#### Appendix 3A Summary Sheets for Phase III MCWM and DMC Testing

TEST/DESCRIPTION:				
Date	4/28/98	4/29/98	5/21/98	5/28/98
Filtering device	Fabric	Fabric	Ceramic	Ceramic
Coal seam	Hiawatha	Hiawatha	Hiawatha	Hiawatha
Cleaning tech.	Oil Agglomeration	Oil Agglomeration Oi	l Agglomeration	Oil Agglomeration
Natural gas support	31%	30%	30%	30%
WATER/STEAM SIDE				
Steam flow rate; lb/h	12,171	12,431	11,871	11,542
Water temperature into boiler; ° F	230	232	218	219
Drum pressure; psig	227	226	228	228
Calorimeter temperature; ° F	315	318	318	318
Steam temperature; ° F	393	397	397	397
Steam quality; %	99.9	100.1	100.1	100.1
Blowdown rate; lb/h	3,329	3,344	3,332	3,155
Air, Fuel, Flue Gas Side				
Total firing rate; MM Btu/h	15.6	15.8	15.0	14.9
Natural gas flow rate; lb/h; MM Btu/h	206; 4.8	194; 4.5	193; 4.	193; 4.5
CWSF flow rate; lb/h; MM Btu/h	1,478;10.5	1,560;10.5	1,322;10.5	1,289;10.5
Gas support (%)	30.8	28.8	30.1	30.2
Air temperature entering air heater; ° F	163	165	175	179
Air temperature leaving air heater; ° F	400	396	406	404
Air temperature into boiler; ° F	385	385	397	395
Furnace outlet temperature; ° F	596	591	594	596
Gas temperature leaving air heater; ° F	385	383	384	387
Bagfilter inlet temperature; ° F	389	385	381	386
Bagfilter outlet temperature; ° F	344	338	354	367
Ash content of fly ash;%	48.99	41.66	54.62	55.5
Combustion air flow; acfm	3,870	3,877	3,973	4,048
Boiler draft; in. W.C.	-0.06	-0.07	-0.06	-0.06
Boiler efficiency; %	76.71	76.74	79.57	79.39
Atomizing air pressure; psig	135	135	135	135
Atomizing air flow rate; lbs/h	756	657	756	720
A/F ratio; lb/lb	0.51	0.42	0.57	0.56
CWSF temperature; ° F	137	117	141	138
Natural gas temperature; ° F	90	90	90	90
Coal combustion efficiency; %	97.0	96.6	98.2	97.9
Overall combustion efficiency; %	97.3	97.0	98.4	98.2
EMISSIONS (Dry Basis)				
02; %	3.8	3.5	3.5	3.8
CO; ppm	15	44	N/A	N/A
CO2; %	13.0	12.8	14.0	13.9
SO2; ppm	496	610	N/A	N/A
NOx ppm	586	540	691	453
FUEL ANALYSIS DATA				
Solids Content; %	51.5%	50.3%	55.5%	57.0%

TEST/DESCRIPTION:				
Date	6/1/98	6/3/98	6/9/98	6/16/98
Filtering device	Fabric	Fabric	Fabric	Fabric
Coal seam	Hiawatha	Hiawatha	Taggart	Taggart
Cleaning tech.		Oil Agglomeration		
Natural gas support	30%	26%	30%	30%
WATER/STEAM SIDE				
Steam flow rate; lb/h	11,996	13,110	11,645	11,302
Water temperature into boiler; ° F	231	232	226	231
Drum pressure; psig	232	234	231	229
Calorimeter temperature; ° F	318	319	318	318
Steam temperature; ° F	397	398	397	397
Steam quality; %	100.1	100.1	100.1	100.1
Blowdown rate; lb/h	3,339	3,357	3,330	3,320
Air, Fuel, Flue Gas Side				
Total firing rate; MM Btu/h	14.8	14.6	14.7	14.8
Natural gas flow rate; lb/h; MM Btu/h	192; 4.5	168; 3.9	192; 4.5	194; 4.5
CWSF flow rate; lb/h; MM Btu/h	1,332; 10.5	1,428; 11.0	1,178; 10.5	1,152; 10.5
Gas support (%)	30.4	26.7	30.7	30.5
Air temperature entering air heater; ° F	173	158	171	177
Air temperature leaving air heater; ° F	413	410	415	415
Air temperature into boiler; ° F	389	386	391	391
Furnace outlet temperature; ° F	600	611	597	591
Gas temperature leaving air heater; ° F	377	379	370	360
Bagfilter inlet temperature; ° F	390	395	381	375
Bagfilter outlet temperature; ° F	363	371	354	345
Ash content of fly ash;%	61.16	58.20	37.61	24.02
Combustion air flow; acfm	4,259	4,438	3,732	3,835
Boiler draft; in. W.C.	-0.05	-0.04	-0.05	-0.05
Boiler efficiency; %	79.97	80.16	80.11	79.41
Atomizing air pressure; psig	135	135	135	80
Atomizing air flow rate; lbs/h	754	768	781	389
A/F ratio; lb/lb	0.57	0.54	0.66	0.34
CWSF temperature; ° F	141	147	141	155
Natural gas temperature; ° F	89	82	86	93
Coal combustion efficiency; %	98.7	98.4	97.7	95.1
Overall combustion efficiency; %	98.9	98.6	98.0	95.8
EMISSIONS (Dry Basis)				
02; %	3.7	3.2	3.7	3.4
CO; ppm	N/M	N/M	N/M	212.8
CO2; %	14.1	15.0	14.4	15.9
SO2; ppm	669	828	599	368
NOx ppm	242	224	188	488
FUEL ANALYSIS DATA				
Solids Content; %	55.5%	56.4%	59.5%	59.9%

TEST/DESCRIPTION:				
Date	6/19/00	6/22/00	C /24 /00	7 /21 /00
Filtering device	6/18/98	6/23/98	6/24/98	7/21/98
Coal seam	Fabric	Ceramic	Fabric	Fabric
Cleaning tech.	Taggart	Hiawatha	Hiawatha	Taggart
Natural gas support	23%	Oil Agglomeration		
Matural gas support	2370	30%	23%	30%
WATER/STEAM SIDE				
Steam flow rate; lb/h	11,143	11,476	9,446	10,073
Water temperature into boiler; ° F	231	231	231	229
Drum pressure; psig	230	230	229	231
Calorimeter temperature; ° F	318	318	316	318
Steam temperature; ° F	397	397	397	398
Steam quality; %	100.1	100.1	100.0	100.1
Blowdown rate; lb/h	3,322	3,327	3,320	3,332
Air, Fuel, Flue Gas Side				·
Total firing rate; MM Btu/h	15.0	14.7	140	145
Natural gas flow rate; lb/h; MM Btu/h	150; 3.5	195; 4.5	14.0 145; 3.5	14.5
CWSF flow rate; lb/h; MM Btu/h	1,272; 11.5	1,353; 10.5	1,428; 11.6	190; 4.5
Gas support (%)	23.4	30.6	25.0	1,200; 10.5 31.0
Air temperature entering air heater; ° F	179	180	184	186
Air temperature leaving air heater; ° F	424	423	402	
Air temperature into boiler; ° F	398			415
Furnace outlet temperature; ° F		399	379	391
	597	600	559	582
Gas temperature leaving air heater; ° F	372	378	359	370
Bagfilter inlet temperature; ° F	381	388	368	442
Bagfilter outlet temperature; ° F	353	366	344	347
Ash content of fly ash;%	29.00	52.27	48.30	20.84
Combustion air flow; acfm	3,774	3,859	3,806	3,657
Boiler draft; in. W.C.	-0.05	-0.05	-0.05	-0.05
Boiler efficiency; %	79.13	77.86	76.95	76.75
Atomizing air pressure; psig	135	135	135	135
Atomizing air flow rate; lbs/h A/F ratio; lb/lb	761	728	573	628
CWSF temperature; ° F	0.60	0.54	0.40	0.52
	156	140	147	130
Natural gas temperature; ° F	98	97	95	97
Coal combustion efficiency; %  Overall combustion efficiency; %	96.4 96.8	96.5	97.7	93.7
EMISSIONS (Dry Basis)	30.0	97.0	97.9	94.6
CINISSIONS (Dry Basis)				
02; %	3.8	3.6	4.7	4.2
CO; ppm	N/M	N/M	N/M	N/M
CO2; %	13.9	13.9	13.4	12.6
SO2; ppm	204	N/M	N/M	250
NOx ppm	584	610.2	525	227
FUEL ANALYSIS DATA				
Solids Content; %	60.3%	54.3%	56.0%	59.1%

TEST (DESCRIPTION					
TEST/DESCRIPTION: Date	9/11/00	0/12/00	0 (17 (00	0 /1 0 /0 0	0 (0 0 10 0
Filtering device	8/11/98 Fabric	8/12/98	8/17/98	8/19/98	8/26/98
Coal seam	Taggart	Fabric Taggart	Fabric Hiawatha	Fabric	Fabric
Cleaning tech.			Froth Floatation	Hiawatha	Middle Kittaning
Natural gas support	30%	30%	30%	27%	None 30%
	3070	3070	3070	2170	30%
WATER/STEAM SIDE					
Steam flow rate; lb/h	11,342	10,855	11,582	9,949	10,633
Water temperature into boiler; ° F	229	229	234	233	233
Drum pressure; psig	N/M	237	233	232	231
Calorimeter temperature; ° F	319	317	319	317	318
Steam temperature; ° F	398	398	398	397	397
Steam quality; %	N/M	100.0	100.1	100.0	100.1
Blowdown rate; lb/h	3,443	3,372	3,347	3,339	3,328
Air, Fuel, Flue Gas Side					
Total firing rate; MM Btu/h	15.1	14.9	15.3	14.6	15
Natural gas flow rate; lb/h; MM Btu/h	198; 4.6	192; 4.5	195; 4.5	174; 4.0	187; 4.5
CWSF flow rate; lb/h; MM Btu/h	1,210; 10.5	1,182; 10.5	1,392; 10.5	1,440; 11.0	1,176; 10.5
Gas support (%)	29.8	30.2	29.4	27.3	30.0
Air temperature entering air heater; ° F	186	184	180	177	182
Air temperature leaving air heater; ° F	421	412	419	410	419
Air temperature into boiler; ° F	398	387	396	386	396
Furnace outlet temperature; ° F	598	576	599	577	592
Gas temperature leaving air heater; ° F	373	365	379	365	379
Bagfilter inlet temperature; ° F	380	369	386	369	376
Bagfilter outlet temperature; ° F	366	343	364	348	
Ash content of fly ash;%	16.06	14.92	50.72	53.74	353 42.50
Combustion air flow; acfm	3,775	3,610	3,979	3,943	3,885
Boiler draft; in. W.C.	-0.05	-0.05	-0.05	-0.06	-0.05
Boiler efficiency; %	75.58	77.45	78.59	77.52	77.41
Atomizing air pressure; psig	80	135	135	135	135
Atomizing air flow rate; lbs/h	453	681	706	632	690
A/F ratio; lb/lb	0.38	0.58	0.51	0.44	0.59
CWSF temperature; ° F	158	152	141	110	152
Natural gas temperature; ° F	98	94	96	89	99
Coal combustion efficiency; %	90.9	92.5	97.5	97.4	93.6
Overall combustion efficiency; %	92.1	93.6	97.8	97.7	94.5
EMISSIONS (Dry Basis)					
O2; %	3.6	3.6	3.6	4.4	4.0
CO; ppm	N/M	N/M	N/M	N/M	N/M
CO2; %	14.1	14.2	13.9	12.6	13.2
SO2; ppm	437	417	211	442	290
NOx ppm	276	282	734	475	N/M
FUEL ANALYSIS DATA					
Solids Content; %	57.7%	59.3%	55.0%	54.5%	60.6%

TEST/DESCRIPTION: Date Filtering device Coal seam Cleaning tech. Natural gas support  WATER/STEAM SIDE	9/9/98 Fabric Taggart Oil Agglomeration 30%
WATER/STEAM SIDE	
Steam flow rate; lb/h Water temperature into boiler; ° F Drum pressure; psig Calorimeter temperature; ° F Steam temperature; ° F Steam quality; % Blowdown rate; lb/h	10,474 234 233 317 397 100.0 3,348
Air, Fuel, Flue Gas Side	
Total firing rate; MM Btu/h Natural gas flow rate; lb/h; MM Btu/h CWSF flow rate; lb/h; MM Btu/h Gas support (%) Air temperature entering air heater; °F Air temperature leaving air heater; °F Air temperature into boiler; °F Furnace outlet temperature; °F Gas temperature leaving air heater; °F Bagfilter inlet temperature; °F Bagfilter outlet temperature; °F Ash content of fly ash;% Combustion air flow; acfm Boiler draft; in. W.C. Boiler efficiency; % Atomizing air pressure; psig Atomizing air flow rate; lbs/h A/F ratio; lb/lb CWSF temperature; °F Natural gas temperature; °F Coal combustion efficiency; %	14.8 186; 4.5 1,170; 10.3 30.5 168 406 383 570 359 354 339 16.40 3,706 -0.05 77.99 80 370 0.32 158 86 93.0
Overall combustion efficiency; %	94.0
EMISSIONS (Dry Basis)	
O2; % CO; ppm CO2; % SO2; ppm NOx ppm	4.0 N/M N/M 150 490
FUEL ANALYSIS DATA	
Solids Content; %	59.9%

	TEST/DESCRIPTION:	20/2/3	7/8/0B		20/21/2	66/22/6	00/86/0						
Particle		06/0/0	06/0//		200		3/50/33	66/67/6	9/30/99	66/17/01	10/22/99	10/26/99	10/2//99
Thirty   T	Filtering Device:					Sleeve 0.5	Sleeve 3.5	Sleeve 3.5	Sleeve 4.5		Sleeve 3.5	Sleeve 3.5	Sleeve 3.5
	Burner Settings:	Prim 0	Prim 0	Prim 0	Prim 0	Center 1	Center 0	Center 0	Center 0		Center 2	Outer 7.5	Center 0
Part		Sec 100	Sec 100	Sec 100	Sec 100	Inner Max	Inner 6.5	Inner 6.5	Inner Max		Inner Max	Inner 6.5	Inner 6.5
The control of the		Tert 50	Tert 50	Tert 50	Tert 50	Outer Max	Outer	Outer 7.5	Outer Max		Outer Max	Outer 7.5	Outer 7.5
		Coal Gun +2	Coal Gun +2	Coal Gun +2	Coal Gun +2	Coal Gun -7	Coal Gun -7	Coal Gun -7	Coal Gun -7	Coal Gun	Coal Gun -6	Coal Gun -6	Coal Gun -6
Table State   1		Gas Gun +2	Gas Gun +2	Gas Gun +2	Gas Gun +2	Gas Gun -2	Gas Gun -2	Gas Gun -2	Gas Gun -2	Gas Gun	Gas Gun -2	Gas Gun -2	Gas Gun -2
Part	WATER/STEAM SIDE												
Particular in Delinic T	Steam flow rate; lb/h	11,700		11,066	11,360	10,867	10,492	11,107	10,496		10,875	10,714	10,067
Page	Water temperature into boiler; "F	233		230	230	236	236	236				236	236
Fig.	Drum pressure; psig	526		222	229	246	244	244				244	243
Part	Calorimeter temperature; °F	318		317	318	319	319	319				319	320
	Steam temperature; *F	397		398	398	402	402	402				402	401
Part	Steam quality; %	1.00.1				100.3	100.4					1	100.4
Full GAS SIDE   1,080   1,080   1,080   1,080   1,09	Blowdown rate; lb/h	3,332				3,439	3,425	3,423				3,429	3,415
1,000   1,00	AD CLIC CAC CIDE												
Table Burn 1, 1489 1, 1589 1,	ANN, FUEL, FLUE GAS SIDE												
Fig. 18.2   15.5   15.4   15.5   15.4   15.5   15.4   15.5   15.5   15.4   15.5   15	Coal Flow rate; lb/h	1,080		080,1	1,080	1,050	1,050	1,044				1,050	1,050
Tature elementary F	Coal flow rate; MMBtu/h	14.9		15.4	15.5	15.0	15.0	14.9				15.3	14.9
Tature leaving air heater F	Boiler outlet temperature; "F	614		604	612	612	287	602				603	604
State   Stat	Gas temperature leaving air heater; "F	384		380	386	369	363	367				366	358
Activative incoming in heaters*   Activative incoming   Activati	Air temperature entering air heater; 'F	173		179	186	166	183	178				174	137
Particulate National Particu	Air temperature leaving air heater; "F	417		411	421	421	428	427				430	416
Mustors         Feature (search)         44.70         38.94         45.16         94.1         47.36         47.66         58.53         47.84         48.47         96.7 <t< td=""><td>Air temperature into boiler; "F</td><td>403</td><td></td><td>397</td><td>409</td><td>400</td><td>299</td><td>545</td><td></td><td></td><td></td><td>409</td><td>395</td></t<>	Air temperature into boiler; "F	403		397	409	400	299	545				409	395
Autories Control filtements (Figure No. 1)         4,6         92,4         95,6         94,1         95,2         94,6         96,6         96,7         95,7           Dustron efficiency, Me actinal control filting and proper prope	Ash content of particulate; %	44.70		45.16		47.36	47.66	58.53		7		45.23	54.48
NECOL         12.06         3.226         3.234         3.120         3.082         2.887         3.126         2.956         3.029         2.956           cency, №         8.36         6.06         6.06         6.07         -0.07         -0.07         -0.06         -0.09         -0.09         -0.07         -0.07         -0.06         -0.06         -0.09         -0.09         -0.07         -0.07         -0.06         -0.09         -0.09         -0.07         -0.07         -0.06         -0.06         -0.09         -0.09         -0.07         -0.07         -0.06         -0.06         -0.09         -0.09         -0.07         -0.07         -0.06         -0.06         -0.09         -0.09         -0.07         -0.06         -0.06         -0.06         -0.06         -0.09         -0.07         -0.07         -0.06         -0.06         -0.06         -0.07         -0.07         -0.07         -0.07         -0.06         -0.09         -0.09         -0.07         -0.07         -0.06         -0.09         -0.09         -0.07         -0.07         -0.07         -0.07         -0.06         -0.09         -0.09         -0.09         -0.07         -0.07         -0.07         -0.07         -0.07         -0.07         -0.	Coal combustion efficiency; %	94.6		92.6		95.2	94.6	9.96				92.6	95.5
Lit, Inches W.C.         -0.06         -0.07	Combustion air flow; acfm	3,208			3,120	3,082	2,887	3,126				2,901	3,022
Participate	Boiler draft; inches W.C.	-0.06			-0.09	-0.08	-0.07	-0.07				90.0-	90.0-
Metols         ATA         ASS         ASS<	Boiler efficiency; %	83.4		83.8	83.0	84.9	85.0	86.6				84.9	84.4
temperature, F	Mill air flow rate; acfm	401		396	400	397	409	403			403	408	382
Paper   Pape	Mill outlet temperature; "F	243		322	239	257	239	235			235	235	216
Match   Matc	Filter type	Fabric	Fa	Ceramic	Ceramic	Fabric	Fabric	Fabric	Fabric	Cera		Ceramic	Ceramic
F   Reti-order         388         389         384         373         386         387         384         378         389         389         381	Pressure drop; in W.C.	4.2		13.1	14.0	1.8	1.5	1.7	1.6			2.1	2.1
SC         336         336         456         456         460         360         355           SC         40         79         40         3.4         40         3.4         40         3.4         40         3.4         40         3.4         40         3.4         40         3.4         40         3.4         40         3.4         40         3.4         40         3.4         40         3.4         3.0         3.2         3.2         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.2         3.2         3.3         3.2<	Filter inlet; ° F	381		380	387	384	377	385	384	383		389	374
SS         3.4         3.9         4.0         3.4         4.0         3.4         3.9         3.9         3.9         3.2         3.3         3.3         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2         3.3         3.2	Filter outlet; ° F	330		354	384	455	461	438	460	360		387	345
NEDIC   Parameter   Paramete	EMISSIONS												
No.   14.5   15.7   14.9   16.9   16.9   16.3   12.8   13.7   13.4   13.8   13.5   13.4   13.8   13.5   13.4   13.5   13.5   13.4   13.5   13.5   13.4   13.5   13.5   13.4   13.5   1	02 %	3.4		4.0	3.4	4.0	3.4	3.9				3.7	4.5
No.	со ррт	40		56	69	169	163	228		214		265	384
NVA   SO4   494   SO6   440   362   455   357   469   456	CO2 %	14.5		14.9	15.6	14.5	15.0	15.1	14.3			15.3	14.0
VNEOUS DATA         A13         355         375         397         192         402         411         351         399         336           ONE OUR DATA         NEOUS DATA <th< td=""><td>SO2 ppm</td><td>N/A</td><td></td><td>494</td><td>909</td><td>440</td><td>362</td><td>455</td><td></td><td>469</td><td>456</td><td>475</td><td>427</td></th<>	SO2 ppm	N/A		494	909	440	362	455		469	456	475	427
73.9 71.4 75.6 71.4 73.5 74.0	NOx ppm	413		375	397	192	402	411	351	399	336	236	306
73.9 71.4 75.6 71.4 73.5 74.0													
73.9 71.4 75.6 71.4 73.5 74.0	MISCELL ANEONS DATA												
73.9 71.4 75.6 71.4 73.5 74.0	Maximum foad												
	(based on 14,700 lb steam/h); %	79.6		75.3	77.3	73.9	71.4	75.6				72.9	68.5
NOTES File gas temperature leaving air heater and boller efficiencies from 9/27/99 through 4/26/00 are incorrect. The stransion principle to the property of the principle developed a leak and ambient air was drawn into the systems of starting and principle are efficiency and principle principle leak was observed starting 1937/99, second and more serious leak was observed starting.													
Flue gas temperature leaving air heater and boiler efficiencies from 9/27/99 through 4/26/00 are incorrect. The sexpansion the air heater and outlet ducting developed a leak and ambient air was drawn into the sexpansion and artist and outlet are are outlet and outlet are are outlet and artist and are serious lask was observed starting 4/27/99, second and more serious lask was observed starting.	NOTES												
expansion joint between the air heater and outlet ducting developed a leak and ambient air was drawn into the system. First noticeable leak was observed starting 9/27/99, second and more serious leak was observed starting	Flue gas temperature leaving air heater a	and boiler efficiencies	from 9/27/99 thi	rough 4/26/00 a	are incorrect. The								
System. First noticeable leak was observed starting 9/2//99, second and more serious leak was observed starting	expansion joint between the air heater a	nd outlet ducting deve	eloped a leak and	ambient air was (	drawn into the								
	system. First noticeable leak was obsern	ved starting 9/27/99,	second and more	serious leak was	observed starting	0				_			

Sleeve 3.5	Sleeve 3.5											
	eve 3.5	-								1		
		Sleeve 3.5	Sleeve 5.5	Sleeve 3.5	Sleeve 3.5							
	Center 0	Center 1	Center 1	Center 1	Center 0	Center 1	Center 1					
	Inner 6.5	Inner 6.5	Inner Max	Inner Max	Inner Max	Inner Max	Inner 6.5	Inner 6.5	Inner 6.5	Inner Max	Inner 6.5	Inner 6.5
	Outer 7.5	Outer 7.5	Outer Max	Outer Max	Outer Max	Outer Max	Outer 7.5	Outer 7.5	Outer 7.5	Outer Max	Outer 7.5	Outer 7.5
	Coal Gun -6											
WATENSTEAM SIDE  Steam flow rate; lb/h Water temperature into boiler, "F Drum pressure; psig Calorineter temperature; "F Steam quality; % Blowdown rate; lb/h ARFUEL, FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h Coal Flow rate; lb/h Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h ARFUEL Rate; lb/h ARFUEL Rate Rate; lb/h ARFUEL Rate Rate Rate Rate Rate Rate Rate Rate	7- unn -	2- uno seo	2- uno seo	nas enu -c	2- una sea	cas cun -z	cas can -c	oas onn -c	nas cun -o	2- uno seo	2- uno seo	cas cun -2
Steam flow rate; lb/h Water temperature into boiler; 'F Drum pressure; psig Calorimeter temperature; 'F Steam quality; '8  Blowdown rate; lb/h ARFUEL, FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h Coal Flow rate; lb/h Goal flow rate; lb/h ARFUEL, FLUE GAS SIDE Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h ARFUEL FLUE GAS SIDE Coal Flow rate; lb/h Coal Flow r												
Water temperature into boiler, "F  Drum pressure; psig  Stadorimeter temperature; "F  Steam quality; "B  Blowdown rate; lb/h  ARFUEL, FLUE GAS SIDE  Coal Flow rate; lb/h  Coal flow rate; MMBtu/h  Boiler outlet temperature; "F  Gas temperature leaving air heater; "F  Air temperature leaving air heater; "F	10,630	10,766	10,879	10,688	10,833	10,739	10,203	10,572	10,400	10,417	10,484	10,922
Calorimeter temperature; 'F Steam temperature; 'F Steam quality; '8  Blowdown rate; lb/h AIR,FUEL, FLUE GAS SIDE Coal Flow rate; lb/h Coal flow rate; lb/h Coal flow rate; lb/h AIR,FUEL, FLUE GAS SIDE AIR,FUEL, FLUE GAS SIDE AIR,FUEL, FLUE GAS SIDE Coal flow rate; lb/h AIR,FUEL, FLUE GAS SIDE AIR, FUEL, FLUE GAS SIDE AIR, TEMPERATURE entering air heater; 'F Air temperature entering air heater; 'F Air temperature leaving air heater; 'F Air temperature leaving air heater; 'F Air temperature leaving air heater; 'F Air temperature into boiler; 'F	236	235	235	235	235	236	236	235	236	235	236	234
Calorimeter temperature; 'F Steam temperature; 'F Steam quality; 'M Blowdown rate; lb/h ARFUEL, FLUE GAS SIDE Coal Flow rate; lb/h Coal flow rate; lb/h Boiler outlet temperature; 'F Gas temperature leaving air heater; 'F Air temperature entering air heater; 'F Air temperature leaving air heater; 'F	241	242	242	241	238	240	253	251	250	249	248	231
Steam temperature; 'F  Steam quality; %  Blowdown rate; lb/h  ARFUEL, FLUE GAS SIDE  Coal Flow rate; lb/h  Air temperature leaving air heater; 'F  Air temperature into boiler; 'F	319	319.	320	319	320	319	320	320	318	319	319	318
Blowdown rate; lb/h  ARFUEL, FLUE GAS SIDE  Coal Flow rate; lb/h  Coal flow rate; lb/h  Coal flow rate; MMBtu/h  Boiler outlet temperature; F  Gas temperature leaving air heater; F  Air temperature leaving air heater; F	401	401	401	401	400	401	404	404	403	403	405	398
Blowdown rate; Ib/h  ARFUEL, FLUE GAS SIDE  Coal Flow rate; Ib/h Coal flow rate; MMBtu/h Boiler outlet temperature; *F Gas temperature leaving air heater; *F Air temperature leaving air heater; *F	100.3	100.3	100.4	100.3	100.4	100.3	100.4	100.4	100.3	100.3	100.3	100.3
ARFUEL, FLUE GAS SIDE  Coal Flow rate; lb/h Coal flow rate; MMBtu/h Boiler outlet temperature; "F Gas temperature entering air heater; "F Air temperature leaving air heater; "F	3,402	3,409	3,411	3,407	3,382	3,397	3,491	3,477	3,465	3,459	3,453	3,330
Any Coal Flow and Subsequent Coal Flow rate; Ib/h Coal flow rate; Ib/h Boiler outlet temperature; "F Gas temperature leaving air heater; "F Air temperature into boiler; "F												
Coal flow rate, MBtu/h Coal flow rate, MBtu/h Boiler outlet temperature, 'F Gas temperature leaving air heater, 'F Air temperature entering air heater, 'F Air temperature leaving air heater, 'F Air temperature leaving air heater, 'F Air temperature into boiler; 'F	1 050	1 050	1 050	0001	000	0101	1 055	1 000	1 050	1 055	1 050	1 000
Boiler outlet temperature; *F Gas temperature leaving air heater; *F Air temperature entering air heater; *F Air temperature leaving air heater; *F Air temperature leaving air heater; *F Air temperature leaving air heater; *F	000,	000,1	050,1	1,030	14.7	14.0	14.0	14.0	1,035	1,033	14.7	19 5
Jones outce temperature, 1 Gas temperature leaving air heater, 1º Air temperature entering air heater, 1º Air temperature leaving air heater, 1º Air temperature into boiler; 1º	2.0	14.3	13.0	213	4.7	009	0.4.0	14.0	1.0	13.1	7.4	13.3
Air temperature entering air heater, 'F Air temperature leaving air heater, 'F Air temperature into boiler; 'F	367	369	367	357	359	361	340	344	337	347	316	313
Air temperature leaving air heater, "F Air temperature into boiler; "F	160	171	176	731	147	021	170	175	150	157	152	771
Air temperature into boiler, "F	421	431	430	429	424	420	415	439	443	452	407	420
Call Compensation College, 1	308	400	408	408	404	308	390	414	417	424	381	308
Ash content of particulate: %	48.78	53 17	91.12	47.48	26.75	64 42	39.95	37.08	31 61	31 52	42.48	11 44
Coal combustion efficiency: %	95.3	95.7	95.8	979	8 96	97.6	93.0	919		91.12	93.2	85.6
Compustion air flow: acfm	3.163	2,679	3.133	3.012	2.987	3.125	3.011	3.047		2.946	3.056	3.132
Boiler draft; inches W.C.	90.0-	-0.04	-0.04	-0.11	-0.05	-0.08	-0.07	-0.07	-0.06	-0.08	-0.07	-0.06
Boiler efficiency; %	84.3	84.6	84.4	84.7	85.4	82.8	83.4	82.8	82.0	81.5	83.4	79.2
Mill air flow rate; acfm	406	404	404	412	407	406	403	403	392	407	324	405
Mill outlet temperature; "F	218	230	238	223	221	500	220	238	220	230	170	223
	Ceramic											
Pressure drop; in W.C.	4.6	4.6	4.8	2.0	5.0	5.5	4.7	5.4	9.6	5.9	5.6	5.9
Filter inlet; ° F	377	386	388	378	372	375	358	374	356	389	346	342
Filter outlet; °F	343	375	374	362	385	351	419	396	369	378	315	360
EMISSIONS												
02 %	3.3	3.4	3.3	3.8	3.7	3.2	3.5	3.5	4.0	3.2	3.9	3.9
CO ppm	268	305	291	432	225	152	319	511	1,068	1,045	367	515
CO2 %	14.9	15.2	15.1	15.1	15.4	15.0	15.1	15.7	15.4	15.8	13.6	15.4
S02 ppm	469	478	461	465	470	462	463	471	445	488	312	88
NOx ppm	342	325	353	200	338	371	367	355	342	373	317	343
ATTOCITY ANTOCINA										†		
MiscellaneOUS DATA												
(based on 14.700 lb steam/h): %	72.3	73.2	74.0	72.7	73.7	73.1	69.4	21.9	707	20.9	713	74.3
NOTES												
Flue gas temperature leaving air heater and b												
expansion joint between the air heater and on												
system. First noticeable leak was observed st												
3/15/00, and expansion joint was replaced be												

Seeve 3.5   Sleeve 3.5   Slee	TEST/DESCRIPTION:	4/6/00	4/7/00	4/11/00	4/12/00	4/18/00	4/19/00	4/20/00	4/21/00	4/24/00	4/25/00	4/26/00	7/5/00
Control   Cont													
Control   Cont	Filtering Device:	Sleeve 3.5	Sleeve 3.5	Sleeve 3.5	Sleeve 3.5	Sleeve 3.5	Sleeve 3.5	Sleeve 3.5	Sleeve 3.5				
Particular   Par	Burner Settings:	Center 1	Center 1	Center 1	Center 2	Center 2	Center 2	Center 2	Center 2	Center 2	Center 2	Center 2	Center 2
Control   Cont		Inner Max	Inner Max	Inner 6.5	Inner 6.5	Inner 6.5	Inner 6.5	Inner 6.5	Inner 6.5	Inner Max	Inner 6.5	Inner 6.5	Inner 6.5
March   Marc		Outer Max	Outer Max	Outer 7.5	Outer 7.5	Outer 7.5	Outer 7.5	Outer 7.5	Outer 7.5	Outer Max	Outer 7.5	Outer 7.5	Outer 7.5
County   C		Coal Gun -6	Coal Gun -6	Coal Gun -6	Coal Gun -6	Coal Gun -6	Coal Gun -6	Coal Gun -6	Coal Gun -6				
VATION SIET         Common Signation Siet         Signation Signature Signation Signation Signature Signatu		Gas Gun -2	Gas Gun -2		Gas Gun -6	Gas Gun -2	Gas Gun -6	Gas Gun -6	Gas Gun -6	Gas Gun -2	Gerning	Corning	Corning
						Corning	Corning	Clinetroom	Clinetream	Clinetream	Slinstream	Slinstream	Slinstream
Comparison   Com	WATER/STEAM SIDE	107	70611	11 469	11 540	Jupstream 11 ACE	311pstream	11 709	11 698	11 387	11.383		10,477
Control Cont	Steam flow rate; Ib/n	11,137			0.50	234	233	233	733				231
Participation   Participatio	Water temperature into boiler; 'F	233			200	222	221	219					226
	Drum pressure; psig	231			317	317	318	319					318
	Calorimeter temperature; T	308			396	395	394	394					
### 1975   1975	Steam temperature; r	1003			1002	100.2	100.3	100.3		-		-	100.3
	Steam quairty; 76	3 3 2 9			3 296	3 264	3.255	3.241					3,293
the coverage of the coverage	BIOWGOWN FALE; ID/TI	636,6			2021								
Own Rate, Burnham         1 0553	AIR, FUEL, FLUE GAS SIDE												
March   Marc	Coal Flow rate; lb/h	1,055			1,055	1,055	1,055	1,055					080,1
March   Marc	Coal flow rate; MMBtu/h	14.3			14.4	14.5	14.5		14.5				14.5
Propertive fearing air heaters**	Boiler outlet temperature; °F	613			625	209	618		635				905
Part	Gas temperature leaving air heater; "F	320			257	263	272	274				287	396
Page page page page page page page page p	Air temperature entering air heater; °F	178			157	191	167	168					191
Apperature Into boling: T	Air temperature leaving air heater; °F	431			429	404	415	421	423				424
Number of particulates, by a bill of the particulates a bill of the particula	Air temperature into boiler; °F	409			407	383	395						404
Particle	Ash content of particulate; %	49.63			06.89	50.10	61.02						61.89
State   Stat	Coal combustion efficiency; %	84.8			9.76	94.7	9.96						96.5
Control of the con	Combustion air flow; acfm	3,051			2,868	3,147	3,172						2,111
Filterency, %   Filterency,	Boiler draft; inches W.C.	-0.07			90.0-	-0.07	-0.06						-0.07
LAMEOUS DATA   LAME	Boiler efficiency; %	78.5			90.1	87.1	88.3	90.0					83.7
let temperature; F	Mill air flow rate; acfm	403			401	401	401	408					317
Ype         Ceramic         Table;         Table; </td <td>Mill outlet temperature; "F</td> <td>222</td> <td></td> <td></td> <td>221</td> <td>222</td> <td>228</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>677</td>	Mill outlet temperature; "F	222			221	222	228						677
re drop; in W.C.	Filter type	Ceramic	Cera	Cera	Ceramic	Fabric	Fabric					a.	Ceraniic
March   Marc	Pressure drop; in W.C.	6.2			7.3	2.8	1.4						4.3
Numberty of promotes as a semperature leaving air heatest and burnet severe the air heatest and burnet severe the air heatest and burnet cape leav was replaced by a control and are are a control and are are and burnet and burnet and burnet are	Filter inlet; ° F	352			335	323	328						967
No.	Filter outlet; °F	354			323	287	295	308					270
m         3.7         3.6         3.8         4.0         3.6         3.8         4.0         3.6         3.9           m         228         228         236         179         179         116         252         3.9           pm         90         88         88         88         88         253         341         426         472         526         412         442           pm         90         88         88         88         84         425         469         362         436           pm         312         325         339         397         419         368         469         469         392         436           pm         325         339         397         419         368         469         469         392         436           LANEOUS DATA         358         77.5         77.9         80.7         79.6         77.5         77.4           LAMEOUS becament the air heater and b.         358         77.9         80.7         79.6         77.5         77.4           Solido joint between the air heater and b.         358         77.5         77.9         80.7         79.7         77.5         77.4<	EMISSIONS											1	
15.0   15.8   15.9   10.0   15.6   17.9   13.3   11.6   25.2   30.6   13.3   15.1   15.2   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3	02 %	3.7			3.8	4.0	3.6						4.7
15.3   15.4   15.2   15.1   15.6   15.5   15.3   15.1   15.2   15.2   15.3   15.1   15.2   15.2   15.3   15.1   15.2   15.2   15.3   15.1   15.2   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.3   15.1   15.2   15.2   15.3   15.3   15.3   15.3   15.3   15.3   15.3   15.3   15.3   15.3   15.2   15.3	CO ppm	228			100	156	179						848
NEOUS DATA   90	CO2 %	15.3			15.3	15.1	15.6						12.4
NEGUS DATA   19   36   425   469   469   392   436   446   486	S02 ppm	06			253	341	426						30
NeDus DATA   14,700 lb steam/h); %   75.8   77.5   78.0   78.5   77.9   80.7   79.7   79.6   77.5   77.4   79.6   79.6   77.5   77.4   79.6	NOx ppm	325			419	368	425						374
AMEOUS DATA In load Itemperature leaving air heater and b. In soint between the air heater and out Instruction load was observed by In load expansion lont was replaced by													
AMEQUS DATA         ANEQUS DATA         ANEQUS DATA         ANEQUS DATA         ANEQUE DATA													
In load  In	MISCELLANEOUS DATA												
temperature leaving air heater and b.  First noticeable leak was observed st D, and expansion loint was replaced be	Maximum load	-			70 5	9 2 2	80.7					62	71.3
NOTES Flue gas temperature leaving air heater and b expansion joint between the air heater and ou system. First noticeable leak was observed st 3/15/00, and expansion ioint was replaced be	(based on 14,700 lb steam/n); %	(3.0			007	2							
Flue gas temperature leaving air heater and b.  expansion joint between the air heater and ou system. First noticeable leak was observed st 3/15/00, and expansion joint was replaced be	NOTES												
expansion joint between the air heater and ou system. First noticeable leak was observed st 3/15/00, and expansion joint was replaced be	Flue gas temperature leaving air heater and	٥											
system. First noticeable leak was observed st 3/15/00, and expansion loint was replaced be	expansion joint between the air heater and	no											
3/15/00, and expansion joint was replaced be	system. First noticeable leak was observed	st											
	3/15/00, and expansion joint was replaced be	þć											

TEST/DESCRIPTION:	1,00	2/2/00	2/10/00	7/11/00	2/13/00	7/14/00	2/17/00	2/18/00	2/19/00	2/20/00	2/21/00	1/24/00
	1/6/00	22/1//	00/01//	3								
Eiltering Device	Sleeve 3.5											
Rumar Sattings	Center 2											
	Inner 6.5	Inner Max										
	Outer 7.5	Outer Max										
	Coal Gun -6											
	Gas Gun -6	Gas Gun -2	Gas Gun -6	Gas Gun -2	Gas Gun -2	Gas Gun -6	Gas Gun -2	Gas Gun -2	Gas Gun -6	Gas Gun -2	Gas Gun -2	Gas Gun -6
	Corning											
WATER/STEAM SIDE	Slipstream											
Steam flow rate; lb/h	11,278		11,360	11,255	7,849	11,303	11,613	11,448	11,179	11,955	11,605	11,616
Water temperature into boiler; "F	231	231	231	231	222	231	231	231		231	231	232
Drum pressure; psig	226	225	228	225	216	218	217	212		214	213	214
Calorimeter temperature; °F	306	318	317	318	317	317	317	317		318	317	317
Steam temperature; °F	396		397	396	393	394	394			393	393	392
Steam quality; %	9.66	100.3	100.3	100.3	100.2	100.2	100.2	100.2		100.3	100.2	100.2
Blowdown rate; lb/h	3,295	3,285	3,309	3,289	3,222	3,235	3,230	3,228	3,228	3,205	3,197	3,202
AR FIFE FLUE GAS SIDE												
Coal Flow rate: lh/h	1.080	1,080	1,080	1,110	1,110	1,110	1,110	1,080	1,101	1,101	1,101	1,091
Coal flow rate: MMBtu/h	14.7		14.5	15.0	15.1	15.0	15.1	14.6	14.9	15.1	12.1	14.4
Boiler outlet temperature: °F	617		625	009	548	603	614	585		209	613	909
Gas temperature leaving air heater: °F	404		413	396	360	392	398	383		391	397	392
Air temperature entering air heater: °F	186		188	190	202	191	191	187	182	188	188	189
Air temperature leaving air heater; "F	429	427	432	423	412	431	438			433	438	437
Air temperature into boiler: "F	407		411	403	388	408	414	394	396	411	416	413
Ash content of particulate; %	62.03	59.45	52.39	47.33	39.28	42.69	42.52	7		36.00	38.98	58.77
Coal combustion efficiency; %	9.96	96.2	94.6	94.2	91.7	92.7	92.2	92.8			92.0	94.7
Combustion air flow; acfm	3,241		3,329	3,186	2,515	3,060	3,114	3,133			3,136	2,983
Boiler draft; inches W.C.	-0.06		-0.07	-0.02	-0.08	-0.07	-0.07				-0.07	-0.05
Boiler efficiency; %	85.1		80.2	83.3	79.4	81.8	81.6		79.7	80.3	81.4	83.8
Mill air flow rate; acfm	400		405	405	294	416	418		414	425	477	410
Mill outlet temperature; °F	242	243	257	191	125	137	140			144	. 43	147
Filter type	Ceramic	Cera	Cera	Ceramic	Ceramic	Ceramic						
Pressure drop; in W.C.	6.5	6.7	9.9	5.9	3.9	5.3	5.4			5.7	6.3	5.8
Filter inlet; °F	383	386	395	377	340	372	378			375	377	372
Filter outlet; ° F	353	357	363	347	321	340	345	331	329	345	347	342
EMISSIONS											-	
02 %	3.9		8.5	4.5	8.9	5.2	4.2			4.1		5.3
CO ppm	412		345	275	424	424	405			98/		463
CO2 %	15.5	-	10.0	14.8	10.1	14.1	15.0				14.6	15.7
SO2 ppm	20		29	105	71	98	88				16.	76
NOx ppm	578	330	210	417	288	409	435	4 8	21/	499	anc.	070
MISCELL ANEOUS DATA												
Maximum load												
(based on 14,700 lb steam/h); %	7.97	75.3	77.3	76.6	53,4	6.92	79.0	6.77	76.0	81.3	78.9	79.0
NOTES												
Flue gas temperature leaving air heater and b	nd br											
expansion joint between the air heater and ou	no po											
system. First noticeable leak was observed st	ed st											
3/15/00, and expansion joint was replace	ad be											

											30,00	20,110
TEST/DESCRIPTION:	8/21/00	8/22/00	8/23/00	8/24/00	8/25/00	8/29/00	8/30/00	8/31/00	9/1/00	9/2/6	9/6/00	9/1/6
Filtering Device:	Sleeve 3.5											
Burner Settings:	Center 2											
	Inner Max	Inner Max	Inner 6.5	Inner Max	Inner Max	Inner 6.5						
	Outer Max	Outer Max	Outer 7.5	Outer Max	Outer MaX	Outer 7.5						
	Coal Gun -6											
	Gas Gun -2	Gas Gun -2	Gas Gun -6	Gas Gun -2	Gas Gun -2	Gas Gun -6						
	Corning	Clintroom	Clinetroam	Clinetream	Slinstream	Slinetream						
WATER/STEAM SIDE	Slipstream	Sipstream	Silpsi	12 271	12 470	12 370	12 463	12 606	12 189	11.448	11.912	11.747
Steam flow rate; ID/n	11,940	71		12,31	220	230	230	230	231	231	231	731
Water temperature into boiler; 'F	787			212	211	211	212	211	211	211	213	213
Drum pressure; psig	213			217	213	310	212		318	317	317	318
Calorimeter temperature; °F	318			317	313	302	302		392	391	392	392
Steam temperature; *F	393	100.2	1003	100.2	1000	1003	1003		-	100.2	100.3	100.3
Steam quality; %	1.244			3,190	3,182	3,186	1,245		1,243	3,182	3,198	1,247
Diomonti Tacci, Ibi i												
AIR, FUEL, FLUE GAS SIDE											.00	
Coal Flow rate; Ib/h	1,091	1,091	1,091	1,091	1,091	1,091	1,091	_	1,091	160,1	160'1	160,1
Coal flow rate; MMBtu/h	14.4			14.5	14.7	15.1	15.0		14.1	14.2	14.1	14.1
Boiler outlet temperature; °F	613		288	611	009	298	609		609	297	019	8 9
Gas temperature leaving air heater; "F	404			407	399	405	408		405	392	406	411
Air temperature entering air heater; "F	187		185	184	184	183	182		183	183	)) l	1/8
Air temperature leaving air heater; "F	450	447	432	443	432	435	438		436	432	436	441
Air temperature into boiler; "F	410				394	397	401			393	397	403
Ash content of particulate; %	70.27	79.94		7	75.00	71.79	81.36			86.69	90.61	92.73
Coal combustion efficiency; %	96.4			98.1	98.0	98.5				95.7		99.3
Combustion air flow; acfm	3,102			3,215	3,228	3,260				3,106	3,213	3,185
Boiler draft; inches W.C.	60.0-			-0.09	-0.10	-0.07	-0.08			9.10	50.0	-0.00
Boiler efficiency; %	85.1			90.9	86.3	86.8	86.9			201	90.0	2.10
Mill air flow rate; acfm	405			411	402	405	410			391	404	408
Mill outlet temperature; °F	217			212	202	214	214			208	617	212
Filter type	Ceramic	Cera	Cera	Ceramic	Ceramic	Ceramic	Ceramic	Cera	Ceramic	Ceramic	Ceramic	Ceramic
Pressure drop; in W.C.	6.4			7.0	7.0	7.6	8.0		()	6.4	6.7	1.1
Filter inlet; ° F	386	392	370	389	382	388	390			375	20,00	392
Filter outlet; ° F	364	389	373	410	368	367	374	376	364	351	363	367
EMISSIONS										•		1
02 %	3.1				3.5	3.4				4.1	3.8	3.7
CO ppm	368				98	115						98
CO2 %	16.1				15.6	15.7	15.5					15.8
SO2 ppm	453			422	221	402	414					384
NOx ppm	545	541	441	269	561	613	999	//9	290	461	610	0/0
ATEC DISCOURT PAGE												
Movimum load												
(based on 14,700 lb steam/h); %	81.2	82.4	80.8	84.2	84.8	84.1	84.8	85.8	82.9	6.77	81.0	79.9
NOTES												
Flue gas temperature leaving air heater and by	Ą											
expansion joint between the air heater and ou	no											
system. First noticeable leak was observed st	st											
3/15/00, and expansion joint was replaced	ă											

TECT /DESCRIPTION:						00, 20, 0	00,00,0	00/01/0	00/00/0	00/16/0	0/22/00	0/22/00
	9/8/00	9/11/00	9/12/00	9/13/00	9/14/00	9/15/00	9/18/00	9/19/00	00/07/6	2/2//2/6	27.57.00	3/13/60
Eliterina Device:	Sleeve 3.5											
Burner Settings:	Center 2											
	Inner 6.5	Inner 6.5	Inner Max	hner Max	Inner Max	Inner Max	Inner 6.5	Inner Max				
	Outer 7.5	Outer 7.5	Outer Max	Outer Max	Outer Max	Outer Max	Outer 7.5	Outer Max				
	Coal Gun -6											
	Gas Gun -6	Gas Gun -6	Gas Gun -2	Gas Gun -2	Gas Gun -2	Gas Gun -2	Gas Gun -6	Sas Gun -2				
	Corning	Clinetream	Clinetraam									
WATER/STEAM SIDE	Slipstream	Slipstream	Slipstream	Slipstream	Shpstream	Silpstream	Supstream	11 001	12 000	11 975	11 793	11 345
Steam flow rate; lb/h	11,861	11,544	11,934	12,048	12,303	12,044	11,47	100,11		0.00	201	231
Water temperature into boiler; °F	231		230	230	157	230	215			212	201	211
Drum pressure; psig	213		500	211	219	214	213		916	212	217	317
Calorimeter temperature; °F	318		318	318	318	318	318		3010	201	301	473
Steam temperature; °F	392		392	392	392	392	392	196	1003	100.2	0.001	1002
Steam quality; %	100.3		100.3	100.3	100.3	100.3	100.3			2.001	2 082	3.186
Blowdown rate; lb/h	1,246	3,184	3,168	3,184	3,197	3,206	3,139	9,191	3,101	3,130	200,0	201.0
AR.FUEL. FLUE GAS SIDE												
Coal Flow rate: lb/h	1,091	1,091	1,091	1,091	1,091	1,091	1,091	1,091	1,091	1,091	1,091	1,091
Coal flow rate: MMBtu/h	14.1		14.5	14.5	14.6	14.6	14.4	14.5	14.4	14.5	14.4	14.5
Roller outlet temperature: "F	618		909	614	622	615	589	909		617	583	592
Gas temperature leaving air heater: °F	409		406	408	410	404	386	401	406	407	389	385
Air temperature entering air heater: °F	182		187	185	182	181	186	183	183	179	187	173
Air temperature leaving air heater: °F	442		441	443	449	444	431	440	440	440	430	424
Air temperature into boiler: °F	404		401	407	412	407	389			403	397	381
Ash content of particulate; %	17.16	82.20	86.63	80.50	76.37	72.51	64.41	_	_	89.99	89.66	72.01
Coal combustion efficiency; %	99.3		98.5	98.3	98.5	97.9	92.6			99.2	99.3	6.96
Combustion air flow; acfm	3,189		3,150	3,183	3,232	3,239	3,047				2,840	3,071
Boiler draft; inches W.C.	-0.09		-0.10	-0.09	-0.09	-0.08	-0.08				-0.15	9.0-
Boiler efficiency; %	87.1	86.0	86.7	86.2	86.2	82.8	84.5		86.7	8.98	86.0	85.5
Mill air flow rate; acfm	403		410	414	414	406	404		409	414	354	404
Mill outlet temperature; °F	213		174	147	142	142	172		174	165	151	158
Filter type	Ceramic	Cere	Ceramic	Ceramic	Ceramic	Ceramic	Ceramic	Cera	Cera	Ceramic	Ceramic	Ceralille
Pressure drop; in W.C.	7.9		2.0	7.1	8.9	7.1	6.4			8.2	9.0	3.7
Filter inlet; ° F	391	368	386	388	390	383	369			388	200	207
Filter outlet; ° F	366	342	362	361	360	352	346	357	377	384	385	330
EMISSIONS						1	000	000	3 6	2.0	8 4	4.2
02 %	3.6	1.00	3.5	0.0	1.07	411	235				82	174
CO ppm	9079			15.7	16.1	15.5	15.3			-		15.0
# ZOJ	13.3			416	428	402	434			455		377
NOV SOM	869		662	674	720	069	485			765		385
MISCELLANEOUS DATA												
Maximum load	100			0 00	02.7	0.18	78 1	2 18	82.3	81.5	80.2	77.2
(based on 14,700 ib steam/h); %	80.7	(0.3	7.10	0.20	2	2						
NOTES												
Flue gas temperature leaving air heater and bi	ā											
expansion joint between the air heater and ou	nc											
system. First noticeable leak was observed st	St											
3/15/00, and expansion joint was replaced be	Þ¢											

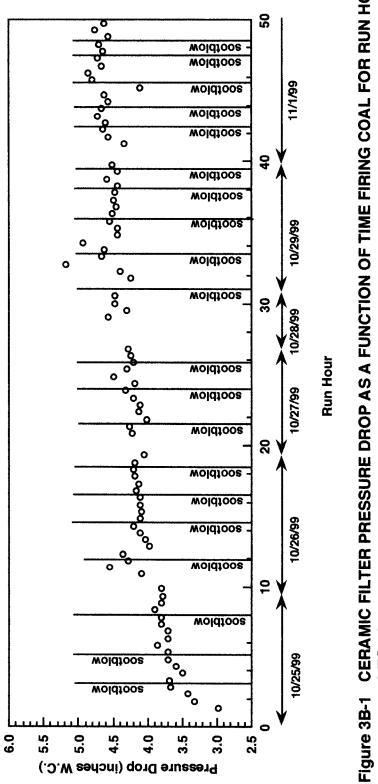
Sleeve 3.5 Sleeve 3.5 Sleeve 3.5 Sleeve 3.5 Sleeve 3.5 Center 2 Center 3 Ce	NO.	9/26/00	9/27/00	9/28/00	4/17/01	4/19/01	4/20/01	4/23/01	4/24/01	4/25/01	4/26/01	4/27/01	4/30/01
Center 2   Steeve 3										L c		0.00	3 6 4 10 13
Conter 2   Center 2   Center 2   Center 3		Sleeve 3.5	Sleeve 3.5	Sleeve 3.5	Sleeve 3.5	Sleeve 3.5							
Coal Gan 6   Coa		Center 2	Center 2	Center 2	Center 2	z aluar							
Coal Gan, 6   Cast Gan, 6		Inner 6.5	luner 6.5	Inner 6.5	Inner 6.5	Inner 6.5	Inner 6.5	Inner max	inner 0.5				
Coal Gun-6   Coa		Outer 7.5	Outer 7.5	Outer 7.5	Outer max	Outer 7.3							
Conting		Coal Gun -6	Coal Gun -6.5	Coal Gun -6.5	Coal Gun -6.5	Coal Gun -6.3	Coal Guil -0						
Signaturan		Gas Gun -6	cas cun -o	cas con -o	o- uno seo	Ods Gull -O							
1,001		Corning	Corning	Corning									
1,315   1,700   1,137   1,271   1,270   1,137   1,13		Slipstream	Supstream	Sipstream	11 241	12 205	12 625	12 437	11 597	12.259	12.884	12,993	12,546
1,091   1,091   1,091   1,1140   1,1	b/h	916,11	11,780	11,344	150	230	230	230		231	231	230	231
The color of the	e into boiler; 'F	231	167	010		216	219	216		215			213
PE         317         317         317         317         317         317         317         3177         3177         3176         3196         3217         3317         3177         3177         3176         3196         3217         3317         3177         3177         3176         3196         3217         3317         3177         3177         3176         3196         3217         331         3217         331         3217         331         3217         331         331         321         331         321         331         321         331         321         331         321         321         331         321         321         331         321         321         331         321         321         331         321	Sig	210	017	21.5		217	317	318		316			317
DE	erature; *F	317	317	317	301	397	392	393	393	391	391		391
DE	.e. 1	100.2	465	100.2		1001	1001	1001	100.1	100.0	100.0	1001	1001
DE         1,091         1,091         1,091         1,140         1           F         1,091         1,091         1,091         1,140         1           F         1,091         1,091         1,091         1,140         1           air heater, F         609         617         620         588         605           air heater, F         175         122         176         137         140         17           lei, T         175         122         176         176         177         143         144         421         421         431         144         421         431         144         421         431         144         421         431         144         421         431         144         421         431         144         421         431         144         421         431         144         421         431         144         421         431         144         421         431         144         421         431         432         432         432         432         432         432         432         432         432         432         432         432         432         432         432         432	1	2.177	3 177	3.176		3.217	3.207	3,218				3,213	3,200
DE         1,091         1,091         1,140         1           e; F         609         617         620         588         605           air heater; F         609         617         620         588         605           air heater; F         609         617         620         588         605           air heater; F         609         617         620         379         395           teir heater; F         338         401         176         177         164           teir heater; F         338         401         176         378         389           teir heater; F         83.84         84.54         88.58         64.36         69.34         7           teir heater; F         83.84         84.54         88.58         64.36         69.34         7           teir heater; F         83.84         94.54         88.58         64.36         69.34         7           teir heater; F         83.7         86.2         86.2         86.2         86.2         80.6         80.6           teir heater         63.7         86.2         86.2         86.2         86.2         86.2         86.2         86.2         86.2 <td>u/c</td> <td>2,1,7</td> <td>3,1,5</td> <td>5</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>,</td> <td></td> <td></td>	u/c	2,1,7	3,1,5	5							,		
1,091   1,091   1,091   1,140   1   1,091   1,140   1   1,146   1,14	GAS SIDE												,
14.6   14.5   14.6   14.5   14.6   14.5   14.6   14.5   14.6   14.5   14.6   14.5   14.6   14.5   14.6   14.5   14.6   14.5   14.6   14.5	-	1,091	1,091	1,091	1,091	1,140	1,164	1,158	1,158	1,158	1,158		1,158
air heater; F 609 617 620 588 605 air heater; F 138 401 402 379 355 1 air heater; F 138 401 412 114 1 air heater; F 138 401 115 1 air heater; F 139 401 115 1 air heater; F 139 401 116 1 air heater; F 139 401 116 1 air heater; F 139 401 117 1 air heater; F 139 401 117 1 air heater; F 139 401 117 1 air heater; F 139 113 114 1 air heater; F 139 114 1 air heater; F 130 114 1 air heater; F 130 114 1 air heater; F 130 114 1 air heater and b.  air heater; F 130 114 1 air heater and b.  air heater; F 130 114 1 air heater and b.	4Btu/h	14.6	14.5	14.6	14.3	14.6	15	15.0	15.2	15.3	15.5		15.5
Part	perature: °F	609	219	620	588	909	209	009	587	603	604		591
rature entering air heater, Trong in Models         175         122         176         187         164           rature intering air heater, Trong in heat	leaving air heater; °F	398	401	405	379	395	396	403	391		397		399
Particle leaving air heater, T   435   438   441   421   431   4	entering air heater: °F	175	122	176		164	160	189			164		179
antific boller; F	eaving air heater: °F	435	438	441		431	428	439	432	424	425		431
nt of particulate; % 83.84 84.54 83.58 64.36 69.34 77 or between leaving air heater and but the integration of particulate; % 83.84 84.5 98.6 95.5 96.1 3.202 3.202 3.202 3.202 3.202 3.202 3.202 3.202 3.202 3.202 3.202 3.203 3.202 3.203 3.2	nto boiler: °F	395	401	176		389	388	397					391
Number of fincipancy; %         94.8         98.7         98.6         95.5         96.1           nn air flow; acfm         3,140         3,153         3,148         3,023         3,202         3           nn air flow; acfm         3,140         3,153         3,148         3,023         3,202         3           ciency; %         8.0.C         6.009         -0,09         -0,09         -0,09         -0,01         -0,01           ciency; %         8.0.C         86.2         86.3         413         124         -0,1           ciency; %         8.0.E         86.2         86.3         411         406         412           ciency; %         8.0.E         86.3         411         406         412         -0.1         -0.1           ciency; %         8.0.E         8.0.E         86.3         411         406         412         -0.1	articulate; %	83.84	84.54	83.58		69.34	72.29	70.54	7	9			75.61
Trienches W.C.         3,140         3,153         3,148         3,023         3,202         3           Clency; %         Construction         -0.09         -0.09         -0.08         -0.01         -0.01           Clency; %         Sa;7         66,2         86,3         86,3         86,3         80,6         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01         -0.08         -0.01	efficiency; %	94.8	7.86	98.6		96.1	6.96	96.8					97.1
t, inches W.C.         0.09         -0.09         -0.09         -0.09         -0.08         -0.01           ciency; %         83.7         86.2         86.3         84.3         80.6         -0.01           ciency; %         83.7         86.2         86.3         84.3         80.6         -0.01           w rate; acfm         172         141         149         133         124         142           temperature; "F         7         7.2         7.2         7.5         9.2         7.8         124	ow; acfm	3,140	3,153			3,202	3,273	3,300					3,213
ciency, %         88.7         86.2         86.3         84.3         80.6           w rate; acfm         396         392         411         406         412           temperature; F         172         172         411         149         133         124           frop; in W.C.         6.8         7.2         7.5         9.2         7.8           frop; in W.C.         6.8         7.2         7.5         9.2         7.8           frop; in W.C.         6.8         3.6         3.6         3.6         403           st; or         3.6         3.6         3.6         403         3.5           st; or         3.6         3.6         3.6         403         3.5           st; or         3.6         3.6         3.6         4.6         4.48           st; or         3.6         3.6         4.6         4.48         3.6         4.6         4.48           st; or         3.6         3.6         3.6         3.6         4.6         4.48         4.8           st; or         3.6         3.6         3.6         4.6         4.48         4.6         4.48         4.8           st; or         3.6 <td>ss W.C.</td> <td>-0.09</td> <td>60.0-</td> <td></td> <td></td> <td>-0.1</td> <td>60.0-</td> <td>-0.08</td> <td></td> <td></td> <td>-0.07</td> <td></td> <td>-0.07</td>	ss W.C.	-0.09	60.0-			-0.1	60.0-	-0.08			-0.07		-0.07
temperature; 'F         396         392         411         406         412           temperature; 'F         172         141         149         133         124           temperature; 'F         Ceramic         C	8	83.7	86.2	86.3		80.6	84.8	85.0			85.4		85.2
temperature; "F         172         141         149         133         124           tep; In W.C.         Ceramic         Ceramic <td>acfm</td> <td>396</td> <td>392</td> <td>411</td> <td>406</td> <td>412</td> <td>411</td> <td>415</td> <td></td> <td></td> <td>405</td> <td>ļ</td> <td>404</td>	acfm	396	392	411	406	412	411	415			405	ļ	404
Part	rature; °F	172	141	149		124	125	132			164		180
Incomposition         Incompos		Ceramic	Ceramic	Ceramic	Cera	Ceramic	Ceramic	Ceramic	Ē	Cera	3	Cera	Ceramic
S 361 384 386 561 403  S 36 356 367 368 321 355  S 36 367 368 321 355  S 36 36 367 368 321 355  S 36 36 36 367  I 12 255 140 105 69  I 15 6 15,0 15,6 15,4 15,8  I 16 628 721 571 545  I 14,700 lb steam/h); % 81.1 80.1 81.3 76.5 83.0  Emperature leaving air heater and but the air heater and out to the air	W.C.	6.8	7.2	7.5		7.8	8.2	8.2					2.1
S		381	384	386		403	434	386					385
S   3.6   3.7   3.6   3.5   3.5		356	367	368		355	341	356	335	347	339	354	346
112   255   140   105   69   110   112   255   140   105   69   112   15.6   15.6   15.6   15.6   15.6   15.6   15.6   15.8													i c
112   255   140   105   69     156   15,6   15,8   15,8     156   15,6   15,8   15,8     157   15,8   15,8     158   15,8   15,8     158   15,8   15,8     158   15,8   15,8     158   158   15,8     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158   158     158   158     158   158   158     158   158   158     158   158   158     158   158     158   158   158     158   158   158     158		3.6		3.6		3.5	3.4	3.2					3.5
15.6   15.0   15.8   15.8   15.8   15.9   15.8   15.8   15.9   15.8   15.9   15.8		112				69	82	75					
NEOUS DATA   80.1   80.1   81.3   76.5   83.0		15.6				15.8	15.8	16.0					
NEOUS DATA  INEOUS DATA  Inad		391				448	460	434					486
NEOUS DATA   14,700 lb steam/h); %   81.1   80.1   81.3   76.5   83.0     14,700 lb steam/h); %   81.1   80.1   81.3   76.5   83.0     81.2   82.0       82.0       82.0       82.0		646		721	571	545	634	630	208	591	209	528	/79
81.1 80.1 81.3 76.5 83.0													
81.1 80.1 81.3 76.5 83.0													
81.1 80.1 81.3 76.5 83.0	DAIA												
	70 H ctcom /h): 96	118		81.3			85.9	84.6	78.9	83.4	87.6	88.4	85.3
NOTES Flue gas temperature leaving air heater and b expansion joint between the air heater and ou	O ID stealingly, 70	0											
Five gas temperature leaving air heater and bi expansion joint between the air heater and ou													
expansion joint between the air heater and ou	ture leaving air heater and b												
Times and and an about the second of	etween the air heater and ou												
system. First noticeable leak was observed at	system. First noticeable leak was observed st												
3/15/00, and expansion joint was replaced bt	pansion joint was replaced be			-									

										10/01/0	20/30/1	4720702
TEST/DESCRIPTION:	5/1/01	5/3/01	2/9/01	5/15/01	5/17/01	5/22/01	5/24/01	5/3//01	10/6/9	0/17/01	7/ 50/ 05	20,02
Tilk culture Double	Sleeve 3.5											
Filtering Device.	Center 2											
partie securids.	Inner 6 5	Inner 6 5	Inner 6.5									
	Outer 7.5											
	Coal Gun -6											
	Gas Gun -6	Coal Gun -6	Gas Gun -6	Coal Gun -6	Gas Gun -6	Coal Gun -6	Coal Gun -6	Coal Gun -6				
WATER/CIEAN SIDE												
Steam flow rate: lh/h	12.320	11.967	11.735	12,186	12,019	9,107	9,158	11,870	690'6	11,950	12,025	12,442
Motor tomographic into holler °F	230	231	230	231	230	231	231	231		230	234	234
Deim pressure nsid	210			210	210	214	214	215		211	234	229
Calcrimater temperature "F	316			316	316	316	316	317		317	319	320
Steam temperature: °F	391		391	390	390	392	392	392			397.7	395.9
Steam quality: %	100.1	100.1	1001	100.1	100.1	100.0	100.0	100.1				100.0
Blowdown rate; lb/h	3,176	3,177	3,180	3,176	3,178	3,208	3,208	3,211	3,190	3,183	3,351	3,317
AIR, FUEL, FLUE GAS SIDE	.00	1001	1001	1 00 1	1 091	830	829.8	1.091	830	1,091	1,158	1,158
Coal Flow rate; lb/h	190,1		160,1	1.60,1	14.2	10.5	10.7	14.3		13.9		15.4
Coal flow rate; MMBtu/h	14.6	13.0		40.5	589	591	575	602		615	298	296
Boller outlet temperature; F	409			400	397	395	387	409		414	393	388
Sas temperature leaving air heater, r	189			179	174	194	199	170	197	196	168	148
Air temperature leaving all lieater, r	442			435	428	442	439	428	434	448		412
Air temporature into holler. "F	401			393	388	396	394	389	390	409		374
Ash content of particulate: %	75.78	7		77.20	79.96	80.82	80.71	83.38			,	65.00
Coal combustion efficiency: %	6.96		N.M.	97.1	97.6	97.3	97.8					1.96.1
Combustion air flow; acfm	3,179	3,128	3,133	3,123	3,202	2,707	2,475					3,300
Boiler draft; inches W.C.	-0.08	60.0-		60:0-	-0.09	-0.09	-0.09					6.03
Boiler efficiency; %	84.9	84.2		85.3	85.6	85.0	85.9					403
Mill air flow rate; acfm	406				391	393	355				104	ממר
Mill outlet temperature; "F	171				163	165				Coramic	و	Ceramic
Filter type	Ceramic	<u>.</u>	Ē	Ceramic	Fabric	Fabric	20	1	rapric			10.6
Pressure drop; in W.C.	11.5			11.4	9.7	2	07.6	6.7				364
Filter inlet; °F	390			382	380	370					,	327
Filter outlet; ° F	359	352	338	344	324	319	311	344	308			770
EMISSIONS				7.0	0.0	4 8	3.3	0.5	3.7	6.5	3.3	3.5
02 %	3.8	3.0	3.0			95	65					109
CO ppm	727			-		14.7	_	14.4	15.4	12.4	14.7	14.4
% ZOO	417					359		331	405	335	N/A	N/A
NOv man	611			585	622	598	640	628	9 670	431	N/A	N/A
MISCELLANEOUS DATA												
Maximum load					0	0.63	623	80.7	7 19	813	81.8	84.6
(based on 14,700 lb steam/h); %	83.8	4.18	79.8	6.20								
NOTES												
Fine cas temperature leaving air heater and bo	φp											
expansion joint between the air heater and ou	no											
system. First noticeable leak was observed st	d st											
3/15/00, and expansion joint was replaced be	d be											

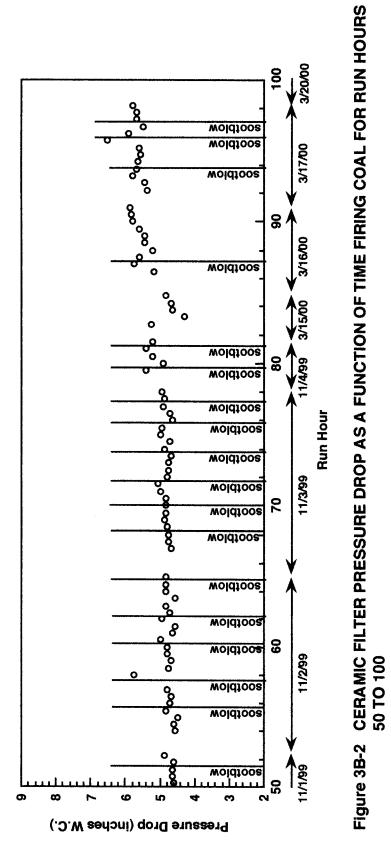
	TEST/DESCRIPTION:	8/28/02	8/30/05	9/2/02	9/26/02	10/7/02	10/14/02	5/15/03	6/17/03
Supplementary   Supplementar			i.	L	0	7 6 010013	Cloove 3 5	Cleeve 3.5	Sleeve 3.5
Content	iltering Device:	Sleeve 3.5	Seeve 3.3	Center 2	Center 2				
Contact   Cont	Burner Settings:	Center 2	laner 6 5	Inner 6.5					
Coal Gan - 6   Coa		Inner 6.5	mier 6.5	Outor 7 E	Outer 7.5				
EV. T.         Coal Gan. 6 Coal Ga		Outer 7.5	Cast Cira 6	Coal Gim -6	Coal Gin -6				
For the control of th		Coal Gun -6							
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	Later than the second s								
Part	WATER/STEAM SIDE	12 721	12 663	12 644	11.059	11.962	11,757	12,160	12,338
1	steam flow rate; ID/II	230	232	231	235	235	232	232	222
100   100	water temperature into bouer; r	200	222	221	223	231	229	228	223
100   100	Jrum pressure; psig	317	319	314	318	319	318	319	319
1000   1000	alorimeter temperature; r	395.8	395	395	399	397	396	397	395
2005 SIDE   1,164	thom mulity 04	10001	100.0	100.0	100.0	100.0	100.0	100.0	100.0
1,164   1,164   1,164   1,164   1,165   1,152   1,15	Slowdown rate; lb/h	3,279	3,271	3,262	3,388	3,334	3,317	3,309	3,274
1,164   1,164   1,164   1,164   1,152   1,15									
15.5   15.7   15.2   15.2   15.4   15.5   15.5     15.6   6.06   6.08   6.08   6.18   6.18   6.18     17.7   16.6   182   182   187   169   150   177     17.7   16.6   182   182   182   404   412   418     24.0   40.2   3.69   3.69   3.69   3.69   406   40.2     25.2   3.69   3.250   3.250   6.021   6.820   6.540   6.950   7.1     25.2   3.69   3.250   3.250   3.250   3.251   3.139   3.139     25.2   3.69   3.250   3.250   0.09   0.09   0.09   0.09     25.3   3.69   3.250   3.250   3.251   3.139   3.139     25.3   3.69   3.250   3.250   0.09   0.09   0.09   0.09     25.3   3.69   3.60   3.60   3.50   3.251   3.141   3.64     25.3   3.60   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60   3.60     25.3   3.60   3.60   3.60   3.60     25		1.164	1.164	1,164	1,164	1,152	1,152	1,152	1,152
177   166   620   650   654   613   616   620	Coal flow rate: MMRtu/h	15.5	15.7	15.2	15.2	15.4	15.4	15.2	15.0
177   186   410   412   378   404   419   419   419   418	Soiler outlet temperature: "F	909	620	809	584	613	919	630	618
177   166	as temperature leaving air heater; "F	395	404	412	378	404	401	419	409
18	Vir temperature entering air heater; °F	177	166	182	157	169	150	1771	168
rotube into bolles; 'f         376         386         402         366         391         388         406           rot of percloalets; 'fs         64.01         62.70         73.0         60.21         68.20         69.50         77           not of percloalets; 'fs         65.2         95.2         95.7         96.8         94.3         96.9         96.5         <	ir temperature leaving air heater; "F	418	436	439	407	429	426	447	432
Interperature   Faving   Fav	Air temperature into boiler; "F	376	396	405	366	391	388	406	391
Number Structure (Frichency, % of the branch of the leaving air heater and b of the structure (Frichency, % of the structure)         95.7 96.8 94.3 3.539         94.3 3.539         94.4 7 9.59         94.9 9.5 9 9.4 9.7 9.9 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7	Ash content of particulate; %	64.01	62.70	73.30	60.21	68.20	65.40	69.50	0.90
Nu circle Mr.C.  Nu ci	coal combustion efficiency; %	95.2	95.7	96.8		95.9	94.7	96.6	90.3
t; inches W.C.         0.09         -0.09	Combustion air flow; acfm	3,443	3,589	3,250		3,227		3,139	3,240
Part	Soiler draft; inches W.C.	60:0-	-0.09	-0.09	-0.09	60.0-		-0.07	-0.03
temperature; F   189   1802   1804   1804   1804   1804   1804   1805	3oiler efficiency; %	83.0	83.0	84.8	83.2	83.9	82.9	83.4	84.0
temperature if several control contro	Aill air flow rate; acfm	399	400	406	397	404	402	401	904
100   100	Mill outlet temperature; "F	188	180.2	182.8	164	174	163	2/1	imera)
10.3   9.4   9.8   9.5   9.0   9.7   9.0     10.3   9.4   9.8   9.8   9.5   9.0     1.5	filter type	Ceramic	Ceramic	Ceramic	Ceramic	Ceramic	Cera	Ceramic	11.2
• F         NA A         388         388         389         NA A         339         NA A         339         NA A         339         NA A         339         348         341         350         350         351         356         357         358         351         358         351         358         351         358         351         358         351         358         37         37         70         70         70         70         70         475         70         475         70         475         70         465	Pressure drop; in W.C.	10.3	9.4	9.8	9.8	9.0			2.1.
S.         357         355         362         315         348         341         364           S.         4.3         4.7         3.3         4.0         3.5         3.7         3.3           S.         4.7         3.3         4.0         3.5         3.7         3.3         7.0           A.         3.7         5.3         2.7         14.3         5.0         4.7         7.0           A.         4.31         3.84         4.84         4.84         4.84         4.85         4.7         7.0           NEOUS DATA         4.59         4.44         5.14         3.58         5.23         4.83         5.81           I.14,700 lb steam/h); %         86.5         86.1         86.0         75.2         81.4         80.0         82.7           Emperature leaving air heater and outlooticeable leak was observed st         86.1         86.0         75.2         81.4         80.0         82.7	liter inlet; °F	389	388	392	357	394			35.0
SS         4.3         4.7         3.3         4.0         3.5         3.7         3.3           NEOUS DATA         4.3         86.5         86.1         86.0         86.1         86.1         86.0         86.1         86.0         86.1         86.0         86.1         86.0         86.1         86.1 </td <td>filter outlet; ° F</td> <td>357</td> <td>355</td> <td>362</td> <td>315</td> <td>348</td> <td>341</td> <td>364</td> <td>360</td>	filter outlet; ° F	357	355	362	315	348	341	364	360
NEOUS DATA  NEOUS DATA  THIS INSTITUTE leaving air heater and ou light between the air heater and ou l	EMISSIONS		17	0.0	7.0	2 2			3.6
NEOUS DATA   14.7   1	32 %	7.0	2	7.0	143				47
NEOUS DATA   489   484   489   436   416   470   465     NEOUS DATA   86.5   86.1   86.0   75.2   81.4   80.0   82.7     I 4,700 lb steam/h); %   86.5   86.1   86.0   75.2   81.4   80.0   82.7     I a 7.700 lb steam/h); %   86.5   86.1   86.0   75.2   81.4   80.0   82.7     I a 7.700 lb steam/h); %   86.5   86.1   86.0   75.2   81.4   80.0   82.7     I a 7.700 lb steam/h); %   86.5   86.1   86.0   82.7     I a 7.700 lb steam/h); %   86.5   86.1   86.0   82.7     I a 7.700 lb steam/h); %   86.5   86.1   86.0   75.2   81.4   80.0   82.7     I a 7.700 lb steam/h); %   86.5   86.1   86.0   82.7     I a 7.700 lb steam/h); %   86.5   86.1   86.0   82.7     I a 7.700 lb steam/h); %   86.5   86.1   86.0   82.7     I a 7.700 lb steam/h); %   86.5   86.1   86.0     I a 7.700 lb steam/h); %   86.5   86.1   86.0     I a 7.700 lb steam/h); %   86.5   86.1   86.0     I a 7.700 lb steam/h); %   86.5   86.1   86.0     I a 7.700 lb steam/h); %   86.5   86.1   86.0     I a 7.700 lb steam/h); %   86.5   86.1   86.0     I a 7.700 lb steam/h); %   86.5   86.1     I a 7.700 lb steam/h); %   86.5   86.1     I a 7.700 lb steam/h); %   86.5   86.1     I a 7.700 lb steam/h); %   86.5     I a 7.700 lb steam/h, %   86.5     I a 7.700	O ppm	16	13.4	15.2	144			-	14.4
NEOUS DATA         459         444         514         358         523         483         581           NEOUS DATA         load           14,700 lb steam/h); %         86.5         86.1         86.0         75.2         81.4         80.0         82.7           emperature leaving air heater and bujoint between the air heater and outlineable leak was observed st           14,700 lb steam and outlineable leak was observed st           14,700 lb steam and outlineable leak was observed st	00 %	421	384	484	436	416			476
86.5 86.1 86.0 75.2 81.4 80.0 82.7	NOx ppm	459	444	514	358	523			527
86.5 86.1 86.0 75.2 81.4 80.0 82.7									
	Maximum load	2 98 5	86.1	86.0		81.4			83.6
NOTES   Flue gas temperature leaving air heater and b. expansion joint between the air heater and ou system. First noticeable leak was observed st	(based on 14,700 to steam/11); 70								
Flue gas temperature leaving air heater and b expansion joint between the air heater and ou system. First noticeable leak was observed st									
expansion joint between the air heater and ou system. First noticeable leak was observed st	Flue gas temperature leaving air heater ar	đ pu							
system. First noticeable leak was observed st	expansion joint between the air heater an	d ou							
	system. First noticeable leak was observe	ed st							

#### Appendix 3B

**Ceramic Filter Chamber Pressure Drop as a Function of Time Firing Coal** 



CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 0 TO 50



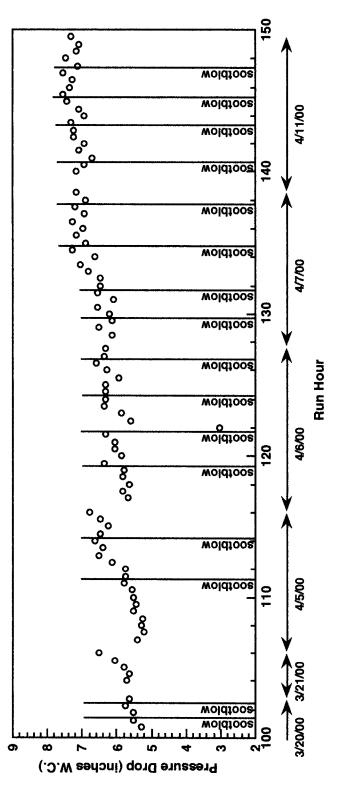


Figure 3B-3 CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 100 TO 150

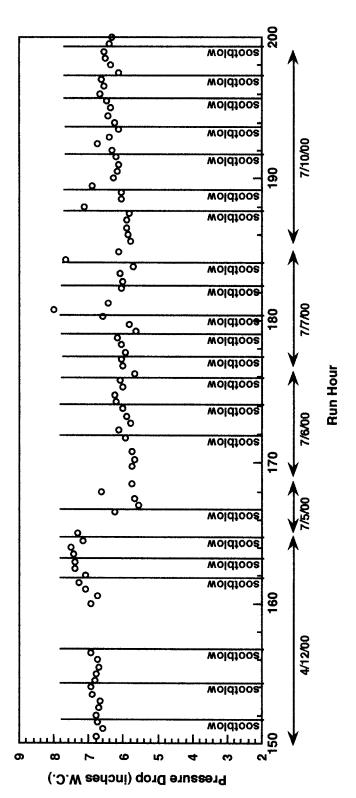


Figure 3B-4 CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 150 TO 200

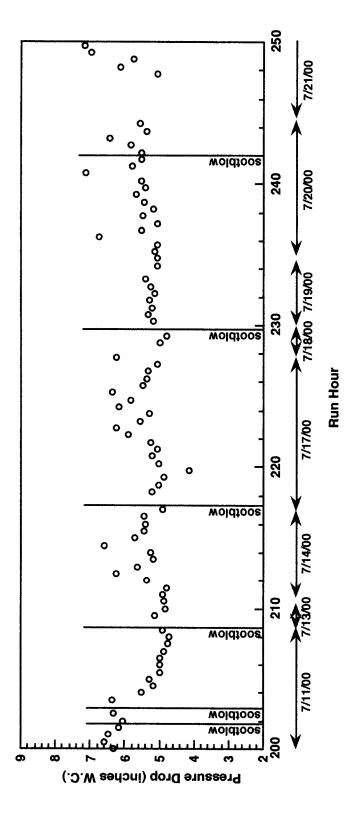


Figure 3B-5 CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 200 TO 250

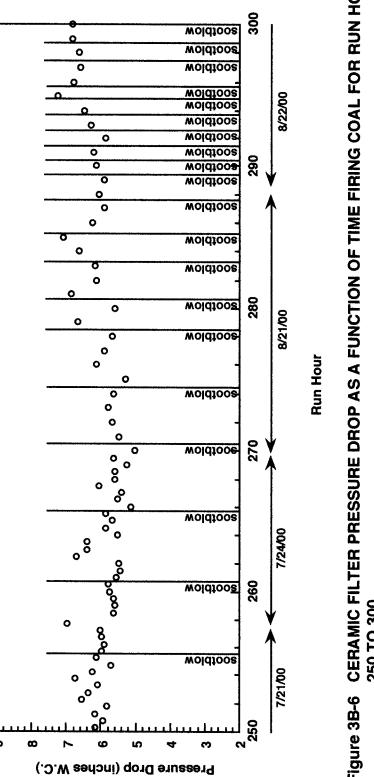
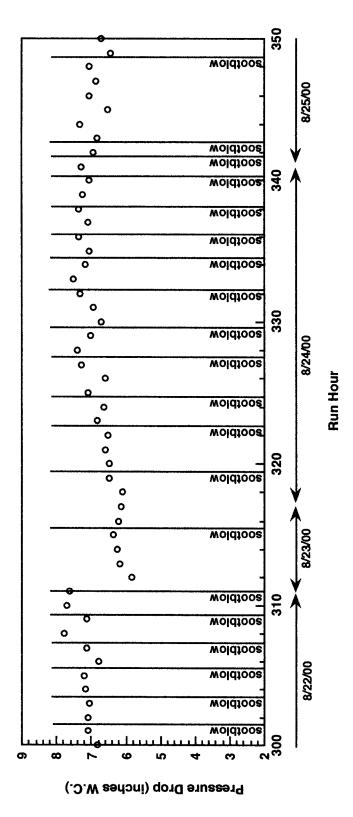
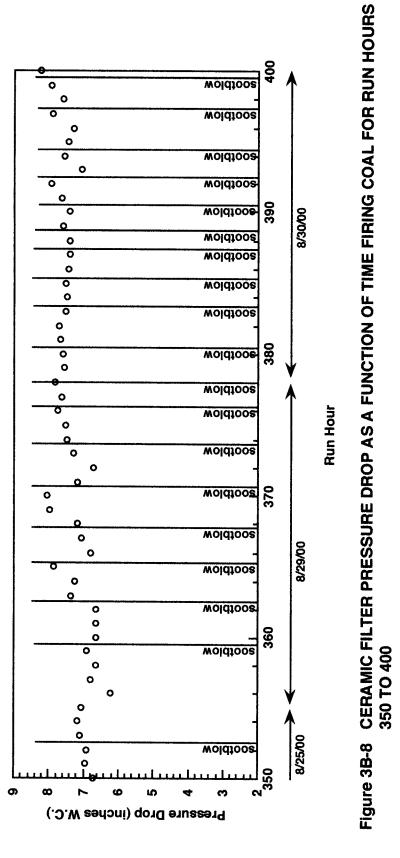
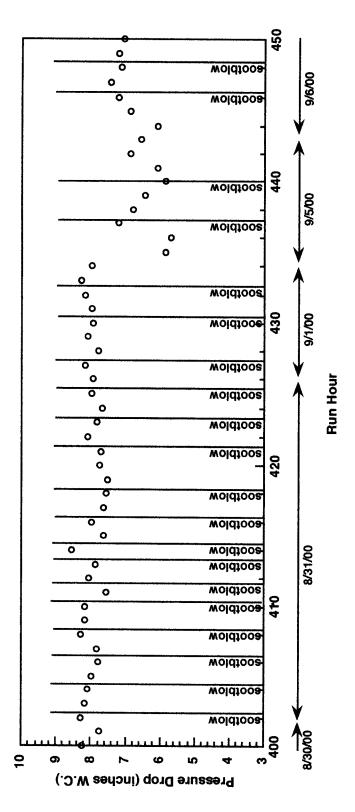


Figure 3B-6 CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 250 TO 300

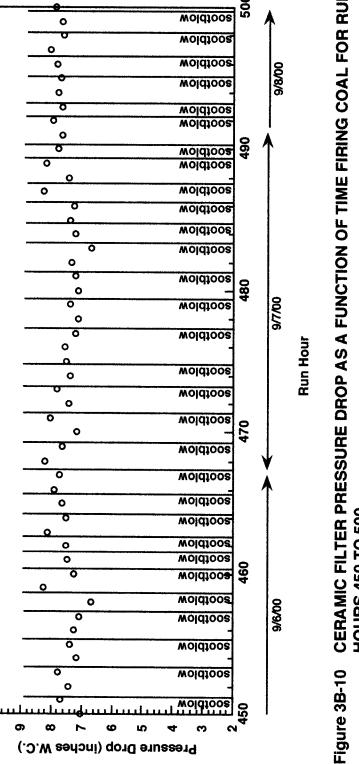


CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 300 TO 350 Figure 3B-7



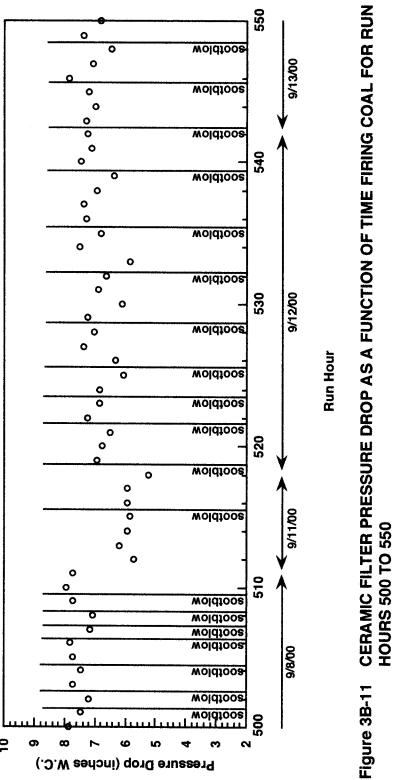


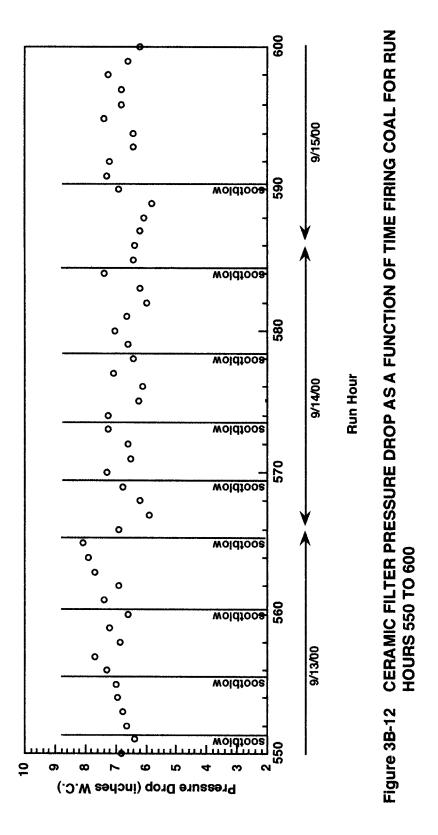
CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 400 TO 450 Figure 3B-9

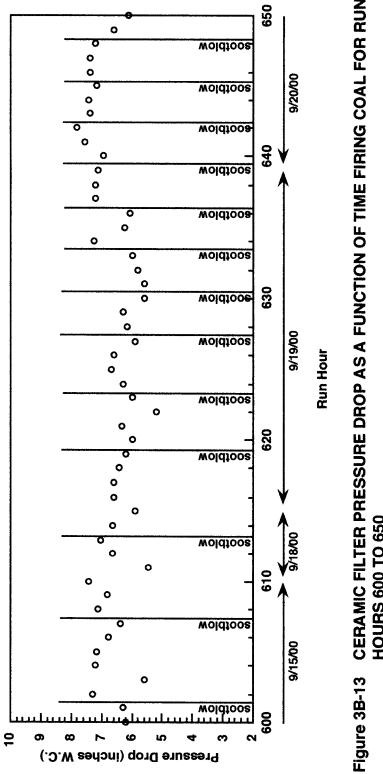


9

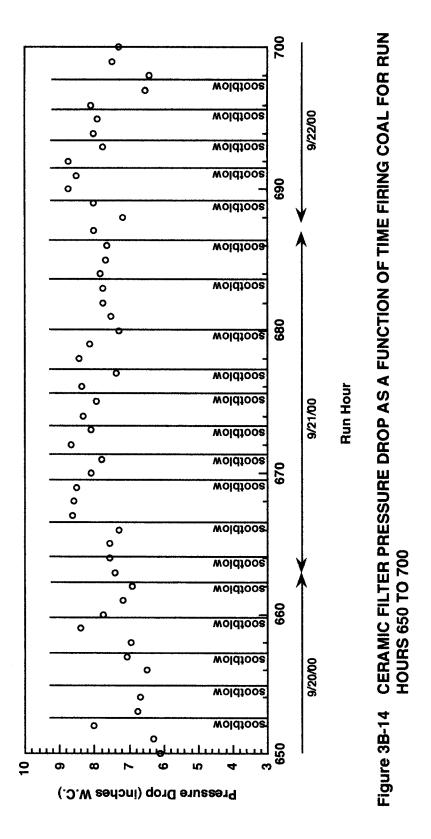
CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 450 TO 500

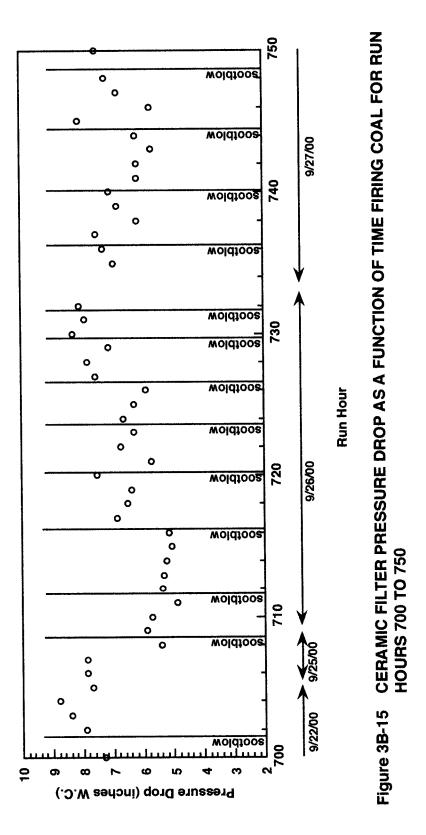


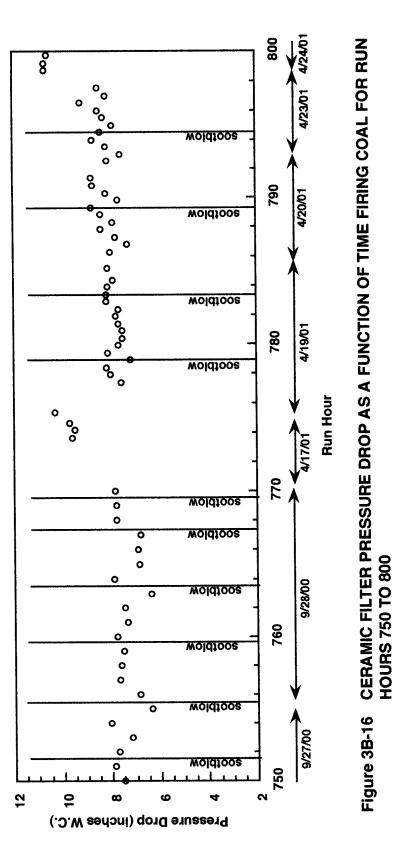


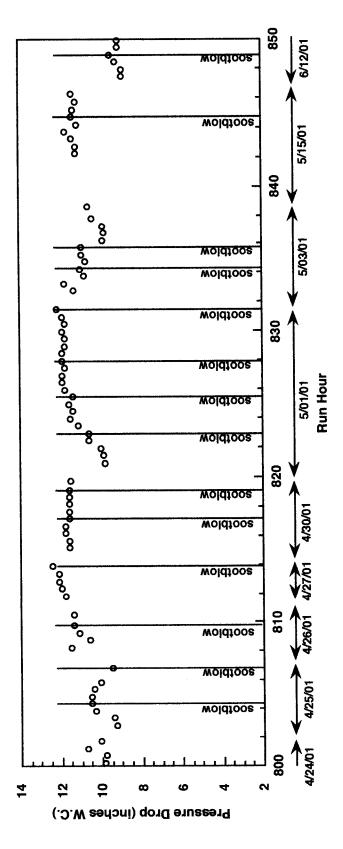


CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 600 TO 650

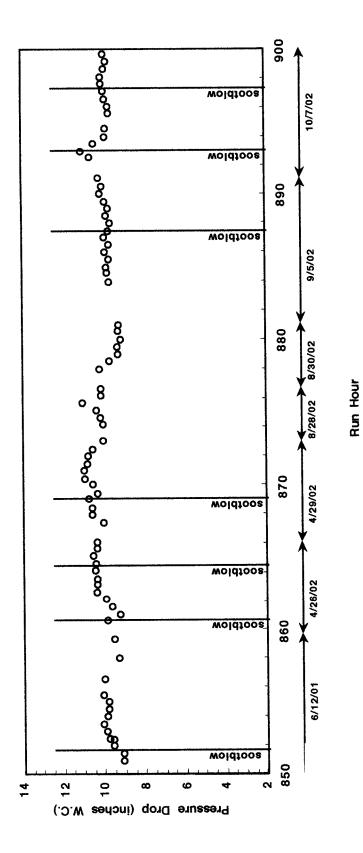




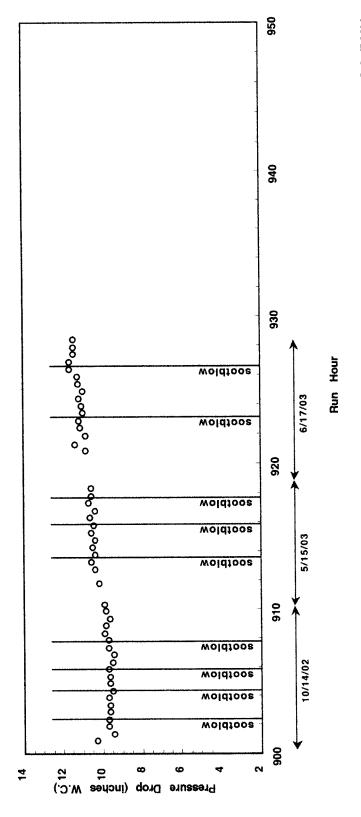




CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 800 TO 850 Figure 3B-17



CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 850 TO 900 Figure 3B-18



CERAMIC FILTER PRESSURE DROP AS A FUNCTION OF TIME FIRING COAL FOR RUN HOURS 900 TO 950 Figure 3B-19

#### **Appendix 4A**

#### Market Penetration Model Source Code Listing

```
STITLE OPTIMAL ALLOCATION OF BOILER RETROFITS
SOFFUPPER
  This model determines the optimal allocation of retrofitted boilers
  in the Indiana and Cambria county region among the installed base
  of water tube boilers. The approach is to use a transportation model
  that considers the costs to produce the boiler retrofit fuel, the costs
  to transport MCWM to the retrofitted boilers, and the capital and
* O&M costs of retrofitting. The transportation model framework minimizes
* the costs to boiler owners given the location of each boiler, and its
* individual characteristics, and the location of each possible source of
* MCWM. The decision to retrofit is assumed to be made if the total costs
* of retrofitting are less than the costs to continue firing oil or gas.
        AUTHOR: A. Michael Schaal
          DATE: March 3, 1995
       Revised: April 17, 1995 - Updated MCWM and retrofit cost curve
SETS
       fuel supply points / GAS, COAL1 * COAL8 /
    i
                               / BLR1 * BLR18 /
    j
       boilers
       mine characteristics / ASH, SULFUR, OUTPUT / boiler locations / 15701, 15901, 16330, 15931 /
      boiler locations
    LABELS for boiler plant data
        / BSIZE boiler size in MMBtu per hour
           UTIL
                   average annual boiler utilization in %
                   boiler's price of gas
           PGAS
                   boiler location's zip code
           BLOC
                   total capital requirement to retrofit boiler /
           TCR
SCALARS
          % additional mine output due to MCWM
                                                          100.0
  MFACT
  CMOIST coal moisture content in %
                                                      /
                                                            0.0
          price of chunk coal f.o.b. mine
                                                              0.0
  PCOAL
                                                       / 12810
  CHHV
           coal higher heating value in Btu per lb
  CWMHV MCWM higher heating value in Btu per lb / 14000
                                                          1190
                                                     /
  STHV
          heat content of steam in Btu per lb
                                                            5.60
  ASHCST coal ash disposal cost in $ per ton
                                                             0.168
  FXUNLD fixed cost to unload MCWM in $ per MMBtu /
  VARUNLD transport cost in $ per MMBtu per mile / 0.00373

ASHPER dry basis weight percent ash in MCWM / 5.00

PIFACT annual P+I on $1000 at 4% and 20 years / 73.582

FXOMFACT fixed O&M maint. cost as a % of capital / 2.0
                                                              0.00373
```

```
MINE(i)
                  annual mine coal output in tons
 FS(i)
                  annual fuel available from each site in MMBtu
 DIST(i,1)
                  distance from ith fuel source to 1th town in miles
                  distance from ith fuel source to jth boiler in miles
 BDIST(i,j)
 BOILER(j, LABELS) boiler plant data
                   annual boiler demand for fuel in MMBtu
                   annualized TCR to retrofit jth boiler
 ATCR(j)
                  non-transport costs less production costs in \$ per MMBtu
 FUELFC(i,j)
                   price of chunk coal in $ per MMBtu
 PCOALM
                  MCWM transport cost in $ per MMBtu
 TCOST(i,j)
PARAMETER MINE(i)
                tpy
     / COAL1 1686875
       COAL2
             878230
              870403
       COAL3
       COAL4
             258030
       COAL5
             188760
       COAL6
             865017
             485980
       COAL7
       COAL8
            282732 /
 TABLE DIST(i,1)
              15701
                       15901
                                16330
                                         15931
   GAS
                 0
                          0
                                   0
                                             0
                                    9
                                             3
                 30
                          23
   COAL1
                 22
                         35
                                   32
                                            20
   COAL2
   COAL3
                 20
                         40
                                   33
                                            25
                40
                         44
                                   32
                                            22
   COAL4
   COAL5
                45
                         15
                                   35
                                            29
                30
                         42
                                   57
   COAL6
                                            51
   COAL7
                14
                         44
                                   43
                                            36
   COAL8
                23
                         19
                                   33
                                            26
 TABLE BOILER (j, LABELS)
             BSIZE
                      UTIL
                              PGAS
                                      BLOC
                                               TCR
            MMBtu/hr
                       용
                             $/MMBtu
                                      zip
                                               $M
                                              5.01
   BLR1
              68.0
                       60
                             3.62
                                      15701
   BLR2
              50.4
                       53
                              3.62
                                      15901
                                              4.22
   BLR3
              50.4
                       53
                              3.62
                                      15901
                                              4.22
                             3.62
                      53
   BLR4
              50.4
                                      15901
                                              4.22
             50.4
                             3.62
3.62
                      53
                                              4.22
   BLR5
                                      15901
              68.0
                      60
   BLR6
                                      15701
                                              5.01
                             3.62
             19.4
                      50
                                              2.43
   BLR7
                                      15901
                             3.62
   BLR8
             19.4
                       50
                                      15901
                                              2.43
                      5
   BLR9
             11.6
                             4.50
                                      15901
                                              1.81
   BLR10
             11.6
                       5
                             4.50
                                      15901
                                              1.81
                     30
                             3.62
              27.7
                                      16330
                                              2.99
   BLR11
                             3.62
                     30
                                              2.99
   BLR12
              27.7
                                      16330
                             3.62
                      30
   BLR13
              27.7
                                      16330
                                              2.99
                             3.62
                       30
   BLR14
              11.6
                                      15901
                                              1.81
   BLR15
              11.6
                       30
                              3.62
                                      15901
                                              1.81
                              3.62
   BLR16
              11.6
                       30
                                      15901
                                              1.81
                             3.62
              53.2
                                      15901
                                              4.35
   BLR17
                        1
              94.5
                        5
   BLR18
                              3.62
                                      15931
                                              6.06
 BDIST(i,j) $ (BOILER(j, "BLOC") EQ 15701) = DIST(i, "15701") ;
 BDIST(i,j) $ (BOILER(j, "BLOC") EQ 15901) = DIST(i, "15901");
```

```
BDIST(i,j) $ (BOILER(j,"BLOC") EQ 16330) = DIST(i,"16330");
 BDIST(i,j) $ (BOILER(j, "BLOC") EQ 15931) = DIST(i, "15931");
          = (10000 * ASHPER * ASHCST ) / ( 2000 * CWMHV ) ;
          = ( 2000 * (MFACT/100) * MINE(i) * CHHV * (1-CMOIST/100) ) / 1e6;
 FS(i)
 FS('GAS') = 1e9;
          = BOILER(j, "BSIZE") * (BOILER(j, "UTIL")/100) * 24*365.25;
 BQ(j)
         = PIFACT * BOILER(j,"TCR") * 1000;
 ATCR(j)
              = ASHBCST + FXUNLD +
 FUELFC(i,j)
                ( ATCR(j) + (1e6*BOILER(j,"TCR")*FXOMFACT/100) )/BQ(j);
 FUELFC('GAS', j) = BOILER(j, 'PGAS') ;
            = 1e6*(PCOAL/(2000*CHHV));
              = VARUNLD * BDIST(i,j);
 TCOST(i,j)
OPTION BQ:0:0:1;
OPTION FS:0:0:1 ;
OPTION ATCR:4:0:1;
DISPLAY PCOALM, FS, BOILER, BDIST, TCOST, BQ, ASHBCST, ATCR, FUELFC;
VARIABLES
                MCWM production cost at supply point i
 PMCWM(i)
                 fuel demanded of zero marginal cost coal
 QFUEL(i)
                 fuel costs less transport costs
 FUELCOST(i,j)
                 annual flow of fuel from supply point i to boiler j
 X(i,j)
                 total annual boiler costs
 Z
POSITIVE VARIABLES X, OFUEL, FUELCOST, PMCWM
 ;
= 0.0;
 PMCWM.L('GAS')
                   = 0.0;
 X.L(i,j)
 X.L('COAL8',j)
                   = BQ(j);
                  = BQ(\dot{1});
 X.L('GAS',j)
EQUATIONS
                 define objective function
  COST
                determine fuel demand for each supplier
  FUELSPLY(i)
  SUPPLY(i)
                 observe supply limits
                 satisfy boiler fuel demands
  DEMAND(j)
                total fuel preparation cost at each mine
  SPLYCST(i)
                fuel cost less transportation
  FUEL(i,j)
  FUELG(i,j)
                gas price
  COALFX
                 coal mine fixed constraint
```

```
Z = E = SUM((i,j), FUELCOST(i,j)*X(i,j) + TCOST(i,j)*X(i,j));
COST ..
                   QFUEL(i) =E=SUM(j, X(i,j));
FUELSPLY(i) ..
                   QFUEL(i) =L= FS(i);
SUPPLY(i) ..
                   SUM(i, X(i,j)) = E = BQ(j);
DEMAND(j) ..
SPLYCST(i) MINE(i) .. PMCWM(i) *( QFUEL(i)+1) **(0.969) ) -
                       0.6727*((QFUEL(i)+1)**(0.969)) = E= 211561;
FUEL(i,j) $MINE(i) .. FUELCOST(i,j) = E = PMCWM(i) + FUELFC(i,j);
                  FUELCOST('GAS',j) =E= FUELFC('GAS',j) ;
FUELG('GAS',j) ..
                   SUM( i, QFUEL(i)$MINE(i) ) - QFUEL('COAL8') =E= 0
COALFX ..
MODEL RETROFIT /ALL/;
OPTION NLP = MINOS5 ;
OPTION ITERLIM = 4000;
SOLVE RETROFIT USING NLP MINIMIZING Z ;
SOLVE RETROFIT USING NLP MINIMIZING Z ;
DISPLAY X.L, PMCWM.L, QFUEL
```

#### Appendix 4B

## **MCWM Supply Cost Model**

#### Introduction

This appendix describes basic economics for the supply of coal-based fuels for an industrial boiler that has been converted from firing fuel oil to firing a premium coal fuel. The boiler conversion technologies were studied by Penn State for DOE and DOD. The focus of Phase I activities were the development, design, and evaluation of two candidate technologies for boiler conversion. The boiler that was considered for conversion was a 25.2 MM Btu/h unit located at the Naval Surface Warfare Center at Crane, Indiana. The conversion technologies considered were to fire either, a micronized coal water mixture (MCWM) or a dry, micronized coal (DMC).

### **MCWM and DMC Conversion Technology Overview**

The MCWM and DMC technologies utilize the particular form of the feed coal to minimize solids handling problems and minimize boiler derating. Both technologies require premium quality coal fuels, one difference between the two being the physical form of the fuel as delivered to the boiler. DMC is delivered to the boiler as a chunk coal (nominal 2" x 0) and reduced to the necessary micron size at the boiler site. MCWM, on the other hand, is transported, stored, handled, and fired in the boiler in slurry form. Both technologies use coal with the same basic qualities as listed in Table 4B-1.

The first three coal characteristics were determined by Penn State as minimums acceptable for either technology. The coal higher heating value (HHV) is an estimate for a coal of this quality. The estimated HHV is probably on the conservative side considering other DOE researchers use a value closer to 15,000 Btu/lb coal.

Table 4B-1 MCWM and DMC Coal Quality Specifications

	10.00	
Ash Content	≤ 5	wt.% (dry basis, d.b.)
Sulfur Content	≤ 1	wt. % (d.b.)
Volatile Matter	> 30	wt. % (d.b.)
Higher Heating Value	≈ 14,000	Btu/lb coal (d.b.)

Sufficient reserves of acceptable coal sources have been identified by Penn State to exist in the immediate area of Crane (within a radius of 40 miles, or closer) for either technology.

#### **Crane Boiler Characteristics**

The Crane boiler that was evaluated for retrofit to fire coal is one of three, roughly equivalent, boilers located within the same boiler house. These boilers are presently used

for building heat, with occasional demands for process steam. The Phase I case study considered only six month operation of the retrofitted boiler corresponding to the heating season. The basic boiler retrofit requirements are listed in Table 4B-2.

Table 4B-2 Crane Boiler Specifications

Boiler Rated Capacity	25.2	MM Btu/h
Annual Hours of Operation	4,383	Hours
<b>Boiler Load During Operation</b>	100	%
Coal Requirement (Operating)	0.9	tons per hour (tph) coal (d.b.)
<b>Annual Coal Requirement</b>	3,945	tons per year (tpy) coal (d.b.)

The annual operating hours assumes that the retrofitted boiler is used during a typical six-month heating season at full rated capacity. Additional steam requirements for DOD users are met by adding boilers to the system. This arrangement of smaller, modular, boilers follows a normal DOD facilities planning philosophy that emphasizes maximization of system reliability under adverse conditions and standardized designs. Industrial- and commercial-scale boilers tend to be larger in order to minimize per unit cost of steam.

## MCWM Supply

The MCWM fuel form, as a slurry, has some potential advantages as compared to the DMC fuel. First, since the fuel is handled as a slurry it can be easily pumped into the system, stored, and sent to the burner for atomization into the boiler. Also, the slurried fines pose little problem in the generation of airborne dust (as long as splashing and spillage is avoided). Supply of the slurry may, potentially, come from a variety of relatively low cost sources as compared to other coal-forms. Since the slurry is delivered to the boiler at the proper size, the relatively capital and O&M cost intensive grinding mills for each boiler that is converted to fire the coal fuel are not necessary. Finally, cost advantages could be derived from the installation of a single slurry preparation system to supply several converted boilers.

One disadvantage of MCWM is that boiler derating tends to be more severe with slurry fuels, ceteris paribus, due to; 1) fuel atomization forming droplets consisting of several coal particles requiring longer residence times for burnout, 2) ash deposition and erosion on boiler tubes, and 3) heat losses (latent and sensible) associated with the higher moisture content of the fuel. Storage of the slurry can also be problematic due to a tendency of the solids in the slurry to settle and form a 'hard' or 'soft' pack. This settlement problem requires the development of specialized slurry preparation techniques and chemical additive packages. Minimizing boiler derating and improving the handleability and storage of the slurry were goals of the technology development effort by Penn State.

A basic difference governing the economics of fuel supply between MCWM and DMC technologies is that the form of the fuel delivered to the boiler is not readily

available from an existing market source. Coal is not generally produced for delivery to customers in slurry form. In fact, state-of-the-art production of a MCWM with the requisite handleability, storage, and atomizing qualities is limited in terms of total quantity produced annually and in the number of potential suppliers. In addition, there can be substantial variation in the quality of slurry produced by the different suppliers. For that reason, the MCWM retrofit option must consider the costs of production and delivery of slurry to the Crane boiler.

#### **MCWM Factored Cost Estimate**

A factored cost estimate for the production and transportation of MCWM to the Crane boiler was developed to aide in comparing this fuel to DMC. At the present time, no specific coal source has been identified. The production and transportation analysis presented here is loosely based on using AMAX Coal Company's Minnehaha operation (located about 40 miles from the Crane boiler) to site the MCWM preparation plant.

Creation of a market for MCWM potentially addresses a problem faced by nearly every coal preparation plant operation, namely the disposition of coal fines. Coal fines are difficult to clean and dry to a level of acceptable moisture content. Even when recovered and dried to acceptable levels, conventional handling methods tend to cause fines to become easily airborne, representing both a loss of product and the creation of a potential health hazard. Both the above problems can be addressed by producing and transporting the fines in a slurried fuel. Bearing this in mind, the feed to a MCWM production process can come from a variety of sources including; 1) existing coal impoundment, 2) existing operational coal preparation plant, and 3) conventionally produced chunk coal.

Considerable uncertainty surrounds the recovery of coal from existing coal impoundments due to the difficulties of locating appropriate impoundments, the adequate characterization of the distribution of coal (and potential contaminants), and the higher expected costs associated with reclamation/dredging of the coal. An impoundment must be able to provide an inexpensive product possessing the rather stringent quality specifications. Mixtures of the desired coal with other coals and contaminants in the impoundment complicates the beneficiation and slurry production process.

The surest method of providing the MCWM fuel is from coal obtained from the market in chunk form that already possesses the desired quality specifications. The size reduction and slurrying required can then be carried out in a straight-forward manner. The disadvantages of this method are the expected higher cost of coal, as compared to the alternatives, and the extra equipment and effort required to reduce the +2" x 0 coal the size required for MCWM.

A third option exists for producing MCWMs from slurry refuse streams in an existing coal preparation plant. Here, the characteristics of individual refuse streams in the conventional preparation plant can be utilized with little variation expected in the stream compositions over time (when cleaning the same coal). Since coal is recovered from process streams that would normally be discarded, the marginal cost of feed coal and refuse disposal for the slurry production plant would be zero. In fact, an economic benefit can be derived for reducing quantities of solids requiring disposal.

To date a particular site has not been selected, hence characterizing a preparation plant sufficiently to carry out a detailed design of the slurry preparation plant is not

possible. The MCWM production plant speculated here, however, makes use of this last scenario by providing what may be considered typical slurry preparation plant equipment. A MCWM production plant for the Crane boiler may be sized as described in Table 4B-3.

Table 4B-3 MCWM Production Plant Characteristics

MCWM Plant Production Rate	2	tph (d.b.)
Slurry Plant Annual Operating Hours	1,972	
Annual Production (Crane)	3,945	tons coal (d.b.)
Annual Maximum Rated Capacity	14,026	tons slurry

As can be seen from Table 4B-3, the slurry plant is oversized relative to the boiler requirement. The MCWM sizing reflects, 1) difficulties associated with the problems in differentiating between processes of a capacity in the range of one to three tph, 2) a built-in margin for both the large uncertainty in the capital equipment requirement, and 3) a production rate sufficient to provide for preparation plant down time while the boiler operates 24 hours per day, seven days a week. The MCWM production plant maximum annual capacity assumes a plant availability of 80 percent and the existence of a market for all of the production.

A simple factored capital cost estimate is provided in \$90.6/ton coal (d.b.) or \$3.23/MM Btu. This cost includes all capital, operation and maintenance charges.

Table 4B-4. The equipment list provides allowances for a single mill, conventional flotation cells, spirals (or the equivalent in other cleaning equipment), pumps, and a 25,000 gallon slurry storage tank sized for a three day supply of Crane, with an additional 10% allowance for miscellaneous equipment items. The electrical load of the equipment was estimated at 94 horsepower. The estimated equipment costs and electrical loads were generated after reviewing several sources and applying standard cost estimation methodologies to account for inflation, at 4%, and scale. The slurry plant described here purposely avoids the use of advanced fine coal cleaning methods reflecting an emphasis upon locating refuse streams that require minimum efforts to recover coal fines of the required quality.

The total capital requirement is estimated to be \$993 thousand dollars. As can be seen from the equipment list, by far the largest capital requirement is represented by the mill. This item also represents the greatest proportion of the estimated horsepower due to the demanding grinding regime expected. The equipment list, and associated costs, is considered speculative due to the incomplete knowledge regarding potential feed stream characteristics.

The plant cost factor used for determining the installed plant cost was generated using the Chilton method. The selection of this method was due to ease of use and consideration of the fact that the MCWM plant is an addition to an existing coal preparation facility. That advantage, along with the simple to implement approach, is somewhat offset by the relatively small size of the plant and the speculative nature of

estimate. The factor derived and presented above of 3.39 is less than the simpler Lang factor of 3.63 for solid-fluid plants.

Annualized capital and operation & maintenance (O&M) costs are presented in the Table 4B-5. The MCWM cost, f.o.b. slurry preparation plant, is estimated to be \$90.6/ton coal (d.b.) or \$3.23/MM Btu. This cost includes all capital, operation and maintenance charges.

Table 4B-4 MCWM Factored Capital Costs (\$K '93)

Mill	176
Flotation Cells	30
Spirals	14
Pumps	13
Tankage	33
Miscellaneous Items (@ 10%)	27
Equipment Cost (Delivered)	\$293
Cost Factor (Chilton Method)	3.39
Total Installed Plant Cost	\$993K

Table 4B-5 MCWM Annualized Capital and O&M Costs (\$ '93)

	Annual Cost	\$/ton Clean Coal (d.b.)	\$/MM Btu
FIVED OF M COSTS.			
FIXED O&M COSTS:			
O&M Labor	39,447	10.00	0.36
Maintenance Materials & Supplies	39,708	10.07	0.36
VARIABLE O&M COSTS:			
Feed Coal	-	-	-
Refuse Disposal	-	-	-
Grinding Media	1,341	0.34	0.01
Flotation Reagents Allowance	2,209	0.56	0.02
Additive Package	30,453	7.72	0.28
Electrical Power	5,509	1.40	0.05
Capital Charges:	238,606	60.49	2.16
TOTAL O&M AND CAPITAL CHARGES	357,273	90.57	3.23

O&M labor is assumed to be marginal to the existing coal preparation plant operation. An allowance of one person at \$20/h is provided. Maintenance materials and supplies are estimated at four percent of total plant cost. Both feed and refuse disposal costs are considered as marginal to the existing preparation plant operation and therefore equal to zero (no benefit assumed to be derived from avoided disposal to an impoundment pond). Consumption of grinding media is estimated to be 0.68 lb media per ton coal (d.b.) at \$0.50/lb. An allowance is made for flotation reagents at \$0.16/ton flocculant and 2 lb fuel oil per ton of coal at \$0.20/lb. Electrical power consumption for the state of Indiana is taken at 4 cents/KWh. Capital charges are calculated at a 15% cost of capital with a payback period of 7 years. At this level of the analysis, the use of government funds to build the MCWM plant (and a 4% discount rate) is not assumed in order to provide an additional margin, and to allow for sizing the plant for multiples of Crane (as discussed below).

The additive package costs primarily consists of a dispersant to avoid the formation of agglomerates that pose problems for storage and atomization of the slurry by the burner. The dispersant is estimated as 0.6 wt.% to coal at a cost of \$0.55/lb (active ingredient). A base is also used in conjunction with the dispersant in order to correct slurry pH. The costs for using the base are estimated as 0.4 wt.% to coal at a cost of \$0.14/lb. It is recognized that several additive packages exist which may provide acceptable results. Physical slurry preparation techniques may also substantially reduce the amount of dispersant required.

A sensitivity analysis of MCWM costs, f.o.b. slurry preparation plant, was conducted using a methodology similar to that accomplished for the Crane base case. It was shown that the \$/MM Btu cost of coal decreases substantially with an increasing number of oil-designed boilers converted over to fire MCWM. At a coal requirement equivalent to 10 boilers the size of Crane, the MCWM cost is \$1.03/MM Btu and drops to \$0.67/MM Btu at 50 Crane boiler equivalents. The analysis presented here does not imply that this many boiler conversions are undertaken. Indeed, only a few industrial or commercial-sized boilers would need to be converted to create an equivalent level of demand.

It should be noted that throughout the analysis of MCWM costs the capital charges are not amortized over a significant fraction of maximum rated slurry plant capacity. Since the demand is assumed to be only for a six month heating season, the slurry plant with all its capital equipment, sits idle for half of the year, regardless of the type of fuel supply. An interesting analysis might be to size the preparation plant for the anticipated annual demand and compare the benefit of a reduced plant capital cost to the added storage costs of slurry.

Another consideration of using MCWM as a boiler fuel is the relatively high costs of transport that range from 0.87 to 1.45 \$/MM Btu. A significant factor in the slurry transportation costs is the weight and bulk penalty of transporting up to 40 wt.% of water with coal. Any slurry fuel system that reduces weight being transported from the source to the point of use would reduce slurry transportation charges. Consideration might be given to transporting MCWM with the highest solids loading possible and then adding the necessary quantity of water at the boiler site. This fuel form also tends to higher charges due the necessity of using tanker versus dry bulk trucks. Extending the previous

concept, the MCWM might be transported in covered trucks as filter cake and then slurried at the boiler site.

## Appendix 4C

## **MCWM Retrofit Technology Cost Model**

Table 4C-1 MCWM Cost Estimate to Retrofit a 25.2 MM Btu/h Boiler

Ref.	Material	Installation
No Item Description	Cost	Hours
General Equipment	** * * * * * *	
116 FD FAN w/vfd	\$14,00	
117 Air Preheater 'steam'	\$4,71	
118 Air Heater (Q-Tube)	\$85,00	
119 Air Heater Sootblower	\$2,70	
120 Bag House	\$49,73	
121 ID Fan w/vfd	\$18,75	
122 Boiler Mods	\$0	0
123 Stack	\$45,00	
124 Floor Air Blast System	\$4,20	
125 Air Dryer	\$8,00	
126 Oil/Water Separator Equip	\$4,00	
127 Air Receiver Tanks	\$1,50	0 24
128 Pitot Grid-Comb. Air	\$3,00	0 16
129 Underground Building	\$20,00	0 1000
130 Compressor Building	\$4,00	0 160
131 Retaining Wall	\$4,50	0 430
132 Excavation	\$1,00	0 120
133 Concrete Slab	\$11,50	0 600
134 Air and FG Ductwork	\$28,50	0 560
135 A.H. Support Steel	\$4,50	0 40
136 Valves and Instrumentation	\$80,00	0 800
137 Controls	\$100,00	00
138 Electrical Work	\$70,00	0 1200
139 Run-Off Drain	\$400	24
140 Concrete Pipeway	\$650	
141 A.H. Sootblower Piping	\$2,20	0 220
Subtotal	·	
Ash Hara Para Faritana		
Ash Handling Equipment	<b>#7</b> 00	0 130
142 Pneumatic Conveying System	\$7,39	
143 Ash Silo	\$18,03	
144 Ash Silo Bin Vent Filter	\$3,50	
145 Rotary Valve	\$4,38	
146 Ash Unloading Screw Conveyor	\$16,61	4 120

Ref. No Item Description	Material I Cost	nstallation Hours
Slurry Feed Equipment	#4.000	2.4
147 MCWSF Transfer Pump (2)	\$4,000	24
148 MCWSF Storage Tank	\$52,000	120
149 MCWSF Mixer	\$34,000 \$4,500	32
150 Strainer (3 Sets) @ 1500 each	\$13,400	32
151 MCWSF Injection Pump (2) 152 MCWSF Heater	\$16,000	60
153 Flush Water Booster Pump	\$1,200	24
154 Waste Processing Tank	\$5,200	24
155 MCWSF Burner	\$66,000	80
156 Air Compressor	\$33,000	80
157 Slurry Building	\$7,500	400
158 Slurry & Flush Water Piping	\$26,000	600
159 Waste Processing Equipment	\$27,500	80
160 Power Station	\$21,500	64
	\$929,577	7970
Direct Construction Costs		
Total Materials	\$929,577	
Total Installation Hours Cost (@ \$40/hr)	\$318,800	
Construction Indirect Costs	¢ 47 020	
Field Supervision (15% of Labor hours)	\$47,820	
Construction Overhead and Fee (20%) Other Project Costs	\$249,675	
Frieght (6%)	\$55,775	
Taxes, Permits (7%)	\$65,070	
Subtotal Subcontractor and Equipment	\$1,666,717	,
Estimating Accuracy Allowance (10%)	\$166,672	
Total Subcontractor and Equipment	\$1,833,389	ì
Engineering (15% of project)	\$376,724	·
Project Management (4% of project)	\$100,460	
Construction Management (6% of project)	\$150,690	
Start up (2% of project)	\$50,230	
Subtotal Project	\$2,511,492	2
Contingencies (about 15%)	\$374,212	
Total Project Cost w/contingency	\$2,885,704	1

#### Appendix 4D

## **ELECTRIC POWER IN YOUR COMMUNITY**

In this survey we are interested in how you feel an electric power plant could affect you and your community. Because we are asking how you feel, there are no right or wrong answers. You do not need to know anything about electricity or how it is produced to answer the questions in this survey. Just answer the questions according to what you know, your own personal experiences, and attitudes. <u>Please answer every question</u>.

Throughout this survey, think of a <u>risk</u> as something that may or may not happen and an <u>impact</u> as the result that actually happens. An impact can be either good or bad.

Q1. Below is a list of technologies and types of facilities common in today's society. With a 1 meaning "not at all risky" and a 5 meaning "very risky," indicate how risky you feel each item is to you and your family.

(Circle appropriate number for each item.)

	NOT AT ALL RISKY		SOMEWHAT RISKY		VERY RISKY
PESTICIDES	1	2	3	4	5
X-RAYS	1	2	3	4	5
NUCLEAR POWER PLANT	1	2	3	4	5
ASBESTOS	1	2	3	4	5
TRAFFIC	1	2	3	4	5
QUARRY OR MINE	1	2	3	4	5
SEWAGE TREATMENT PLANT	1	2	3	4	5
NATURAL GAS-FIRED POWER PLANT	1	2	3	4	5
MANUFACTURING PLANT	1	2	3	4	5
LANDFILL	1	2	3	4	5
COAL-FIRED POWER PLANT	1	2	3	4	5
GROUNDWATER CONTAMINATION	1	2	3	4	5

Many human activities, including the production of electricity, have both good and bad effects on your life and on the community in which you live. We want to learn how individuals like you feel about power plants that burn either coal or natural gas to produce electricity and how you feel electricity production could affect the quality of your life.

Are you aware of any facilities near your home or in your community that produce electricity?

(Circle	appropriate number.)
1. NO 2. YES ( <b>GO</b> 3. NOT SUR	
	Q2A. Approximately how far away from your home is the nearest power plant?
	MILE(S)

Q3.	Do you know what fue	I is burned to produce the electricity that supplies your community with its
	electricity needs?	(Circle appropriate number.)

1. NO

Q2.

- 2. YES PLEASE SPECIFY: \_\_\_\_\_
- 3. NOT SURE

Q4. Do you feel that the amount of electricity that your household consumes is less than, about equal to, or greater than the amount of electricity consumed by other households in your community? (Circle appropriate number.)

- 1. LESS THAN AVERAGE
- 2. ABOUT EQUAL TO THE AVERAGE
- 3. GREATER THAN AVERAGE

Q5.	What is the average amount that you pay for your electricity each month?
	If you are not the person in your household who pays the electricity bill, please indicate about how
	much you think your electricity bill is each month.
	(Write in dollar amount.)

\$	

## A Coal-Fired Power Plant in Your Community

As the population in the United States grows, more electricity will be needed for the extra homes, businesses, and industries. We are interested in how you feel you will be affected if a coal-burning power plant were to be built and operate near your home. We would like you to consider a <u>hypothetical</u> situation in which a coal-burning power plant has been proposed for your community.

In the following pages, you will be asked how you feel the proposed coal-fired power plant will create risks to your health, the environment, and the aesthetic quality of your community. In addition, we will ask how you feel the proposed power plant could affect your community's economy.

## 4.1 CONSIDER THE FOLLOWING PROPOSAL:

YOU AND YOUR COMMUNITY	<ul> <li>You have lived in your community for 5 years and plan to live there permanently.</li> <li>You rely on electricity for all of the heating, lighting, and cooking in your home. In other words, your household does not have a woodstove, an oil furnace, or a hook-up to</li> </ul>
NEED FOR ELECTRICITY	<ul> <li>Because of the growth in the area in which you live, the public utility that supplies your community with its electricity has announced that the proposed power plant is greatly needed.</li> <li>The price you pay for your electricity will remain the same</li> </ul>
GENERAL FEATURES OF THE POWER PLANT	<ul> <li>The coal power plant will produce 180 megawatts of electricity per year. This will be enough power to supply the growth in your area for the next 30 years.</li> <li>The power plant will be built on a 40-acre plot of land near a local river.</li> <li>The site for the proposed coal-fired power plant is 3 miles away from your home.</li> <li>The life span of the power plant is projected to be at least 30 years.</li> </ul>
REGULATORY COMPLIANCE	All local, state, and federal regulations will be obeyed during the construction and operation of the plant.

ANSWER THE FOLLOWING QUESTIONS AS IF YOU WERE TRULY FACING THIS SITUATION.

#### The Coal-Fired Power Plant and Your Health

Human health impacts are due to changes in the air you breath and the water you drink. To answer the following questions, consider how you feel the proposed coal-fired power plant could affect your health and the health of others that live in your community. Please think <u>only</u> of the potential health impacts as you answer the questions on this page.

- Q6. Do you feel that there might be health impacts as a result of the coal-fired power plant described on page 4D-3? (Circle appropriate number.)
  - 1. NO
  - 2. YES
- Q7. Indicate below how positive or negative you feel that the impact(s) to your health could be from the proposed coal-fired power plant.

  (Circle appropriate number.)

	ERY NEGATIVE IMPACT			NO IMPAC	Γ		VERY POSITIVI IMPACT			
-4	-3	-2	-1	0	1	2	3	4		

Q8. How serious do you feel the risks to your health could be from the proposed coal-fired power plant? (Circle appropriate number.)

NOT AT ALL SERIOUS		9	SOMEWHA SERIOUS		VERY SERIOUS	
1	1 2 3		4	5	6	7

Q9. What do you feel is the chance or likelihood that the coal plant will affect your health some time in the future? (Circle percentage.)

NO CHANG	CE		MAY OR						DEFINITELY		
HEALTH WIL	L BE		MAY NOT AFFECT						WILL AFFECT		
AFFECTED	)		HEALTH							HEALTH	
0%	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%	

Q10. How would you describe your feelings when you think about the health risks from the proposed power plant? (Circle appropriate number.)

I FEEL AFRAID			MY FEELINGS ARE				I FEEL HAPPINESS			
AND DREADFUL			NEUTRAL				AND COMFORT			
-4	-3	-2	-1	0	1	2	3	4		

#### The Coal-Fired Power Plant and Your Local Economy

Economic impacts may be caused by changes in the local employment level, tax revenues and tax payments, property values, prices, and overall changes in the business activity in your community. To answer the following questions, consider how you feel the proposed coal-fired power plant could affect your local economy. Please think <u>only</u> of the potential impacts on your community's economy as you answer the questions on this page.

- Q11. Do you feel that there might be economic impacts as a result of the coal-fired power plant described on page 4D-3? (Circle appropriate number.)
  - 1. NO
  - 2. YES
- Q12. Indicate below how positive or negative you feel the impact(s) on your local economy could be from the proposed coal-fired power plant.

  (Circle appropriate number.)

VERY NEGATIVE IMPACT				NO IMPAC	Т		VERY POSITI IMPACT		
-4	-3	-2	-1	0	1	2	3	4	

Q13. How significant do you feel the impacts on your local economy could be from the proposed coal-fired power plant? (Circle appropriate number.)

NOT AT ALL			SOMEWHA	VERY		
SIGNIFICANT			SIGNIFICA	SIGNIFICANT		
1	2	3	4	5	6	7

Q14. What do you feel is the chance or likelihood that the coal plant will affect your local economy some time in the future? (Circle percentage.)

NO CHAN ECONOMY V AFFECTEL	VILL BE			MA	MAY OR Y NOT AF CONOM		DEFINITI WILL AFFI ECONC			
0%	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%

Q15. How would you describe your feelings when you think about the economic impacts associated with the proposed coal plant?

(Circle appropriate number.)

I FEEL AFRAID			MY	MY FEELINGS ARE			I FEEL HAPPINE			
AND DREADFUL				NEUTRAL			AND COMFOR			
-4 -3		-2	-1	0	1	2	3	4		

#### The Coal-Fired Power Plant and Your Environment

Environmental impacts could be caused by changes in the air quality, water quality, plants and wildlife, and how the land in your community is used. To answer the following questions, consider how you feel the proposed power plant may be a risk to the environment, and how serious you feel the actual environmental impact(s) could be from the coal-fired power plant. Please think <u>only</u> of the potential impacts on environmental quality as you answer the questions on this page.

- Q16. Do you feel that there might be environmental impacts as a result of the coal-fired power plant described on page 4D-3? (Circle appropriate number.)
  - 1. NO
  - 2. YES
- Q17. Indicate below how positive or negative you feel that the impact(s) to the environment could be from the proposed coal-fired power plant.

  (Circle appropriate number.)

	VERY NEGATIVE IMPACT			NO IMPAC	Г		VEI	RY POSITI IMPACT	. –
-4	-3	-2	-1	0	1	2	3	4	

Q18. How serious do you feel the risks to the environment could be from the proposed coal-fired power plant? (Circle appropriate number.)

NOT AT ALL SERIOUS		9	SOMEWHA SERIOUS	VERY SERIOUS		
1 2		3	4	5	6	7

Q19. What do you feel is the chance or likelihood that the coal plant will affect the environment some time in the future? (Circle percentage.)

NO CHANG ENVIRONME BE AFFECT	NT WILL							DEFINITELY W WILL AFFECT ENVIRONME		
0%	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%

**Q20.** How would you describe your feelings when you think about the environmental risks from the proposed power plant? (Circle appropriate number.)

I FEEL AFRAID			MY FEELINGS ARE				I FEEL HAPPINESS			
AND DREADFUL			NEUTRAL				AND COMFORT			
-4	-3	-2	-1	Ω	1	2	3	4		

#### The Coal-Fired Power Plant and Aesthetic Quality

The aesthetic quality of your community is how pleasant your community is to live in. Many people think of the noise, sights, and smells around their community when they think of its aesthetic quality. To answer the following questions, consider how you feel the proposed coal-fired power plant could be a risk to the aesthetic quality of your community. Please think <u>only</u> of the potential impacts on the aesthetic quality as you answer the questions on this page.

- Q21. Do you feel that there might be aesthetic impacts as a result of the coal-fired power plant described on page 4D-3? (Circle appropriate number.)
  - 1. NO
  - 2. YES
- Q22. Indicate below how positive or negative you feel that the impact(s) on the aesthetic quality of your community could be from the proposed coal-fired power plant. (Circle appropriate number.)

VERY NEG			NO IMPACT				VERY POSITIVE IMPACT		
-4	-3	-2	-1	0	1	2	3	4	

Q23. How serious do you feel the aesthetic risks could be from the proposed coal-fired power plant? (Circle appropriate number.)

NOT AT ALL SERIOUS		SOMEWHAT SERIOUS				VERY SERIOUS
1	2	3	4	5	6	7

**Q24.** What do you feel is the chance or likelihood that the coal plant will affect your community's aesthetic quality some time in the future? (Circle percentage.)

NO CHAN	CE			N	AAY OR M	1AY			Ε	EFINITELY
AESTHETIC QU	JALITY			N	OT AFFE	CT			WI	LL AFFECT
WLL BE AFFI	ECTED			AEST	HETIC QU	JALITY		A	ESTHETIC PROPERTY.	CQUALITY
0%	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%

Q25. How would you describe your feelings when you think about the aesthetic risks from the proposed power plant? (Circle appropriate number.)

I FEEL AFRA AND DREAD		MY FEELINGS ARE NEUTRAL					I FEEL HAPPINESS AND COMFORT		
-4	-3	-2	-1	0	1	2	3	4	

Consider the "overall con	ncern" you have about	the proposed coal-but	rning power plant.	We are interested
in how much of your con	cern is due to each of the	ne four types of impac	ts covered in the la	st four pages.

Q26.	In the spaces below, write in the percentage of the overall concern that you have for each type of
	potential impact from the proposed coal power plant. Please make sure your answers add up to
	100%.

POTENTIAL HEALTH IMPACTS	
POTENTIAL ENVIRONMENTAL IMPACTS	
POTENTIAL ECONOMIC IMPACTS	
POTENTIAL AESTHETIC IMPACTS	%
OTHER POTENTIAL IMPACTS (PLEASE DESCRIBE:	%
)	TOTAL = 100%

Consider how you feel the proposed coal-burning power plant will affect your health, your local economy, the environment and the aesthetic quality of your community.

- **Q27.** Would you vote in favor of or against the coal-burning power plant proposed for your community?
  - 1. I WOULD VOTE IN FAVOR OF THE COAL POWER PLANT
  - 2. I WOULD VOTE AGAINST THE COAL POWER PLANT
  - 3. DON'T KNOW

Suppose that your electricity supplier proposed to build the coal-fired power plant described on **page 4D-3**. We would like you to imagine that you live in the community in which the coal power plant is being proposed. If the supplier is not able to build this power plant, it will have to increase the price you pay for electricity because the much needed electricity must be purchased at a higher cost from other power producers elsewhere in the state.

Think of how much more money you would be willing to pay on your monthly electricity bill in order to prevent the coal-burning power plant from being built in your community. When answering the following question, please consider your household income, your average monthly electricity bill, and how much extra you can actually afford to pay to prevent the coal-fired power plant.

**Q28.** Circle the dollar value closest to the largest amount you would be willing to pay <u>extra</u> each month on your electricity bill to prevent the coal-fired power plant from being built in your community.

\$0.00	\$0.10	\$0.25	\$0.50	\$0.75	\$1.00
\$1.25	\$1.50	\$2.00	\$3.00	\$4.00	\$5.00
\$6.00	\$8.00	\$11.00	\$14.00	\$19.00	\$22.00
\$26.00	\$30.00	\$35.00	\$40.00	\$45.00	\$50.00
\$55.00	\$60.00	\$70.00	\$80.00	\$90.00	\$100.00
\$110.00	\$120.00	\$140.00	\$160.00	\$220.00	\$300.00
	_				

OTHER: \$\_\_\_\_\_

If You Answered \$0.00 in Question 28, Go To Page 4D-11.

being built in your

	If You Answered \$0.00 in Question 28, Go To Page 41	D-11. →
Q29.	Think of the amount you would pay to prevent the coal-burning community (Q28.) About what percent of that amount would be (Write in percentage.)	
	THAT MY HOUSEHOLD WILL NOT BE AFFECTED AT ALL BY THE POTENTIAL IMPACTS FROM THE COAL -FIRED POWER PLANT.	%
	THAT OTHER HOUSEHOLDS WILL NOT BE AFFECTED AT ALL BY THE POTENTIAL IMPACTS FROM THE COAL-FIRED POWER PLANT.	%
	THAT FUTURE GENERATIONS WILL NOT BE AFFECTED AT ALL BY THE POTENTIAL IMPACTS FROM THE COAL-FIRED POWER PLANT.	%
	THAT COAL-FIRED POWER PLANTS SHOULD BE PREVENTED EVEN IF NO ONE WILL HAVE TO LIVE NEAR THEM.	%
	REASONS OTHER THAN THESE (PLEASE DESCRIBE:)	%
PLEA	ASE MAKE SURE YOUR ANSWERS ADD UP TO 100%.	TOTAL = 100%

## A Natural Gas-Fired Power Plant in Your Community

As the population in the United States grows, more electricity will be needed for the extra homes, businesses, and industries. We are interested in how you feel you will be affected if a natural gas-burning power plant were to be built and operate near your home. We would like you to consider a <u>hypothetical</u> situation in which a natural gas-burning power plant has been proposed for your community.

In the following pages, you will be asked how you feel the proposed natural gas-fired power plant will create risks to your health, the environment, and the aesthetic quality of your community. In addition, we will ask how you feel the proposed power plant could affect your community's economy.

## CONSIDER THE FOLLOWING PROPOSAL:

YOU AND YOUR COMMUNITY	<ul> <li>You have lived in your community for 5 years and plan to live there permanently.</li> <li>You rely on electricity for all of the heating, lighting, and cooking in your home. In other words, your household does not have a woodstove, an oil furnace, or a hook-up to a natural gas pipeline.</li> </ul>
NEED FOR ELECTRICITY	<ul> <li>Because of the growth in the area in which you live, the public utility that supplies your community with its electricity has announced that the proposed power plant is greatly needed.</li> <li>The price you pay for your electricity will remain the same after the new natural gas power plant is in operation.</li> </ul>
GENERAL FEATURES OF THE POWER PLANT	<ul> <li>The natural gas power plant will produce 180 megawatts of electricity per year. This will be enough power to supply the growth in your area for the next 30 years.</li> <li>The power plant will be built on a 40-acre plot of land near a local river.</li> <li>The site for the proposed natural gas-fired power plant is 3 miles away from your home.</li> <li>The life span of the plant is projected to be at least 30 years.</li> </ul>
REGULATORY COMPLIANCE	All local, state, and federal regulations will be obeyed during the construction and operation of the plant.

ANSWER THE FOLLOWING QUESTIONS
AS IF YOU WERE TRULY FACING THIS SITUATION.

#### The Natural Gas-Fired Power Plant and Your Health

Human health impacts are due to changes in the air you breath and the water you drink. To answer the following questions, consider how you feel the proposed natural gas-fired power plant could have an affect on your health and the health of others that live in your community. Please think <u>only</u> of the potential health impacts as you answer the questions on this page.

- Q30. Do you feel that there might be health impacts as a result of the natural gas -fired power plant described on page 4D-11? (Circle appropriate number.)
  - 1. NO
  - 2. YES
- Q31. Indicate below how positive or negative you feel that the impact(s) to your health could be from the proposed natural gas-fired power plant.

  (Circle appropriate number.)

VERY NEG			NO IMPAC	Γ		VEF	RY POSITIVI IMPACT	3	
-4	-3	-2	-1	0	1	2	3	4	

Q32. How serious do you feel the risks to your health could be from the proposed natural gas-fired power plant? (Circle appropriate number.)

NOT AT ALL SERIOUS		9	SOMEWHA SERIOUS			VERY SERIOUS
1	2	3	4	5	6	7

Q33. What do you feel is the chance or likelihood that the natural gas plant will affect your health some time in the future? (Circle percentage.)

NO CHANG HEALTH WIL AFFECTED	LL BE			MAY OR MAY NOT AFFECT HEALTH					_	DEFINITELY LL AFFECT HEALTH
0%	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%

Q34. How would you describe your feelings when you think about the health risks from the proposed power plant? (Circle appropriate number.)

I FEEL AFRAID AND DREADFUL				EELING: NEUTRA	-		I FEEL HAPP AND COMFO			
-4	-3	-2	-1	0	1	2	3	4		

## The Natural Gas-Fired Power Plant and Your Local Economy

Economic impacts may be caused by changes in the local employment level, tax revenues and tax payments, property values, prices, and overall changes in the business activity in your community. To answer the following questions, consider how you feel the proposed natural gas-fired power plant could affect your local economy. Please think <u>only</u> of the potential impacts on your community's economy as you answer the questions on this page.

- Q35. Do you feel that there might be economic impacts as a result of the natural gas -fired power plant described on page 4D-11? (Circle appropriate number.)
  - 1. NO
  - 2. YES
- Q36. Indicate below how positive or negative you feel the impact(s) on your local economy could be from the proposed natural gas-fired power plant.

  (Circle appropriate number.)

VERY NEG IMPAC			NO IMPAC		VEI	VERY POSITIVE IMPACT			
-4	-3	-2	-1	0	1	2	3	4	

Q37. How significant do you feel the impacts on your local economy could be from the proposed natural gas-fired power plant? (Circle appropriate number.)

NOT AT AI SIGNIFICAN			SOMEWH. SIGNIFICA	VERY SIGNIFICANT		
1	2	3	4	5	6	7

Q38. What do you feel is the chance or likelihood that the natural gas plant will affect your local economy some time in the future? (Circle percentage.)

NO CHANCE MAY OR ECONOMY WILL BE MAY NOT AFFECT AFFECTED ECONOMY									WI	DEFINITELY LL AFFECT ECONOMY
0%	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%

Q39. How would you describe your feelings when you think about the economic impacts associated with the proposed natural gas plant?

(Circle appropriate number.)

I FEEL AFRAII AND DREADI			EELINGS NEUTRA	I FEEL HAPPINESS AND COMFORT					
-4	-3	-2	-1	0	1	2	3	4	

#### The Natural Gas-Fired Power Plant and Your Environment

Environmental impacts could be caused by changes in the air quality, water quality, plants and wildlife, and how the land in your community is used. To answer the following questions, consider how you feel the proposed power plant may be a risk to the environment, and how serious you feel the actual environmental impact(s) could be from the natural gas-fired power plant. Please think <u>only</u> of the potential impacts on environmental quality as you answer the questions on this page.

- Q40. Do you feel that there might be environmental impacts as a result of the natural gas -fired power plant described on page 4D-11? (Circle appropriate number.)
  - 1. NO
  - 2. YES
- Q41. Indicate below how positive or negative you feel that the impact(s) to the environment could be from the proposed natural gas-fired power plant.

  (Circle appropriate number.)

VERY NEG			NO IMPAC	Γ		VERY POSITIVE IMPACT				
-4	-3	-2	-1	0	1	2	3	4		

Q42. How serious do you feel the risks to the environment could be from the proposed natural gas-fired power plant? (Circle appropriate number.)

NOT AT ALL SERIOUS		S	SOMEWHA SERIOUS	VERY SERIOUS		
1	2	3	4	5	6	7

Q43. What do you feel is the chance or likelihood that the natural gas plant will affect the environment some time in the future? (Circle percentage.)

NO CHANC ENVIRONMEN BE AFFECTI	MAY NOT AFFECT						WILL A	TELY WILL FFECT THE RONMENT		
0%	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%

Q44. How would you describe your feelings when you think about the environmental risks from the proposed power plant? (Circle appropriate number.)

I FEEL AFRAID AND DREADFUL				EELING: NEUTRA			I FEEL HAPPINES AND COMFORT				
-4	-3	-2	-1	0	1	2	3	4			

#### The Natural Gas-Fired Power Plant and Aesthetic Quality

The aesthetic quality of your community is how pleasant your community is to live in. Many people think of the noise, sights, and smells around their community when they think of its aesthetic quality. To answer the following questions, consider how you feel the proposed natural gas-fired power plant could be a risk to the aesthetic quality of your community. Please think <u>only</u> of the potential impacts on the aesthetic quality as you answer the questions on this page.

Q45.	Do you feel that there might be a	esthetic impacts as a result of the natural gas -fired power plant
	described on page 4D-11?	(Circle appropriate number.)

- 1. NO
- 2. YES

Q46. Indicate below how positive or negative you feel that the impact(s) on the aesthetic quality of your community could be from the proposed natural gas-fired power plant. (Circle appropriate number.)

VERY NEGATIVE IMPACT				NO IMPAC	CT		VEI	YERY POSITIVE IMPACT	
-4	-3	-2	-1	0	1	2	3	4	

Q47. How serious do you feel the aesthetic risks could be from the proposed natural gas-fired power plant? (Circle appropriate number.)

NOT AT ALL		S	SOMEWHAT			VERY	
SERIOUS			SERIOUS			SERIOUS	
1	2	3	4	5	6	7	

Q48. What do you feel is the chance or likelihood that the natural gas plant will affect your community's aesthetic quality some time in the future? (Circle percentage.)

NO CHANCE AESTHETIC QUALITY WLL BE AFFECTED				N	AY OR MA OT AFFE HETIC QU	CT		DEFINITELY WILL AFFECT AESTHETIC QUALITY		
0%	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%

Q49. How would you describe your feelings when you think about the aesthetic risks from the proposed power plant? (Circle appropriate number.)

I FEEL AFRAID AND DREADFUL				EELINGS NEUTRA			I FEEL HAPPINESS AND COMFORT		
-4	-3	-2	-1	0	1	2	3	4	

Consider the "overall concern" you have about the proposed natural gas-burning power plant. W	e are
interested in how much of your concern is due to each of the four types of impacts covered in the las	t four
pages.	

Q50.	In the spaces below,	write in the per	rcentage of th	ne overall c	concern tha	at you have	for each	type of
	potential impact from							
	up to 100%.							

POTENTIAL HEALTH IMPACTS	
POTENTIAL ENVIRONMENTAL IMPACTS	%
POTENTIAL ECONOMIC IMPACTS	%
POTENTIAL AESTHETIC IMPACTS	%
OTHER POTENTIAL IMPACTS (PLEASE DESCRIBE:	%
)	TOTAL = 100%

Consider how you feel the proposed natural gas-burning power plant will affect your health, your local economy, the environment and the aesthetic quality of your community.

- Q51. Would you vote in favor of or against the natural gas-burning power plant proposed for your community?
  - 1. I WOULD VOTE IN FAVOR OF THE NATURAL GAS POWER PLANT
  - 2. I WOULD VOTE AGAINST THE NATURAL GAS POWER PLANT
  - 3. DON'T KNOW
  - 4. I WOULDN'T VOTE PLEASE EXPLAIN:

Suppose that your electricity supplier proposed to build the natural gas-fired power plant described on **page 4D-11**. We would like you to imagine that you live in the community in which the natural gas power plant is being proposed. If the supplier is not able to build this power plant, it will have to increase the price you pay for electricity because the much needed electricity must be purchased at a higher cost from other power producers elsewhere in the state.

Think of how much more money you would be willing to pay on your monthly electricity bill in order to prevent the natural gas-burning power plant from being built in your community. When answering the following question, please consider your household income, your average monthly electricity bill, and how much extra you can actually afford to pay to prevent the natural gas-fired power plant.

Q52. Circle the dollar value closest to the largest amount you would be willing to pay <u>extra</u> each month on your electricity bill to prevent the natural gas-fired power plant from being built in your community.

\$0.00	\$0.10	\$0.25	\$0.50	\$0.75	\$1.00
\$1.25	\$1.50	\$2.00	\$3.00	\$4.00	\$5.00
\$6.00	\$8.00	\$11.00	\$14.00	\$19.00	\$22.00
\$26.00	\$30.00	\$35.00	\$40.00	\$45.00	\$50.00
\$55.00	\$60.00	\$70.00	\$80.00	\$90.00	\$100.00
\$110.00	\$120.00	\$140.00	\$160.00	\$220.00	\$300.00

OTHER: \$\_\_\_\_\_

If You Answered \$0.00 in Question 52, Go To Page 19.

Q53.	Think of the amount you would pay to prevent the natural gain your community (Q52.) About what percent of that amount sure your answers add up to 100%. (Write in percentage.)	as-burning power plant from being built nt would be to ensure Please make
	THAT MY HOUSEHOLD WILL NOT BE AFFECTED AT ALL BY THE POTENTIAL IMPACTS FROM THE NATURAL GAS-FIRED POWER PLANT.	%
	THAT OTHER HOUSEHOLDS WILL NOT BE AFFECTED AT ALL BY THE POTENTIAL IMPACTS FROM THE NATURAL GAS-FIRED POWER PLANT.	%
	THAT FUTURE GENERATIONS WILL NOT BE AFFECTED AT ALL BY THE POTENTIAL IMPACTS FROM THE NATURAL GAS-FIRED POWER PLANT.	%
	THAT NATURAL GAS-FIRED POWER PLANTS SHOULD BE PREVENTED EVEN IF NO ONE WILL HAVE TO LIVE NEAR THEM.	%
	REASONS OTHER THAN THESE (PLEASE DESCRIBE:)	%
		TOTAL = 100%

If You Answered \$0.00 in Question 52, Go To Page 19.

# Your Preferences for the Use of Either Coal or Natural Gas in the Proposed Power Plant

Suppose that your electricity supplier has already received local, state, and federal approval to build a power plant for your community. Assume that a power plant will be built in your community, but the type of fuel that it will burn has not yet been determined.

- Q54. Based upon your current knowledge, feelings, and opinions, what type of fuel would you prefer that the plant burn to produce electricity coal or natural gas?
  - 1. COAL
  - 2. NATURAL GAS

OTHER: \$\_\_\_\_\_

Think of how much more money you would be willing to pay on your monthly electricity bill to make sure that the power plant uses the fuel type that you circled above in **Q54**. When answering the following question, please consider your household income, your average monthly electricity bill, and how much extra you can actually afford to pay so the plant burns the fuel that you prefer.

Q55. How much would you be willing to pay each month, in addition to your current electricity bill, to ensure that the plant burns the fuel that you prefer (Q54.)?

Circle the dollar amount closest to the amount you would be willing to pay extra each month.

\$0.00	\$0.10	\$0.25	\$0.50	\$0.75	\$1.00
\$1.25	\$1.50	\$2.00	\$3.00	\$4.00	\$5.00
\$6.00	\$8.00	\$11.00	\$14.00	\$19.00	\$22.00
\$26.00	\$30.00	\$35.00	\$40.00	\$45.00	\$50.00
\$55.00	\$60.00	\$70.00	\$80.00	\$90.00	\$100.00
\$110.00	\$120.00	\$140.00	\$160.00	\$220.00	\$300.00

## ABOUT YOU AND YOUR HOUSEHOLD

# PLEASE REMEMBER THAT ALL INFORMATION IS ENTIRELY CONFIDENTIAL

	I. FEMALE	-						
_	2. MALE	i.						
<b>H2</b> . Y	Your age:							
-		YEARS						
<b>H3.</b> I write "0"		ourself, how	many men	nbers in you	r household	d are in each	age group?	(If none,
- - -	18-35-0			Œ				
	How would (Circle one	•	oe your raci	al or ethnic l	oackground	i?		
3	<ol> <li>BLA</li> <li>HIS</li> <li>ASI</li> <li>NA</li> </ol>	AN OR PACTIVE AME	RICAN AM MEXICAN CIFIC ISLA RICAN INI	AMERICA NDER				
	A high scho	years of ed ool education ber of year	on = 12 yea	re you comp ars.	leted?			
	6	7	8	9	10	11	12	
	13	14	15	16	17	18	19	
							25+	

**H6.** What is your present employment status? (Circle the best answer.)

LABORER
 TEACHER
 SELF-EMPLOYEE
 SELF-EMPLOYEED
 FULL TIME HOMEMAKER
 PROFESSIONAL
 RETIRED
 GOVERNMENT EMPLOYEE
 UNEMPLOYED
 SECRETARY/CLERICAL
 OTHER - PLEASE SPECIFY:

**H7.** What is your total annual household income before taxes and other deductions? (Circle best answer.)

1.	UNDER \$9,999	9.	\$80,000 - 89,999
2.	\$10,000 - 19,999	10.	\$90,000 - 99,999
3.	\$20,000 - 29,999	11.	\$100,000 - 119,999
4.	\$30,000 - 39,999	12.	\$120,000 - 139,999
5.	\$40,000 - 49,999	13.	\$140,000 - 159,999
6.	\$50,000 - 59,999	14.	\$160,000 - 179,000
7.	\$60,000 - 69,999	15.	\$180,000 - 199,999
8.	\$70,000 - 79,999	16.	\$200,000 AND OVER

**H8**. How active have you been active in community related issues during the past two (Circle appropriate number.)

years?

NOT AT ALL ACTIVE		SOMEWHAT ACTIVE		VERY ACTIVE
1	2	3	4	5

Appendix 4E

## **Sector Definition**

Sector	Name	BEA Code
1	Agriculture	1-4
2	Iron Mining	5
3	Non-Iron Mining	6
4	Other Mining	9,10
5	Coal Mining	7
6	Petroleum Mining	8
7	Construction	11,12
8	Manufacturing	13-30,33,34,39-64
9	Petroleum Refining	41
10	Plastics	32
11	Glass	35
12	Stone	36
13	Steel	37
14	Metal Manufacturing	38
15	Transportation	65
16	Communication	66,67
17	Electric Utilities	68.01
18	Gas Utilities	68.02
19	Trade & Finance	69,70
20	Services (including Water & Sanitary Services)	71-79,68.03

Notes: Sectors 5, 6, 9, 17, and 18 from the energy aggregate.