

of ~250 μ m. In the case of 304L stainless steel, the Cr and Ti concentrations were 46 wt% Cr and 40 wt% Ti, respectively, to a depth of 250 μ m. The Cr concentration in Alloy 8030 was in the range of 20-30 wt%, while the Cr content was similar to that of 304L stainless steel.

Specimens with pack-diffusion coatings were oxidized in air for 200 h at 800°C (1652°F) to develop the oxide scales and were exposed to Gas 2 in SMS® (1100°C) for 120 h in Run 27. Figures 60-61 show SEM photomicrographs of the surfaces of oxidized specimens after oxidation and oxidation/metal dusting treatments. Similar photomicrographs for the ChromePlated specimens are shown in Figs. 62-64. In general, the oxidized surface layers were intact after exposure to the metal dusting environment. There was some discoloration of the un-oxidized specimens after exposure to the carbonaceous atmosphere but detailed Starna analysis of the specimen surfaces showed almost no carbon. Additional long-term experiments are planned with several of the surface-modified alloys.

PROJECT SUMMARY

The deposition of carbon from carbonaceous gaseous environments is prevalent in many chemical and petrochemical processes, such as reforming cyclones, synthesis production systems, iron reduction plants, and others. One of the major consequences of carbon deposition is the degradation of structural materials by a phenomenon known as "metal dusting." There are two major issues of importance in metal dusting. First is formation of carbon and subsequent deposition of carbon on metallic materials. Second is the initiation

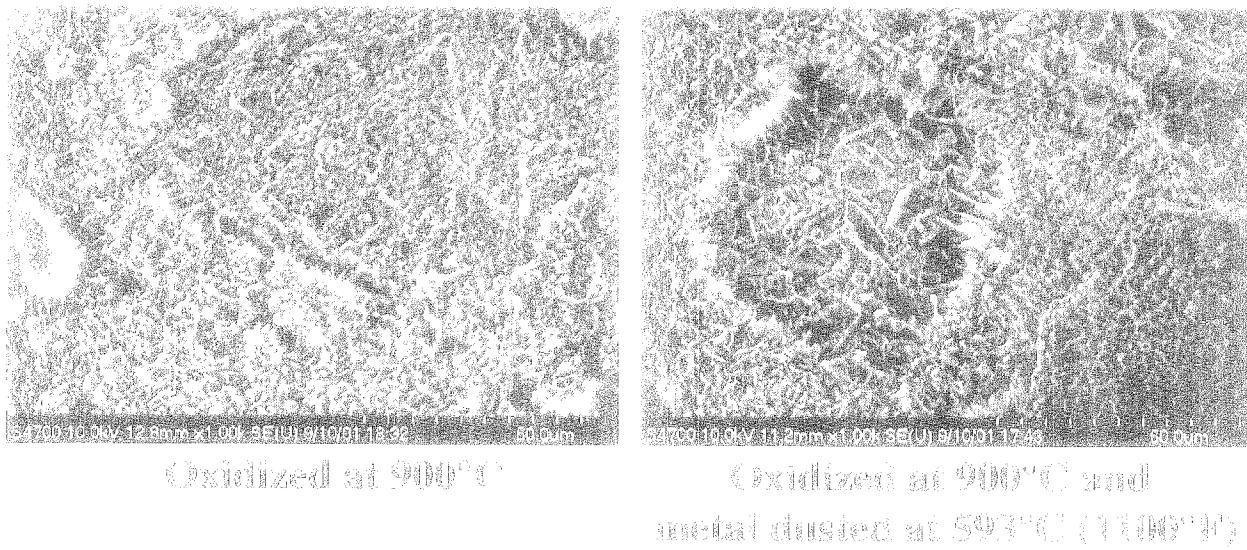


Fig. 60. SEM photomicrograph of surface of oxidized 122 steel after (left) oxidation at 800°C in air and (right) oxidation at 800°C followed by metal dusting exposure for 120 h at 800°C.

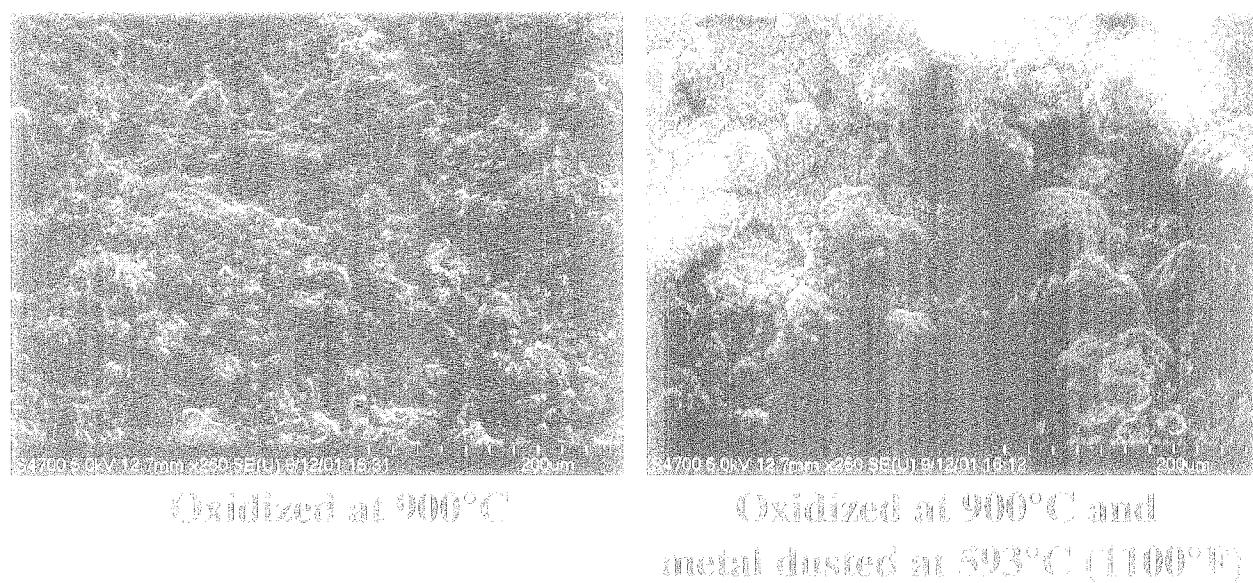


Fig. 6E. SEM photomicrograph of surface of atomized 321 stainless steel after (left) oxidation at 800°C in air and (right) oxidation at 900°C followed by metal dusting exposure for 142 h at 503°C.

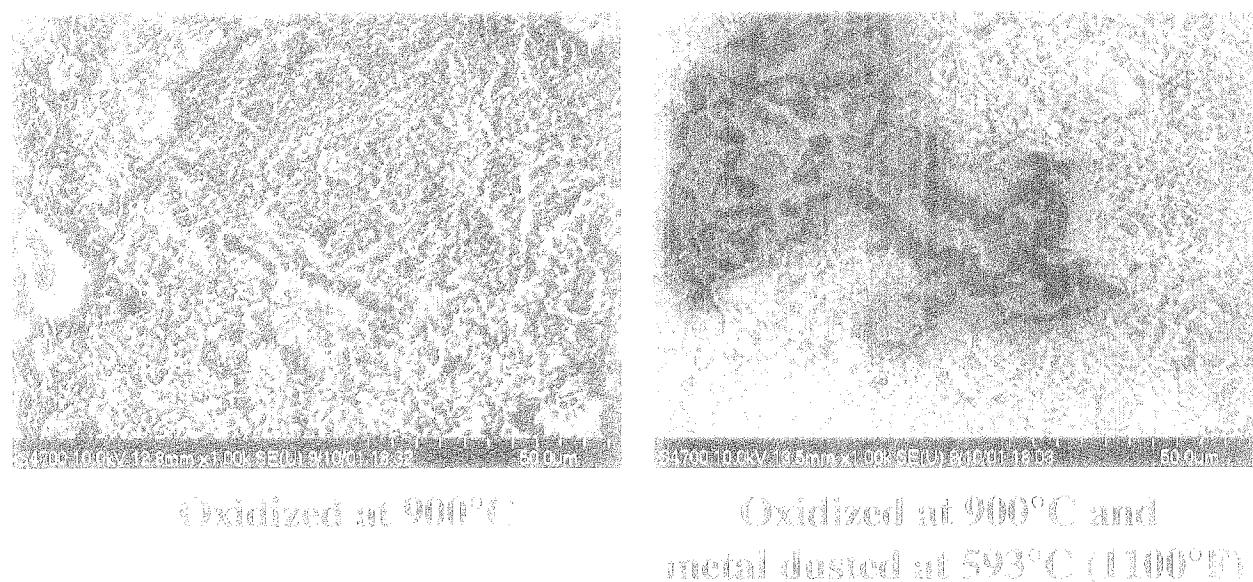


Fig. 6F. SEM photomicrograph of surface of atomized Alloy 800 after (left) oxidation at 800°C in air and (right) oxidation at 900°C followed by metal dusting exposure for 142 h at 503°C.

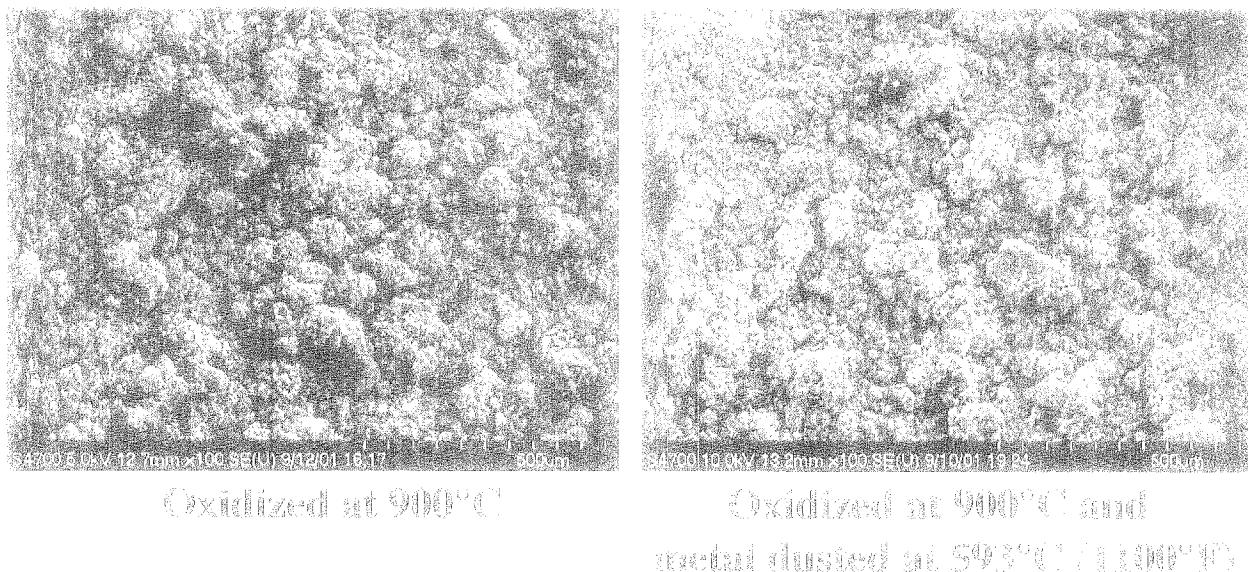


Fig. 62. SEM photomicrograph of surface of Chromellexed 102 steel after (left) oxidation at 900°C in air and (right) oxidation at 900°C followed by metal dusting exposure for 142 h at 593°C.

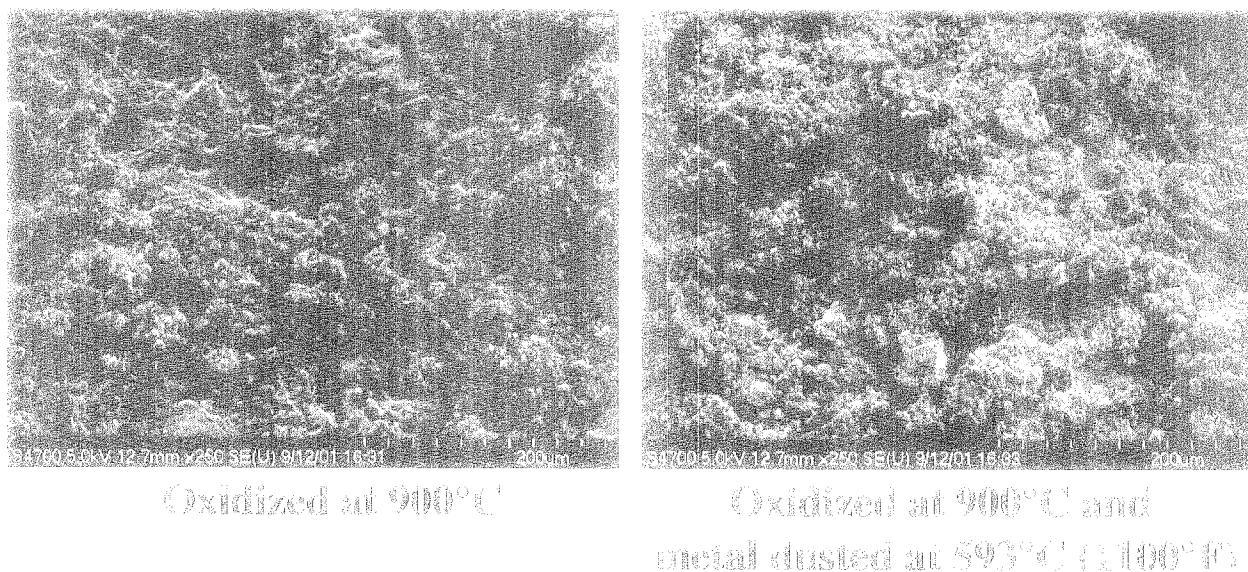


Fig. 63. SEM photomicrograph of surface of Chromellexed 321 stainless steel after (left) oxidation at 900°C in air and (right) oxidation at 900°C followed by metal dusting exposure for 142 h at 593°C.

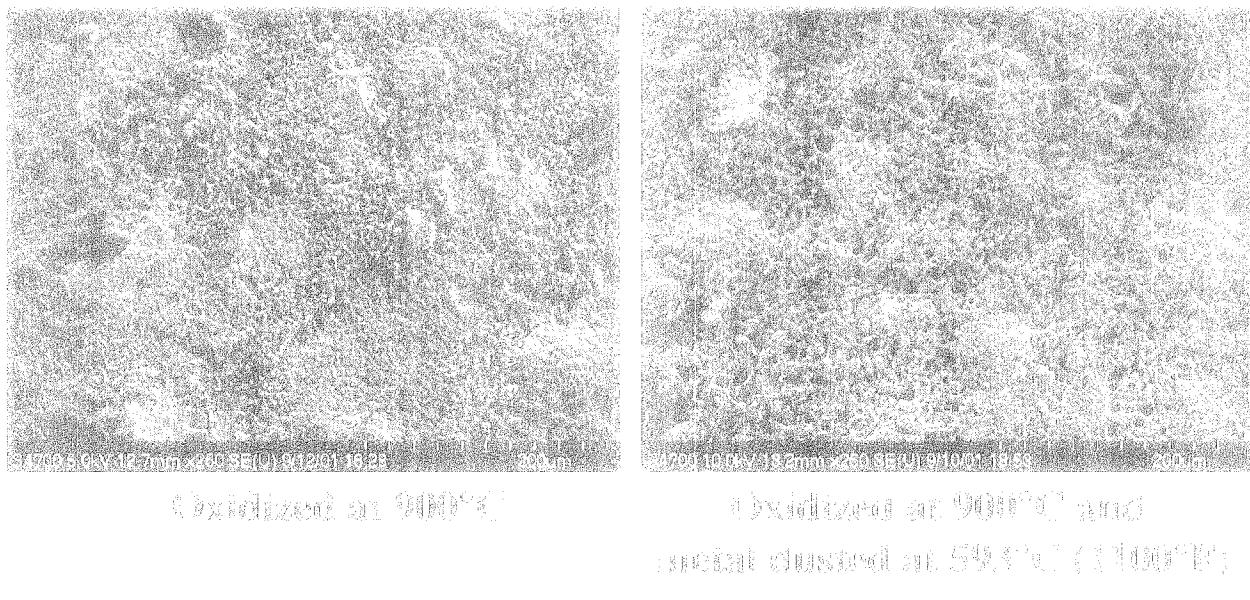


Fig. 56. SEM micrographs of surfaces of Chromium-Alloy 800 after heat treatment at 900°C for 100 h and (right) oxidation at 800°C for 100 h, followed by water quenching (left) or 800°C (right).

of metal clustering/degradation of the alloy. This is reinforced by the low availability of the catalytic surface for carbon-producing reactions to proceed. There may be a threshold in CO_2 for CVD carbon deposition. Metal clustering in the reformer environment is determined by a competition between the initial surface development and access of the virgin metal surface to the oxygen domain. The presence of an oxide scale may not prevent metal clustering and can delay its initiation, thereby slowing the overall attack.

The long duration of cladding (burning by H_2 on the alloy surface) on both Ti- and Ni-based alloys shows that defects in the oxide scales play a large role in initiation. Oxide scaling rate is mainly governed by the H_2O content in the environment to vary over. Numerous experiments have clearly indicated the effect of H_2O chemistry (in particular H_2O content) to the scaling, carbon deposition, and durability behavior. It is evident that the H_2O content in reformers is high enough to H_2O that a Cr-based alloy can develop a conformal scale (upon enough exposure of time) before carbon deposition.

Garnier modification: By preoxidation under various conditions and alternative materials are being examined at ASU, to alleviate the metal clustering problem. Oxide coatings have the advantage in that they can minimize carbon-producing reactions (by reducing the availability of catalytic surface) and can also act as a barrier to minimize carbon ingress and peeling of the substrate alloy. We have conducted *in situ* development of oxide scales, back diffusion of Al or Cr₃N₄, and chemical analysis to further

study. Preliminary tests showed virtually no carbon in pre-oxidized layers of Al-, Cr-, and Si-enriched layers that were subjected to metal dusting environments.

The effort at ANL will emphasize the competitive nature of oxidation and carbon deposition and will assess the options for mitigating metal dusting in waste-heat boilers and eventually eliminating the boilers from the reformer systems, especially for H₂ production.

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