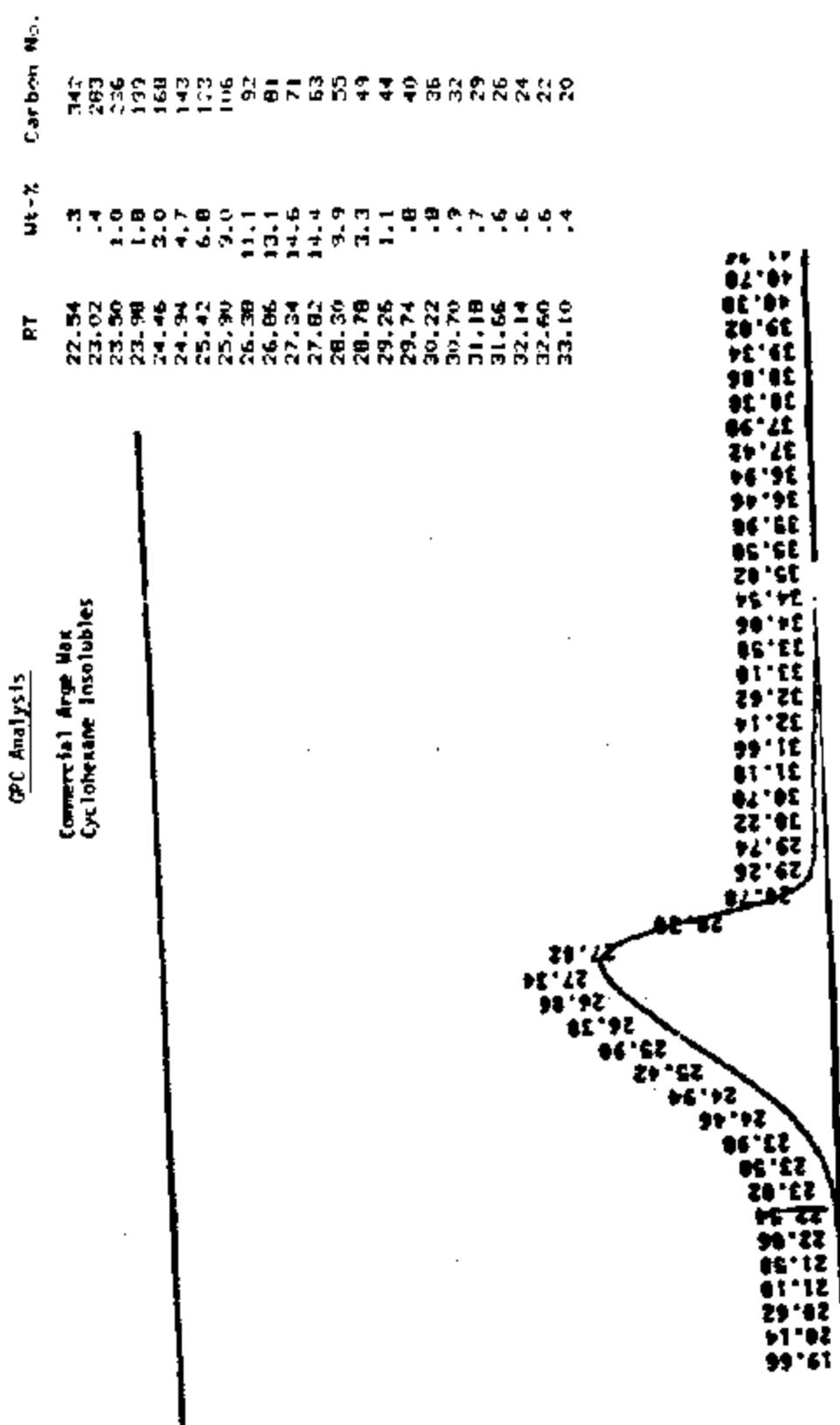




GPC Analysis
 FT Max
 UOP 115-5563
 Distillation Bottles (57°C+)



Retention Time (RT)



FT Wt-% Carbon No.

24.17 .1 200

24.47 .2 101

24.77 .4 165

25.07 .7 150

25.37 1.0 137

25.67 1.5 125

25.97 2.0 115

26.27 2.6 105

26.57 3.2 97

26.87 4.0 90

27.17 4.8 83

27.47 5.7 77

27.77 6.7 71

28.07 7.6 66

28.37 8.3 61

28.67 8.9 57

28.97 8.0 53

29.27 6.2 50

29.57 4.6 46

29.87 4.0 43

30.17 3.6 40

30.47 3.4 38

30.77 3.1 35

31.07 2.8 33

31.37 2.4 31

31.67 1.8 29

31.97 1.2 28

32.27 1.6 26

32.57 1.3 25

32.87 1.2 23

33.17 1.1 22

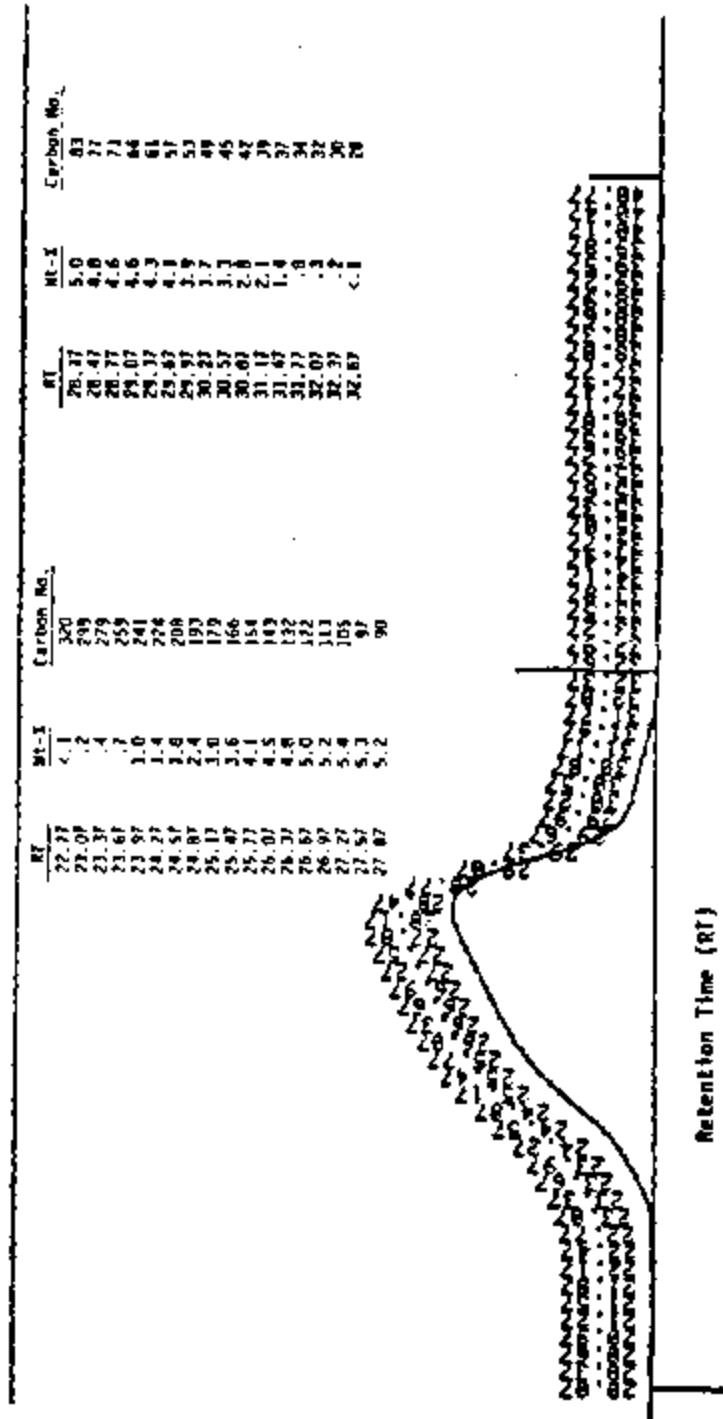
GPC Analysis

Union Carbide Wax
Cyclohexane Insolubles

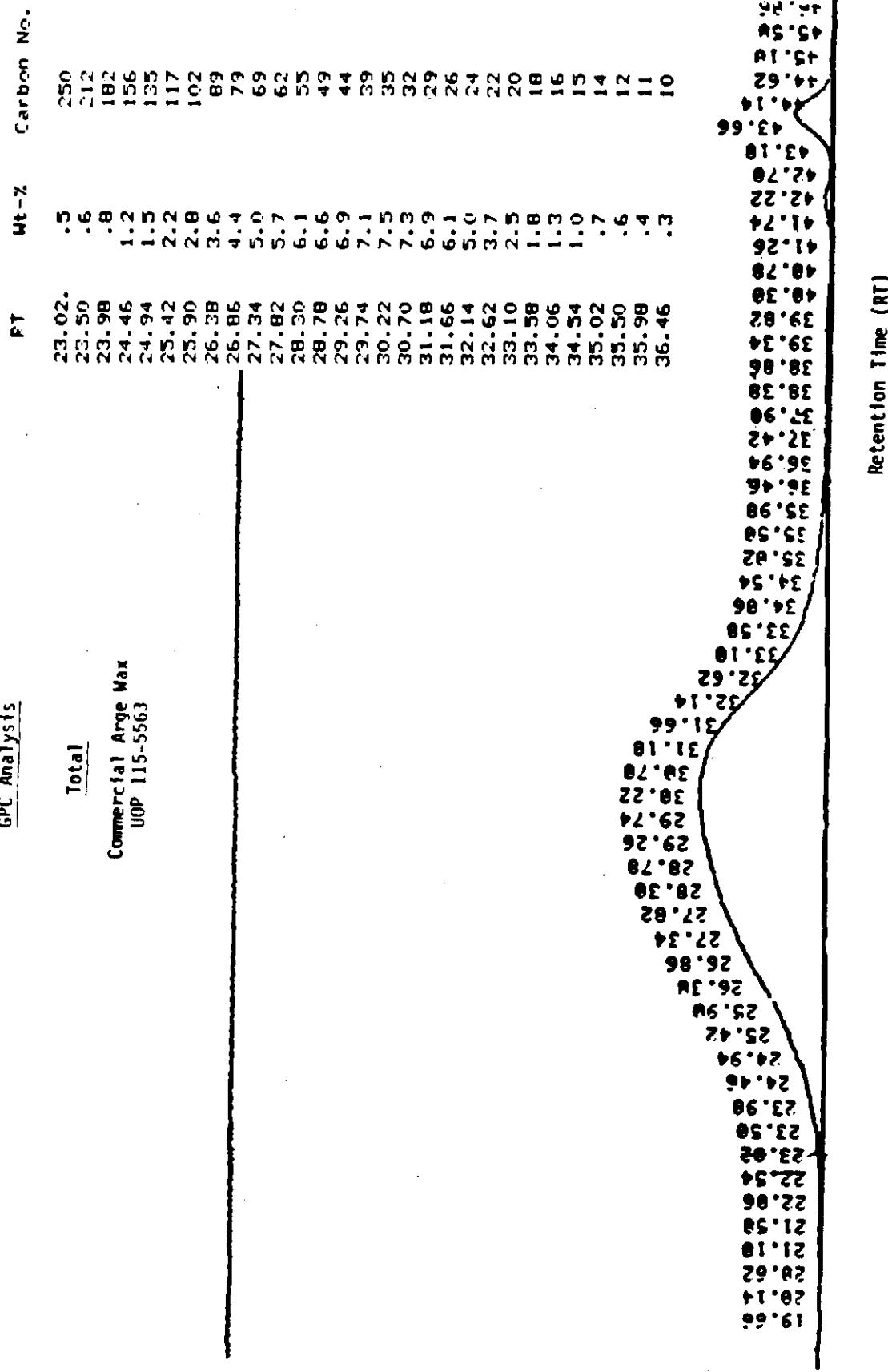
Retention Time (RT)

GPC Analysis

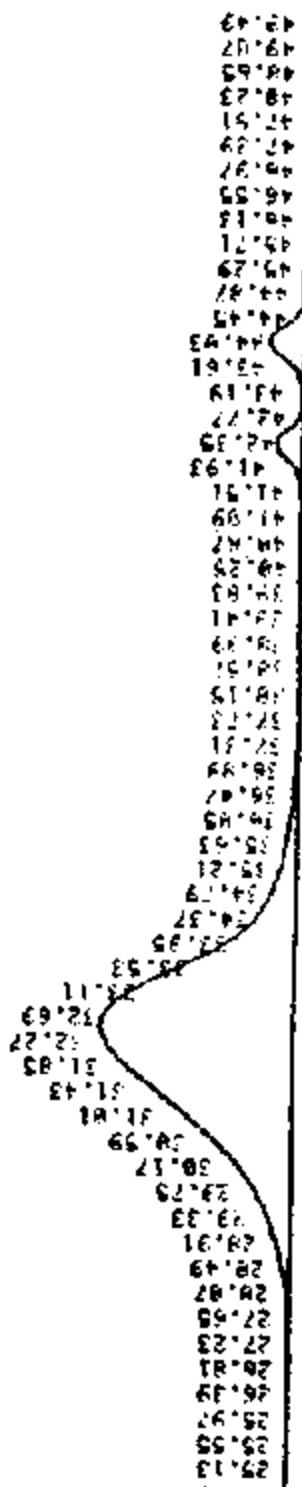
**Mobility Max
Cyclohexane Insolubles**



GPC Analysis



Retention Time (RT)

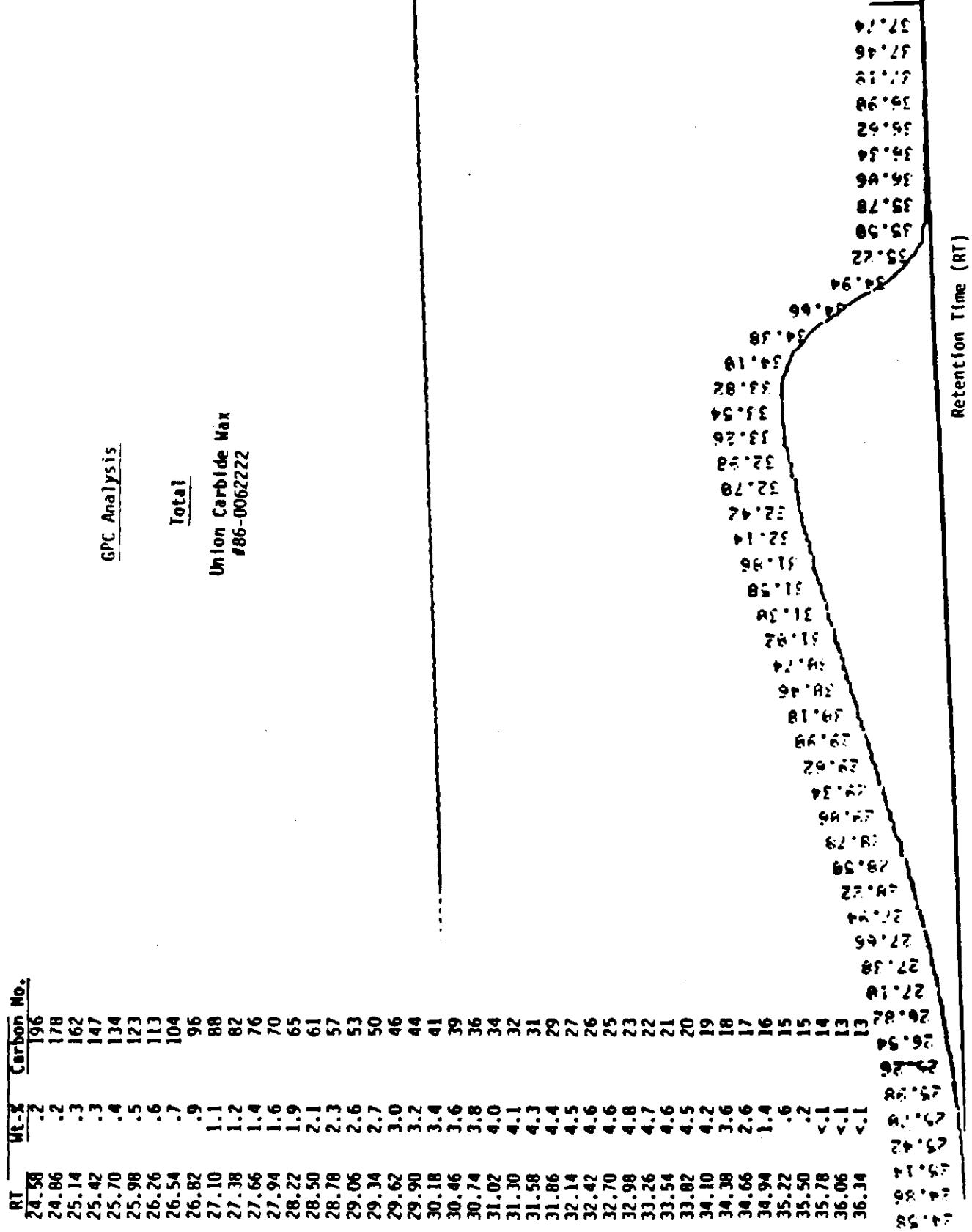


GPC Analysis

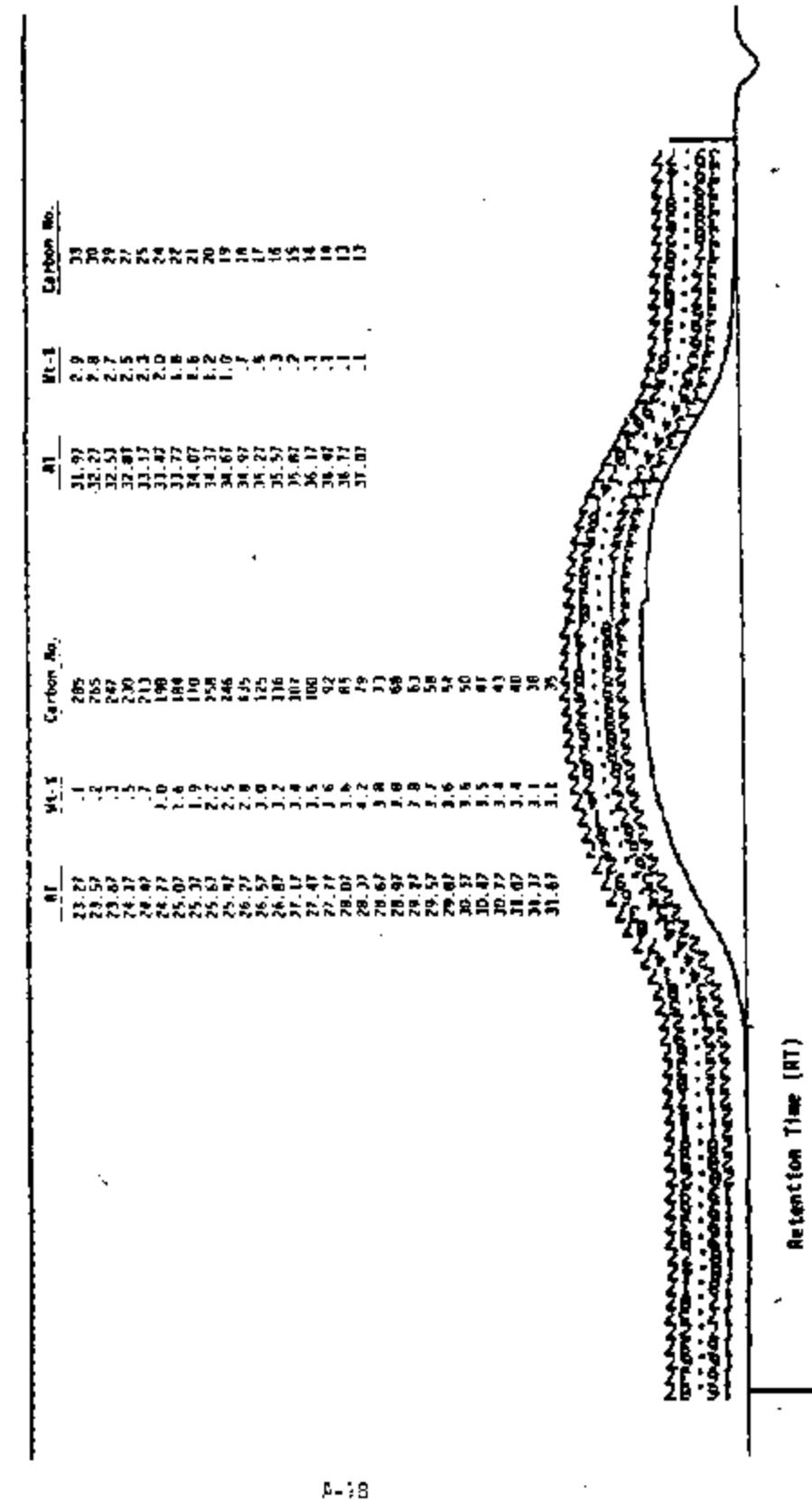
Total

Air Products Max
WOP 49-2920

RT Wt-% Carbon No.



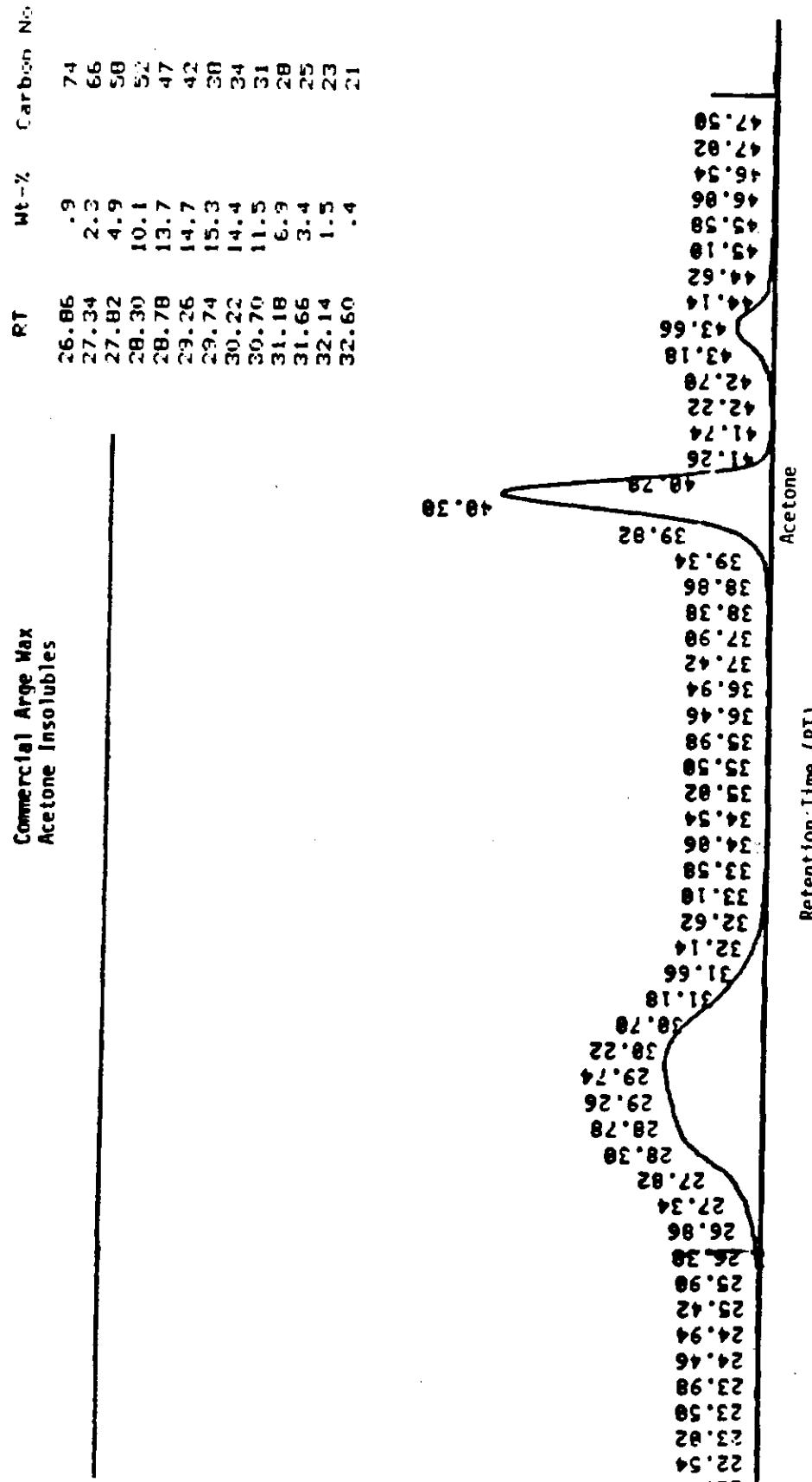
GPC Analysis
Nobit Yar



A-10

GPC Analysis

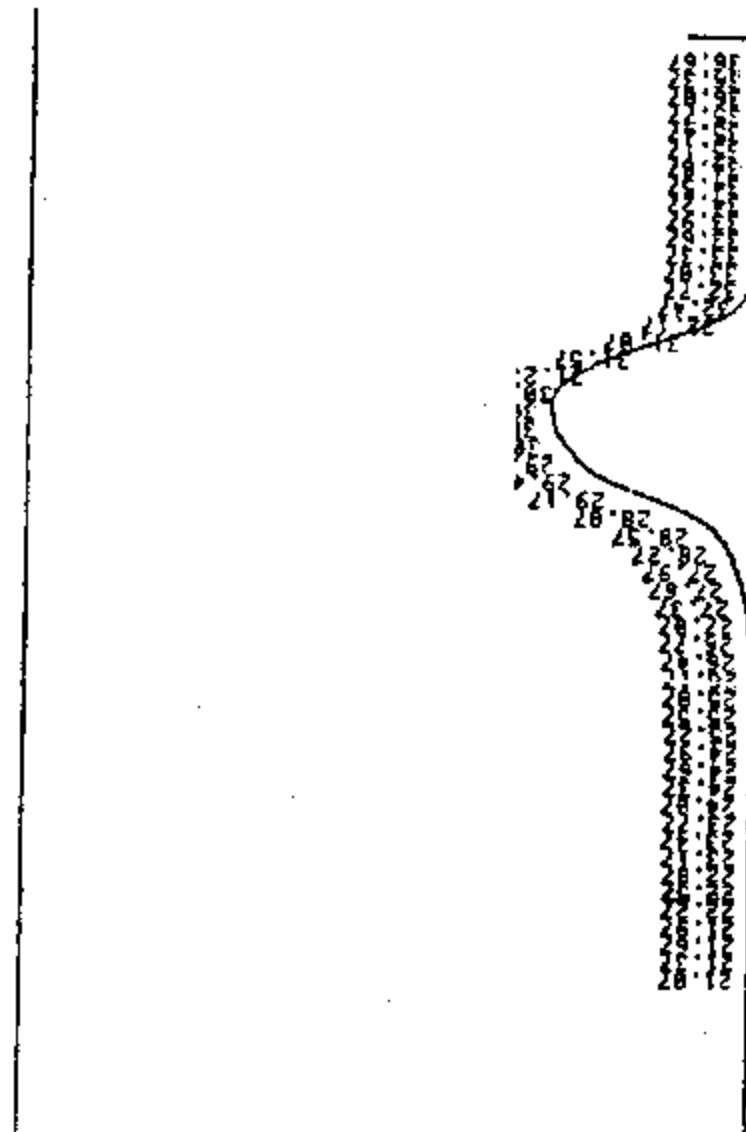
Commercial Arge Wax
Acetone Insolubles



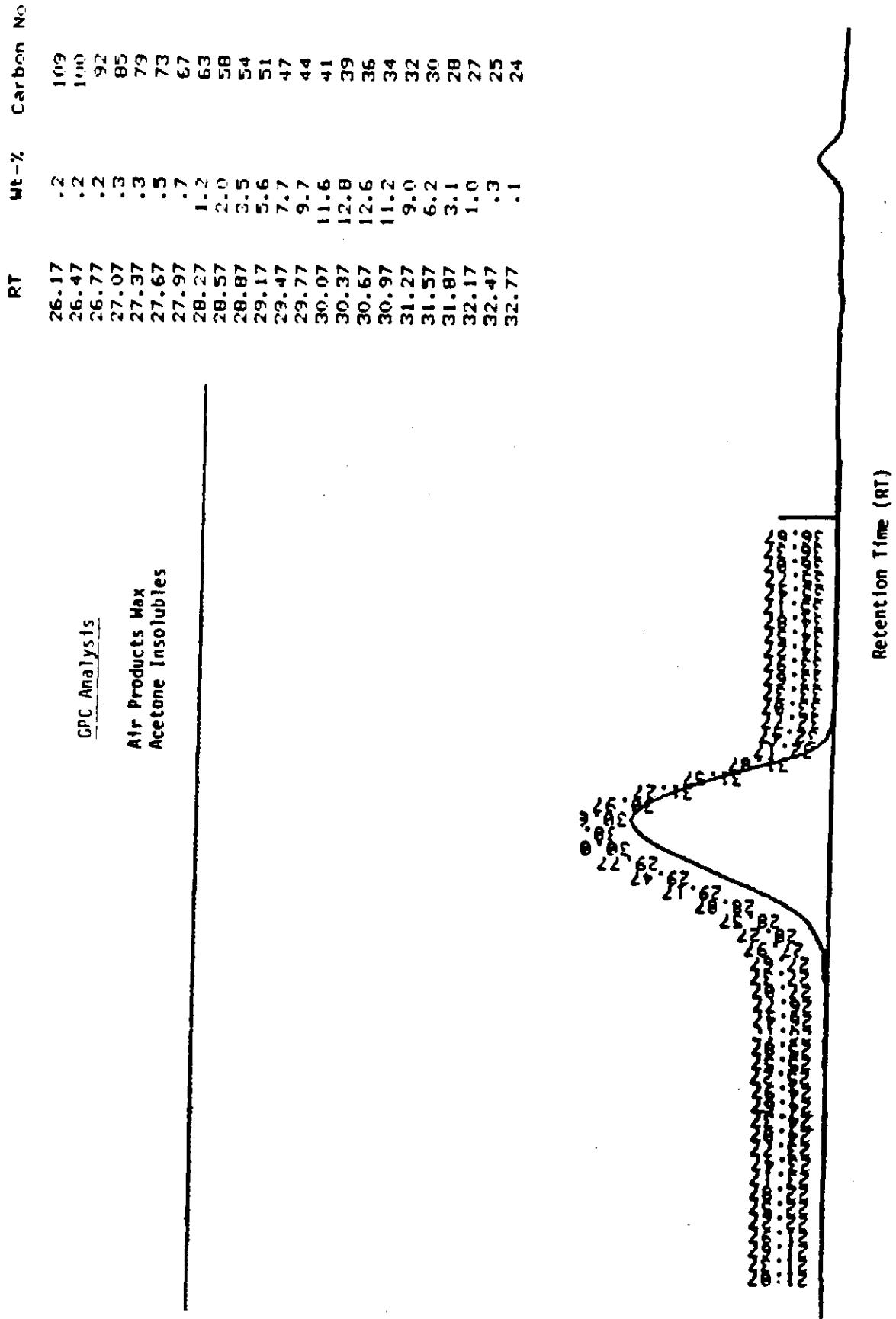
	RT	MS-2	Carbon No.
	26.77	.1	92
	27.07	.2	85
	27.37	.3	79
	27.67	.9	73
	27.97	1.2	67
	28.27	1.7	63
	28.57	2.5	58
	28.87	4.0	54
	29.17	6.4	51
	29.47	8.5	47
	29.77	3.7	44
	30.07	10.4	41
	30.37	10.5	39
	30.67	10.6	36
	30.97	10.0	34
	31.27	8.6	32
	31.57	6.6	30
	31.87	4.2	28
	32.17	2.0	27
	32.47	.8	25
	32.77	.3	24
	33.07	.2	22
	33.37	.1	21
	33.67	.1	20

GPC Analysis

Union Carbide Man
Acetone Insolubles

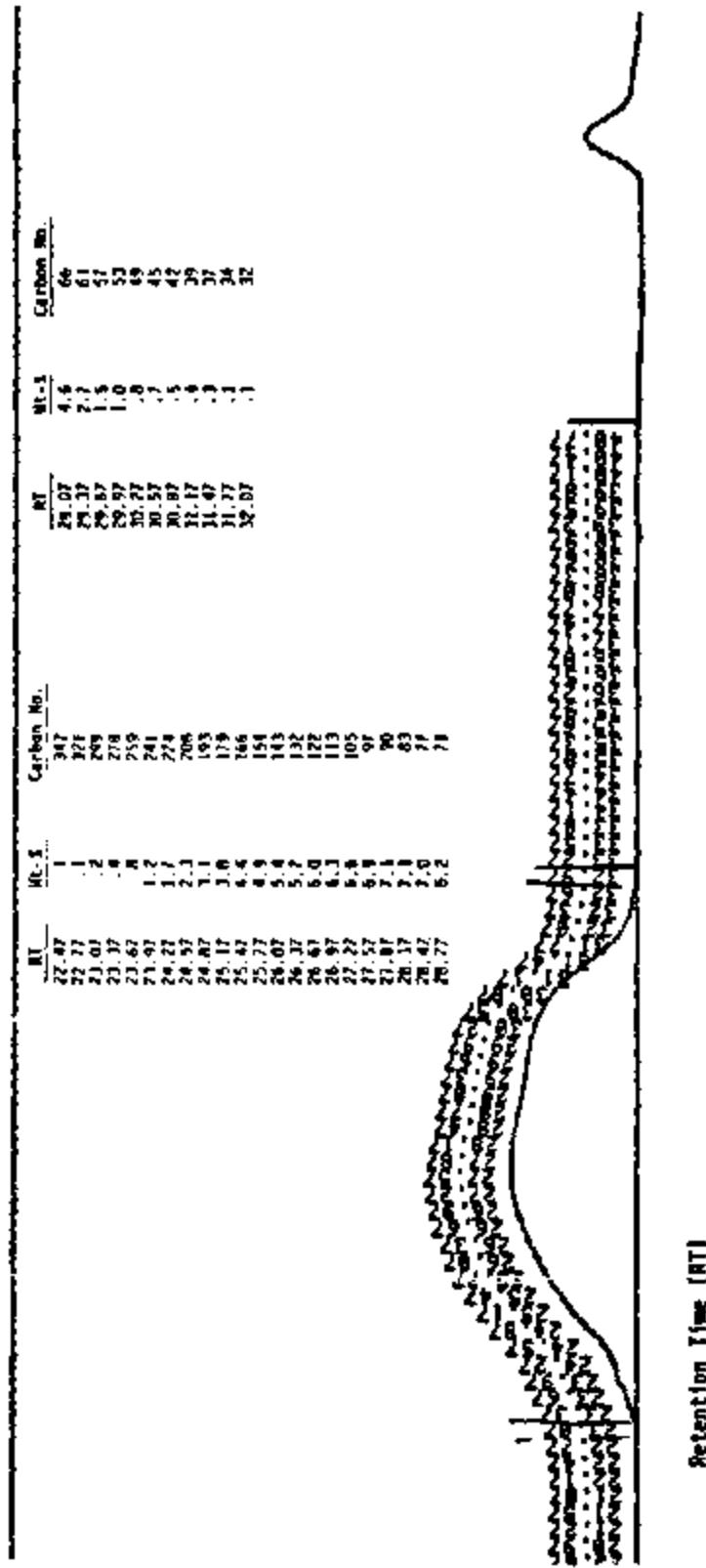


Retention Time (RT)



GPC Analysis

Mohr Wake
Acetone Insolubles



Size Exclusion - Chromatographic Separation of Fischer-Tropsch Waxes (II) (Correction of Retention Times for Calibrations)

INTRODUCTION

Since the release of the memo "Size Exclusion-Chromatographic Separation of Fischer-Tropsch Waxes" addressed to Hayim Abrevaya dated April 14, 1986, it was discovered that when calibration retention times were measured using the Waters model 730 Data Module in the calibration mode, faulty retention times were provided.

The following report contains corrected calibrations.

EXPERIMENTAL

It was found that when the Model 730 Waters Data Module was used in the calibration mode, with the chart speed set at 1 cm/min., a run time of 50 minutes had a pen trace of 50.5 cm. This was 0.99 minutes per centimeter. When the Data Module was placed in the analysis mode the pen trace for a 50 minute run time measured 50 centimeters.

Some of the calibrations in the April 14, 1986 report were made where the retention times had been measured in the calibration mode.

Results appearing in the following report were obtained using corrected retention times for the calibrations.

A 50 μ l aliquot of a 0.25 percent solution of a Fischer-Tropsch wax in ODCB was separated on a set of ASI Ultragel 2-500A, 2-100 Å 30 cm x 7.8 mm columns using a Waters ALC/GPC Model 150C Chromatograph.

Separations were made using ODCB as the eluent with the columns, differential refractometer and the injector maintained at 100°C. The flowrate was set at 4.8/5.0 mL/min. A Waters Model 730 Data Module was used to monitor the detector response. The chart speed was set at 1 cm/min.

The chromatograph of a Fischer-Tropsch wax is shown in Figure 1.

In order for the chromatogram to be of any value, the retention times had to be correlated with the carbon number. Individual samples with known carbon numbers were analyzed. Results are shown in Table 1. A plot of these values is found in Figure 2.

It was noted that for the carbon range of C₆ to C₆₀, the plot was not linear. The carbon numbers and their respective retention times were entered into a Waters Model 730 Data Module, and the third order fit calibration coefficients were calculated using the following formula where:

$$\log CN = D_0 + D_1 RT + D_2 (RT)^2 + D_3 (RT)^3$$

The calibration coefficients are shown in Table 2.

The individual retention times for the standards were manually reentered into the Data Module. The resulting carbon numbers obtained from the retention time input are shown in Table 3. The calculated carbon numbers agreed favorably with the actual carbon numbers.

In order to verify the Waters Data Module calibrations, a least squares fit plot of the retention times vs. carbon numbers was plotted using the Hewlett Packard Model 3357 laboratory automation system. The plot is shown in Figure 3. The calculated carbon numbers were determined using the formula where:

$$C = (1.68352E+11) \times T^{-6.53713}$$

Results are shown in Table 4.

Like the results obtained using the Waters Data Module, the Hewlett Packard calculated values agreed favorably with the actual carbon numbers. The Waters Data Module calibration was used for all analyses.

An attempt was made to extend the range of the carbon number calibration. Aliquots of solutions of Apolane-87, a branched 87 carbon number and polyethylene with a number average molecular weight of 2015 and a calculated carbon number of 143.9 were analyzed in addition to the linear alkanes. The retention times were correlated with the carbon numbers as shown in Table 5.

A plot was made of the values presented in Table 5. The results are shown in Figure 4.

From the above plot it was shown that Apolane-87, a branched 87 carbon number eluted later than when a corresponding linear C₈₇ alkane would elute. However the polyethylene with a number average molecular weight of 2015 and a calculated carbon number of 143.9 fit in the plot of the linear alkanes.

The third order calibration coefficients were calculated for the extended range calibration. Results are shown in Table 6. The individual retention times for the standards were manually reentered into the Data Module. The resulting carbon numbers obtained from the retention time input are shown in Table 7. The calculated carbon numbers agreed favorably with the actual carbon numbers.

The Waters Data Module calibration coefficients for carbon number range of 6-60 shown in Table 8 were used to calculate the results for the was sample shown in Figure 1. Area percentages and carbon numbers were correlated by utilizing the area percents vs. retention times from Table 9 and the carbon numbers vs. retention times found in Table 10.

It has been known that the refractive indices change from compound to compound. Therefore, in order to report concentrations of carbon number as weight percent, response factors for the carbon range relating area to weight had to be determined.

Aliquots with known weights of the individual alkane standards were analyzed. The weight per unit area for the standards were calculated. Results are shown in Table 11.

A plot of the above values in Figure 5 showed a sharp rise of the picogram per unit area from carbon number 12 to 30. From 30 on the curve started to level off.

Using the above correlation between picogram per area vs. carbon number, CHPfeiffer wrote a program for the Hewlett Packard Model 3357 Laboratory Automation system, whereby the area percentages could be converted to weight percent. The corrected area was calculated by using the following formula.

$$A_c = A \times \frac{C}{0.314 + (0.0198 \times C)}$$

The carbon numbers and their respective area percents for the sample shown in Figure 1 were entered into the program.

The resulting weight percents were calculated. Results are shown in Table 12.

CONCLUSIONS

From the work done, it was found that the carbon number range and weight percent for various Fischer-Tropsch wax fractions could be determined by size exclusion chromatography. Two calibrations were essential for the analysis. The first was the third order fit correlating the retention times vs. carbon number and the second one correlating the weight to area response over the carbon number range.


R. F. Swensen

DC/16

ODCB = ortho di-chloro benzene

TABLE I

ULTRAGEL

Calibration of Ultragel 2-500, 2-100 Å Columns Using
Linear Alkanes as Standards

RT MIN	CM
27.90	60
28.60	50
29.20	44
30.10	36
30.60	32
31.30	28
32.10	24
32.60	22
33.00	20
33.60	18
34.30	16
34.90	14
35.70	12
39.40	6

TABLE 2

Calculation of Third Order Fit Calibration
Coefficients Using a Waters Model 740 Data Module

GPC CALIBRATION
NUMBER OF STANDARDS: 14

RT	CN X 10 ³	LOG CN x 10 ³
27.90	8.600000E5	4.778
28.60	6.500000E5	4.658
29.20	8.400000E5	4.643
30.10	6.360000E5	4.556
30.50	9.320000E5	4.585
31.30	9.280000E5	4.447
32.10	9.240000E5	4.380
32.50	8.220000E5	4.342
33.00	8.200000E5	4.341
33.60	8.180000E5	4.255
34.30	8.160000E5	4.204
34.90	8.140000E5	4.146
35.70	8.120000E5	4.079
39.40	8.600000E4	3.778

CALIBRATION COEFFICIENTS

D0 8.139140600000E2
D1 -8.572161000000E0
D2 0.167675000000E-1
D3 -8.156311000000E-3

STD ERR OF ESTIMATE 8.324363E-1
CORR COEFFICIENT 8.392685E0

TABLE 3

Comparison of the Calculated Carbon Number from the
Waters Model 730 Data Module 3rd Order Fit vs.
the Actual Carbon Number

RT Min	ACTUAL CN	Calculated CN Via Entering RT
27.90	60	59.5
28.60	50	50.3
29.20	44	43.85
30.10	36	35.99
30.60	32	32.38
31.30	28	28.0
32.10	24	23.9
32.60	22	21.7
33.0	20	20.1
33.6	18	17.9
34.30	16	15.75
34.90	14	14.09
35.70	12	12.16
39.40	6	5.99

TABLE 4

Comparison of the Calculated Carbon Number from
The Hewlett Packard Model 3357 Laboratory Automation
System vs. the Actual Carbon Number

$$C = (1.68352 \times 10^{11}) \times T^{-6.53713}$$

Details for curve type (1-6/7-PLOT/0-END)? 3

3. Y=F-(X^E) IS A POWER FUNCTION. THE RESULTS
OF A LEAST-SQUARES FIT OF ITS LINEAR TRANSFER
(SORTED IN ORDER OF ASCENDING VALUES OF X)
ARE AS FOLLOWS:

X-ACTUAL	Y-ACTUAL	Y-CALC	FCT DIFFER
27.6	60	55.72	.4
28.6	50	50.78E3	-1.5
29.2	44	44.34E3	-.7
30.1	36	38.38E16	-.8
30.8	32	32.64E	-1.6
31.3	28	28.1E16	-.5
32.1	24	23.67E5	.5
32.6	22	21.58E6	1.5
33.	20	19.62E6	.5
33.6	18	17.71E6	1.8
34.3	16	15.48E6	3.6
34.9	14	13.82E6	1.2
35.7	12	11.91E6	.6
36.4	8	8.2554E	-4

14	34.5	14
15	35.7	12
16	39.4	6

Modifications (Y/N)? N

outdvc? T4

LEAST SQUARES CURVE FIT

CURVE TYPE	INDEX OF DETERMINATION	F	E
1. Y=F+(E*X)	.867816	177.46E	-4.83E33
2. Y=F+EXF(E*X)	.999254	14290.6	-1.19E384
3. Y=F-(X^E)	.699367	1.68352E+11	-6.53713
4. Y=F+(E/X)	.9318E5	-1.33E41E	51E0.04
5. Y=1/(F+E*X)	.894E7	-1.32E167	1.15E36E-02
6. Y=1/(A+E*X)	.80EE16	-11.6932	.4222E9

TABLE 5

ULTRAGEL

Extended Calibration of Ultragel 2-500, 2-100 & Columns Using
Polyethylene and Apolane-87 in Addition to the Linear Alkanes

RT MIN	CN	
24.6	143.9	Polyethylene
27.0	87	Apolane-87
27.7	60	
28.5	50	
29.1	44	
29.9	36	
30.5	32	
31.2	28	
32.0	24	
32.4	22	
32.9	20	
33.5	18	
34.1	16	
34.8	14	
35.6	12	
39.2	6	

TABLE 6

Calculation of Third Order Fit Calibration
Coefficients for an Extended Carbon Number Range
Using a Waters Model 730 Data Module

GPC CALIBRATION
NUMBER OF STANDARDS: 15

RT	MOL WT	LOG MW
24.60	8.143900E6	5.158
27.70	8.600000E5	4.778
28.50	8.500000E5	4.698
29.10	8.440000E5	4.643
29.90	8.360000E5	4.556
30.50	8.320000E5	4.505
31.20	8.260000E5	4.447
32.00	8.240000E5	4.380
32.40	8.220000E5	4.342
32.90	8.206000E5	4.301
33.50	8.180000E5	4.255
34.10	8.160000E5	4.204
34.80	8.140000E5	4.146
35.60	8.120000E5	4.079
39.20	8.600000E4	3.778

CALIBRATION COEFFICIENTS

D0 8.146134990000E2
D1 -8.743032300000E0
D2 8.190661700000E-1
D3 -8.183248900000E-3

STD ERR OF ESTIMATE 8.181333E-1
CORR COEFFICIENT 8.998485E0

TABLE 7

Comparison of the Calculated Carbon Number From the
Waters Model 730 Data Module 3rd Order Fit Using an
Extended Carbon Number Calibration vs. the Actual Carbon Number

RT Min	ACTUAL CN	Calculated CN Via Entering RT
24.60	143.9	143.5
27.70	60	60.4
28.50	50	49.8
29.10	44	43.4
29.90	36	36.4
30.50	32	32.1
31.20	28	27.8
32.00	24	23.8
32.4	22	21.99
32.90	20	19.99
33.50	18	17.86
34.10	16	15.97
34.80	14	14.03
35.6	12	12.1
39.20	6	5.98

TABLE 8

Third Order Fit Calibration Coefficients
Used for the Calculations for Sample Shown in Figure 1

GPC CALISRATION
NUMBER OF STANDARDS: 7

PT	MOL WT	LOG MW
28.00	8.60000E5	4.778
28.70	8.50000E5	4.698
29.30	8.44000E5	4.643
30.20	8.36000E5	4.556
34.30	8.16000E5	4.204
35.90	8.12000E5	4.079
39.40	8.60000E4	3.778

CALIBRATION COEFFICIENTS
D0 8.1576611890000E2
D1 -8.8341480000000E8
D2 8.2178869000000E-1
D3 -8.208451000000E-3

STD ERR OF ESTIMATE 8.448956E-1
CORR COEFFICIENT 8.992795E0

TABLE 5
 Correlation of Area Percent vs. Retention Time
 For Fischer-Tropsch Wax Shown in Figure 1

EXTERNAL STANDARD QUANTITATION

PEAK #	AMOUNT	RT	%
1	0.00300	20.14	0.00
3	0.00300	21.10	0.00
4	0.00300	21.50	0.00
5	30.15400	22.06	0.48
6	54.79200	22.54	0.56
7	111.87000	23.02	1.19
8	175.31100	23.50	1.86
9	238.83900	23.98	2.54
10	327.77700	24.46	3.49
11	437.29500	24.94	4.66
12	563.67300	25.42	5.36
13	531.23100	25.90	5.66
14	547.63200	26.38	5.83
15	549.63000	26.86	5.65
16	538.62800	27.34	5.65
17	514.86600	27.82	5.48
18	462.39400	28.30	5.14
19	454.33500	28.78	4.84
20	418.17300	29.26	4.45
21	390.96100	29.74	4.16
22	345.63200	30.22	3.72
23	323.67000	30.70	3.44
24	305.37800	31.18	3.26
25	308.94900	31.66	3.29
26	320.53700	32.14	3.41
27	348.10500	32.62	3.71
28	333.51600	33.10	3.55
29	299.99400	33.58	3.19
30	214.66500	34.06	2.28
31	130.11300	34.54	1.38
32	74.36400	35.02	0.79
33	35.86200	35.50	0.38
34	28.53300	35.98	0.30
TOTAL	9381.10000		100.00

TABLE 10

Correlation of Carbon Numbers Obtained from
 The Waters Model 730 Data Module
 Third Order Fit vs. Retention Time
For the Fischer-Tropsch Wax Shown in Figure 1

GPC QUANTITATION

RT	WREN	CN X 10 ³	%CN X 10 ³	L
20.14	1	0.100160E7	0.998482E-6	L
21.10	1	0.634482E6	0.157688E-5	L
21.58	1	0.512037E6	0.195298E-5	L
22.06	12718	0.416869E6	0.305083E-1	L
22.54	18264	0.342235E6	0.533668E-1	L
23.02	37298	0.283289E6	0.131632E0	L
23.50	58437	0.236387E6	0.247209E0	L
23.98	79613	0.198679E6	0.400711E0	L
24.46	109259	0.168214E6	0.649523E0	L
24.94	145765	0.143438E6	0.101627E1	L
25.42	167891	0.123116E6	0.136368E1	L
25.90	177077	0.106302E6	0.166579E1	L
26.38	182544	0.923580E5	0.197648E1	L
26.86	183210	0.806731E5	0.227101E1	L
27.34	176876	0.708556E5	0.249626E1	L
27.82	171622	0.625261E5	0.274488E1	L
28.30	160798	0.554516E5	0.289979E1	L
28.78	151445	0.493729E5	0.306737E1	L
29.26	139391	0.441541E5	0.315692E1	L
29.74	130327	0.396282E5	0.328874E1	L
30.22	116544	0.356829E5	0.326610E1	L
30.70	107690	0.322399E5	0.334027E1	L
31.18	102126	0.292009E5	0.349735E1	L
31.66	102983	0.265200E5	0.388322E1	L
32.14	106779	0.241258E5	0.442592E1	L
32.62	116035	0.219874E5	0.527734E1	L
33.10	111172	0.200765E5	0.553741E1	L
33.58	99998	0.183511E5	0.544915E1	L
34.06	71555	0.167793E5	0.426448E1	L
34.54	43371	0.153568E5	0.282436E1	L
35.02	24788	0.148561E5	0.176350E1	L
35.50	11954	0.128676E5	0.928999E0	L
35.98	9511	0.117752E5	0.807714E0	L
NO-AUG		0.429977E5		
WT-AUG		0.761628E5		
Z-AUG		0.128865E6		
UIS-AUG		0.761493E5		
DISPERSITY		0.177132E1		
INTRINSIC VISCOSITY		0.761341E-1		

TABLE II

Comparison of the Weight to Differential Refractometer
Response for Carbon Number Range 12 to 60

5124-203
RI Weight to Area Response for Alkanes

C _N	PIC _{og} /A
60	39.8
50	38.8
44	37.7
36	34.9
32	34.2
28	31.5
24	30.4
22	29.4
20	27.3
18	26.7
16	25.4
14	23.8
12	21.9

TABLE 12

Conversion of Area Percent to Weight Percent
Using a Hewlett Packard Model 3357 Laboratory Automation System

Conversion of Area Percent to Weight Percent for Pit 700 R15 Wax
From Catalyst Outlet 5226-42-3

<u>CN</u>	<u>A%</u>	<u>Wt.%</u>
416.9	.4	.5
342.2	.58	.7
283.3	1.19	1.5
236.4	1.86	2.3
198.6	2.54	3.1
168.2	3.49	4.2
143.4	4.66	5.6
123.1	5.36	6.3
106.3	5.66	6.5
92.4	5.83	6.6
80.7	5.85	6.5
70.9	5.65	6.1
62.5	5.48	5.8
55.5	5.14	5.3
49.4	4.84	4.9
44.2	4.45	4.3
39.6	4.16	3.9
35.7	3.72	3.4
32.2	3.44	3.1
29.2	3.26	2.8
26.5	3.29	2.7
24.1	3.41	2.7
22.0	3.71	2.9
20.1	3.55	2.6
18.4	3.19	2.3
16.8	2.28	1.6
15.4	1.38	.9
14.1	.79	.5
12.9	.38	.2
11.8	.3	.2

FIGURE 1

Size Separation of a Fischer-Tropsich Mix

COLUMN: ASI Ultragel 2-500, 2-1000, 30cm x 7.8 mm

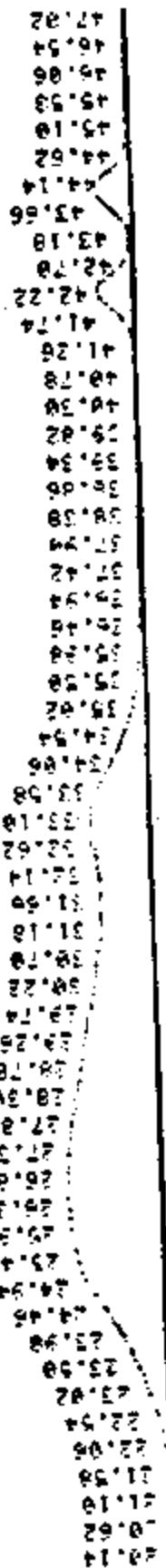
SOLVENT: Orthodichlorobenzene, 0008

TEMPERATURE: 100°C

DETECTOR: Diffr. Refractometer

FLOW RATE: 4.8/5.0 ml/min

CHART SPEED: 1 cm/sec



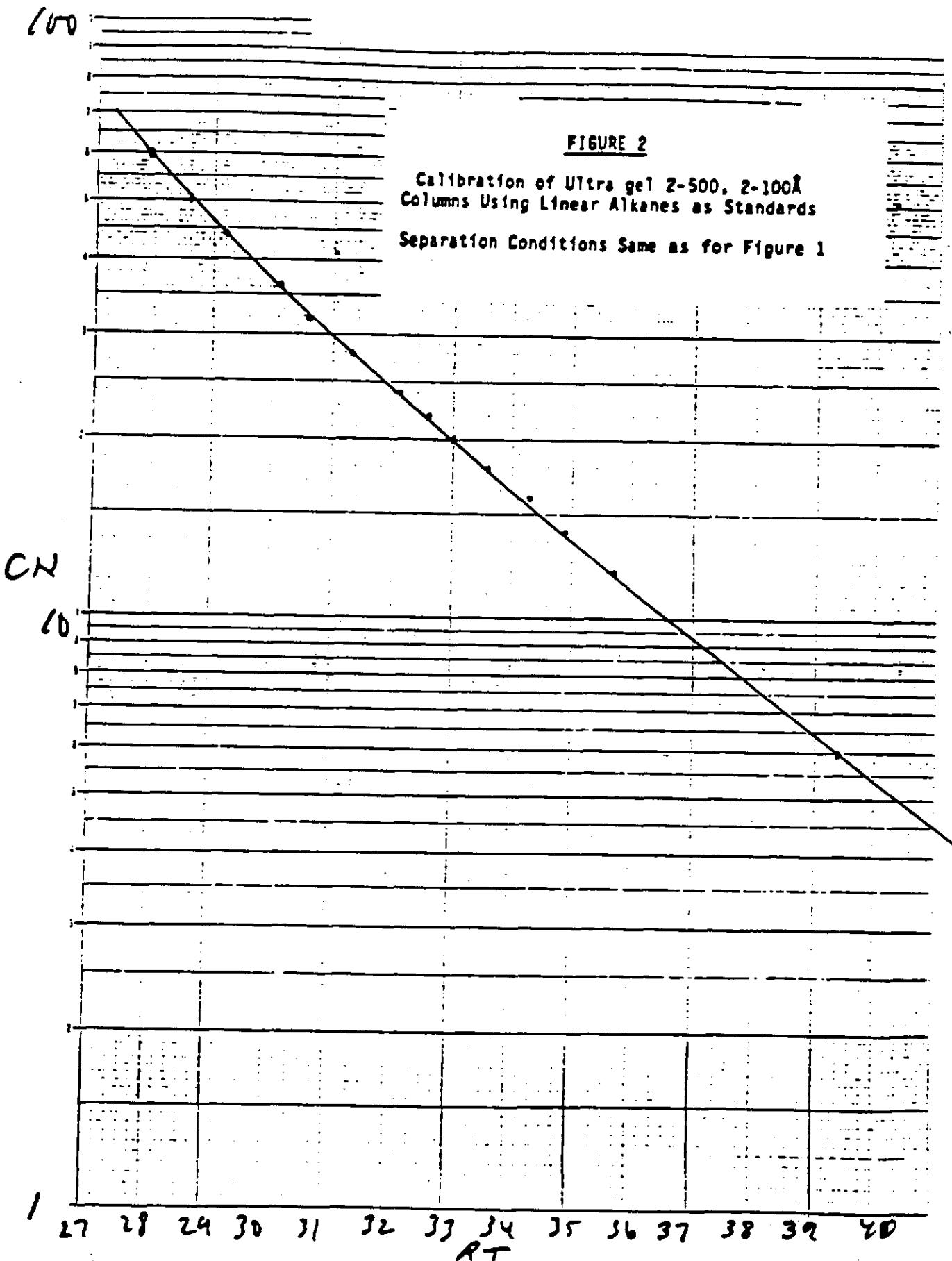


FIGURE 2

Calibration of Ultra gel 2-500, 2-100 Å
Columns Using Linear Alkanes as Standards

Separation Conditions Same as for Figure 1

FIGURE 3

Least Squares Curve Fit Plot of Carbon Number vs. Retention Time
Using the Hewlett Packard Model 3357 Laboratory Automation System

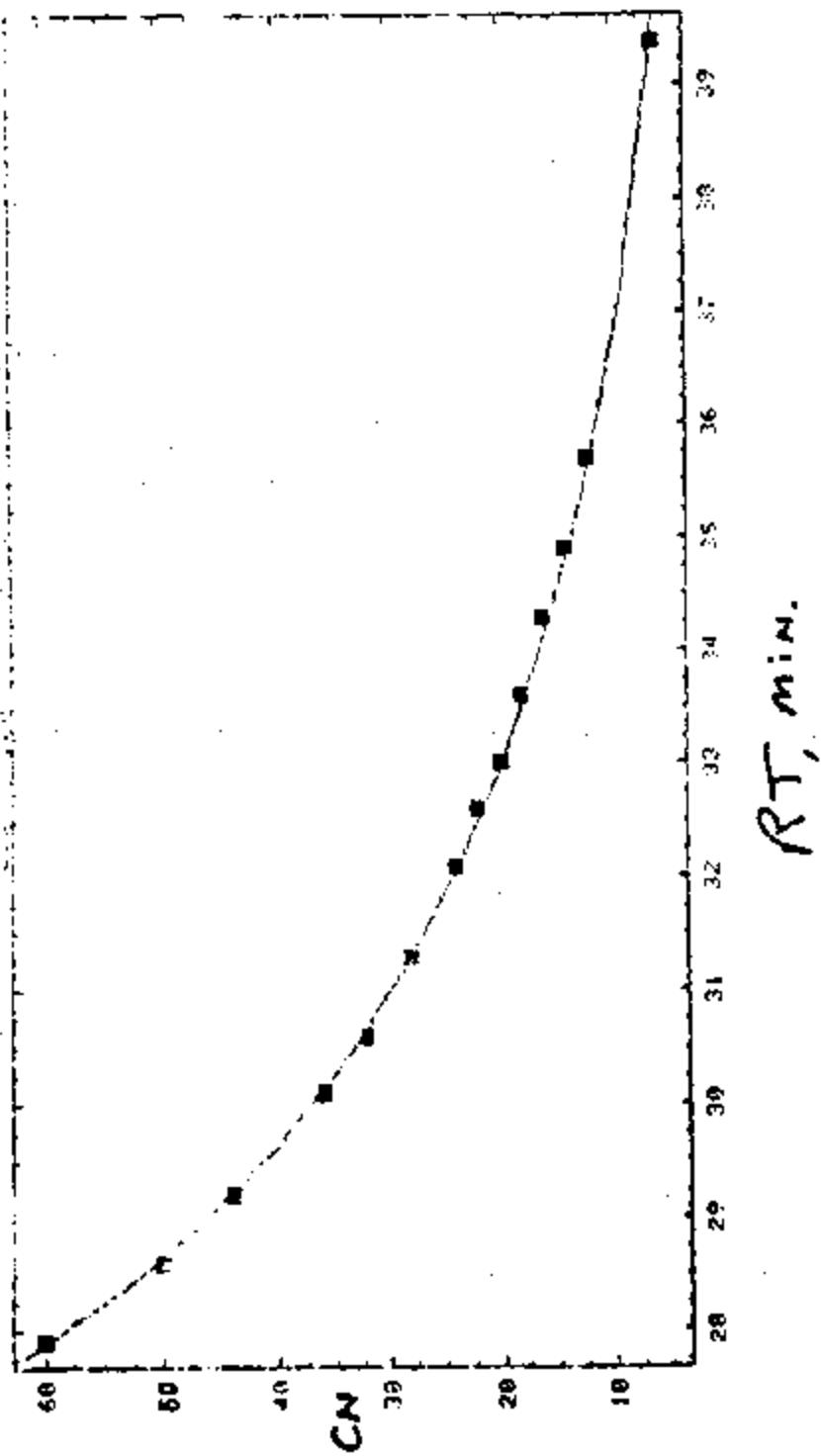


FIGURE 4

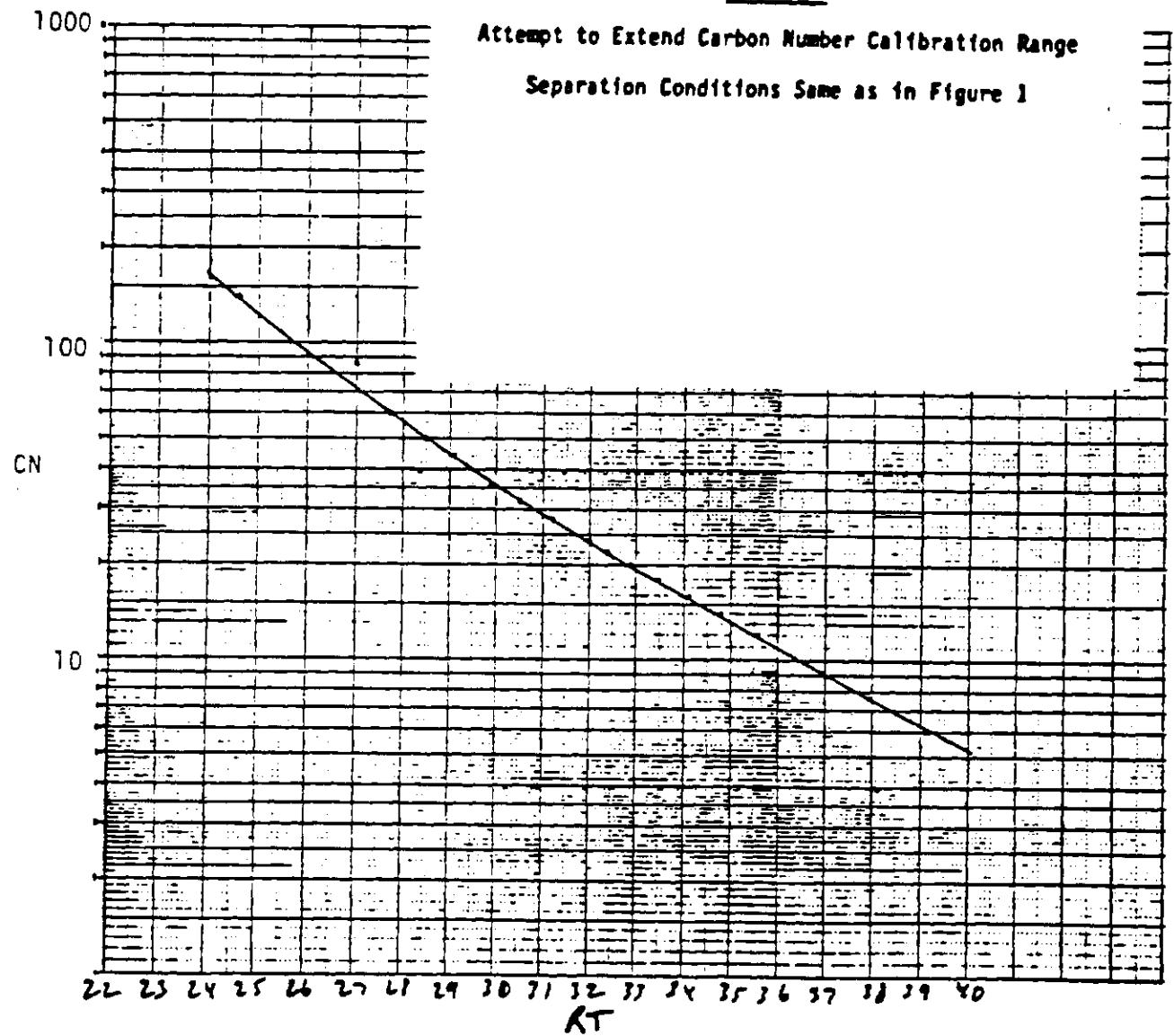


FIGURE 5

Plot of Weight to Differential Refractometer
Area Ratio vs. Carbon Number

