DEVELOPMENT OF FULLY INTEGRATED COAL LIQUEFACTION/CHARACTERIZATION TECHNIQUES

Huaying Huai¹, Henk L.C. Meuzelaar¹, Chung H. Tsai² and Joseph S. Shabtai²

²Department of Fuel Engineering
University of Utah, Salt Lake City, UT 84112

August 1991

INTRODUCTION

Over the past decade, sophisticated chromatographic and spectroscopic techniques have greatly increased our knowledge of the composition and structure of coal-derived liquids as well as of the corresponding feed coals [1]. Notwithstanding these advances, relatively little is known about the precise reaction pathways as well as the intermediate reaction products involved. In order to study these processes in greater detail, previous activities in our laboratory have focused on the development of advanced mass spectrometric techniques in which thermally driven coal conversion reactions are carried out directly within the vacuum environment of an MS ion source (e.g., vacuum TG/MS [2], Curie-point Py-MS [3]) or at near-ambient pressures with a capillary transfer line connection to a combined IR/MS system (e.g., TG/(GC)/IR/MS [4]) while maintaining sufficiently short sampling intervals to provide kinetic information. Although successful in modeling and even predicting [5], a range of different coal liquefaction, devolatilization and gasification reactions, an inherent shortcoming of this class of techniques is the inability to simulate catalytic coal conversion processes at high pressures. Consequently, we have undertaken the development of a direct MS interface for high pressure reaction products under real-time analysis conditions while minimally disturbing the reaction process.

Effectively, whereas our earlier work attempted to bring the reactor into the mass spectrometer, we are now making an effort to bring the mass spectrometer into the reactor.

Between providing us with the opportunity to study coal conversion processes under more realistic reaction conditions, the new approach also enables us to interface our spectrometric equipment to a broader range of existing reactor types and processing environments. In doing

so, we were fortunate enough to profit from several recent developments with regard to automated vapor sampling techniques for GC/MS [6] as well as with regard to mobile, ruggedized GC/MS instruments [7] suitable for use in a wide variety of demanding industrial process engineering environments.

EXPERIMENTAL

A high priority objective in our present work is development of on-line GC/MS monitoring techniques for batch or flow through type autoclave reactors. Due to the relatively long residence times primary reaction products formed in autoclaves are notoriously susceptible to secondary, or even tertiary reactions. Application of real-time, on-line chromatographic and/or spectroscopic techniques capable of throwing light on these processes is hampered by the high temperatures and pressures inside the reactor which complicate direct interfacing to standard analytical instruments.

Using a novel automated vapor sampling (AVS) technique developed at the University of Utah, Center for Micro Analysis and Reaction Chemistry (U.S. Patent No. 4,970,905), we constructed an on-line mass spectrometry interface for high pressure reactor environments (see Figure 1. The interface consists of a valveless, all quartz, heated inlet device suitable for automated, repetitive vapor sampling. The AVS module connects directly to a 1 m long, 150 um i.d., fused silica capillary GC column, thereby providing a highly useful degree of chromatographic preseparation. The effluent from the capillary column is fed directly into the ion source of a highly sensitive ion trap mass spectrometer (ITMS) capable of operating in GCMS as well as tandem MS (MSⁿ) mode while providing electron ionization (EI) as well as chemical ionization (CI) options.

Since the AVS inlet is designed to operate at near-ambient pressures in order to ensure a constant, stable flow of carrier gas through the capillary transfer line column into the high vacuum of the MS system, the high pressures in the autoclave reactor need to be first reduced to near-ambient pressure by means of a 1 m length of narrow bore (e.g. 10 um) fused silica capillary tubing. This tubing is kept at relatively high temperatures (< 300 C) to minimize condensation losses. Moreover, utmost care is taken to eliminate dead spaces at the high pressure end of the transfer line in order to avoid unduly long response times due to the very low liquid flows (e.g.~ 0.1 µl/min) in the narrow bore capillary tube.

Figure 1 shows a schematic picture of the on-line system, whereas Tables 1 and 2 list the experimental conditions for a series of on-line GC/MS studies with model compounds, aimed at establishing the feasibility of our instrumental approach. A second objective was to perform preliminary studies of low temperature hydrotreatment and hydrode(oxygen)(nitrogen)(sulfuriz)ation processes playing a key role in ongoing low temperature coal liquefaction studies under the University of Utah task within the Consortium for Fossil Fuel Liquefaction Science.

RESULTS AND DISCUSSION

Aside from ocassional plugging of the 10-15 µm i.d. capillary pressure reduction line and the protective 2 and 0.5 µm frits the system performed reliably. The cause of the plugging appears to be traceable to particles released by the catalyst. Obviously, more sophisticated particulate matter removal strategies are needed before on-line analysis of conversion processes in coal solids can be attempted. Consequently, current experimental

protocols call for the analysis of carefully filtered liquid samples ranging from model compounds to actual coal derived liquids and/or subfractions.

Apart from these limitations, system performance exceeded design specifications with regard to GC/MS performance, especially isothermal GC resolution (note the separation of decalin isomer peaks in Figure 2) and dynamic range (solvent peaks representing >80% of the reactor contents were as readily measurable as small product peaks representing less than 100 ppm concentrations thus establishing an effective dynamic range $\geq 10^4$). As also demonstrated in previous work [8], the combination of automated, pulsed vapor sampling and short column capillary "transfer line" GC enabled repetitive recording of complete isothermal GC runs at 1-4 minute intervals. Moreover, the transfer time of nonretained sample components between reactor and detector was found to be less than 1 minute. In short, the system shown in Figure 1 is capable of detecting minute changes in sample composition in a time which is short compared to the typical reaction times in autoclave reactors.

Specific results of the three series of experiments shown in Figures 2-7 illustrate the ease with which kinetic profiles of reactor feed as well as reaction products can be obtained in a single experimental run. Using conventional off-line experiments, which usually require the experiment to be repeated numerous times while increasing temperature and/or residence time, it would have taken several weeks or months to obtain equally detailed kinetic profiles, as many among us know all too well from personal experience with autoclave type experiments. It should also be noted that the reduction in number of experiments carried out greatly lessens the demand for excessive quantities of expensive model compounds as well as the eventual disposal of hazardous experimental wastes. Finally, the ability to measure both

the feed components and the reaction products in a single experiment should be instrumental in helping to close mass balances as well as elucidate reation pathways. The mild hydrocracking (Figures 2 and 3), hydrodeoxygenation (Figures 4 and 5) and hydrodenitrogenation and -desulfurization (Figures 6 and 7) experiments provide readily interpretable information about the mechanisms and the kinetics of the primary conversion reactions under catalytically as well as thermally controlled reaction conditions.

CONCLUSIONS

- 1. Aside from occasional plugging of the capillary pressure reduction line, the system performed reliably and according to design specifications.
- 2. Valveless, pulsed sampling of reactor effluents onto short capillary GC columns provides complete GC/MS profiles at 1-4 min intervals. For nonretained sample components the tran fer time between reactor and detector is less than 1 minute.
- 3. A highly useful degree of chromatographic preseparation is achieved as evidenced by the separation of the two decalin (cis and trans) isomer peaks.
- 4. Use of stable solvents in a 9:1 solvent/feed ratio does not adversely affect the performance of the chromatographic system, even if the solvent peak clutes later than most of the reaction product peaks.
- Product concentrations of less than 100 ppm are readily monitored under the same GC/MS conditions as the solvent peak, thereby establishing an effective dynamic range ≥10⁴: 1.

- Effects of time, temperature and catalyst type on hydrocracking and hydrode(oxygen)(nitrogen)(sulfuriz)ation are readily measurable.
- 7. Kinetic profiles of feed as well as product concentrations can be obtained in a fraction of the time needed for conventional off-line measurements.

FUTURE PLANS

To obtain precise mass balance information we are planning to perform similar on-line GC/MS experiments on catalytic and thermal coal conversion reactions in a high pressure TG System. Also, this will further reduce the feed sample quantities needed per experiment, thereby permitting the use of rare and/or expensive model compounds. Since high pressure TG/MS experiments will need to be primarily carried out in solventless environments (e.g. under hydropyrolysis conditions) particulate matter related plugging problems (frits and transfer lines) should be eliminated.

Up till now only relatively simple model compound mixtures have been studied.

Nevertheless, the system is expected to perform quite well with more complex samples such as actual coal-derived liquids. In spite of the rather limited range of compounds which can be analyzed in a single isothermal GC run the formidable analytical capabilities of the ion trap mass spectrometer used in these experiments, which include tandem MS (MSⁿ), as well as various chemical ionizations options, compensate for the shortcomings of the GC system in many applications. Furthermore, we are currently equipping the transfer line GC module with rapid temperature program ning (up to 10 K/sec) capability. This should considerably extend

the range of compounds which can be analyzed in a single GC/MS run, albeit at the expense of longer repetitive intervals, due to the time needed to cool the transfer line between runs.

ACKNOWLEDGEMENTS

The advice and assistance of Neil Arnold, William McClennen, Jacek Dworzanski, Wally Maswadeh and George Chacko is gratefully acknowledged.

The research reported here is supported by the USDOE (grant #UKRF-4-2376-90-10) with matching support from the University of Utah and is carried out under the auspices of the Consortium for Fossil Fuel Liquefaction Science in collaboration with the University of Kentucky, the University of West Virginia, the University of Pittsburgh and Auburn University.

LITERATURE CITED

- 1. Meuzelaar, H.L.C. (ed.) Advances in Coal Spectroscopy, Plenum Publishers, New York, New York, 1990 (in press).
- 2. Yun, Y.; Menzelaar, H.L.C.; Chakravarty, T.; and Metcalf, G. "Computer-Enhanced Pyrolysis Mass Spectrometry: A New Window on Coal Structure and Reactivity," in: Advances in Coal Spectroscopy, 1990, 2 (in press).
- 3. Chakravarty, T.; Windig, W; Taghizadeh, K.; and Meuzelaar, H.L.C. "Computer-Assisted Interpretation of Pyrolysis Mass Spectra of Two Oil Shales and their Corresponding Kerogens," *Energy and Fuels*, 1988, 2, 191-196.
- 4. Dworzanski, J.P.; Buchanan, R.M., Chapman, J.N.; and Meuzelaar, H.L.C. "Characterization of Lignocellulosic Materials and Model Compounds by Combined TG/(GC)/FTIR/MS," ACS Preprints, Div. of Fuel Chemistry, 1991, 36(2), 725-732.
- 5. Chakravarty, T.; Khan, M.R.; and Meuzelaar, H.L.C. "Modeling and Predicting the Composition of Fossil Fuel Derived Pyrolysis Liquids Using Low-Voltage Mass

- Spectrometry and Canonical Correlation Analysis," *Industrial and Engineering Chemistry Research*, 29(11), 2173-2180.
- 6. Arnold, N.S.; McClennen, W.H.; and Meuzelaar, H.L.C. "A Vapor Sampling Device for Rapid Direct Short Column Gas Chromatography/Mass Spectrometry Analyses of Atmospheric Vapors," *Analytical Chemistry*, 1991, 63, 299-304.
- 7. Meuzelaar, H.L.C.; McClennen, W.H.; Arnold, N.S.; Reynolds, T.K.; Maswadeh, W.; Jones, P.R.; and Urban, D.T. "Development of MINITMASS, a Mobile Tandem Mass Spectrometer for Monitoring Vapors and Particulate Matter in Air," Ist International Symposium on Field Screening Methods for Hazardous Waste Site Investigations, Las Vegas, Nevada, October 11-13, 1988, 195-202.
- 8. McClennen, W.H.; Arnold, N.S.; Meuzelaar, H.L.C.; Ludwig, E.; and Lighty, J.S. "The Application of a Mobile Ion Trap Mass Spectrometer System to Environmental Screening and Monitoring," Ilnd International Symposium on Field Screening Methods for Hazardous Waste Site Investigation, Las Vegas, Nevada, February 12-14, 1991, 339-348.

	TABLE '					
Reaction Type	Feed	Solvent	Internal Standard	Products	Temp.	Catalyst
нт	diphenyl methane	decalin	biphenyl	benzene toluer.e	350 C	none
нт	diphenyl methane	decalin	biphenyl	benzene toluene	350 C	FeCl ₃ / SiO ₂ - Al ₂ O ₃
HDO	dibenzyl ether	decalin	biphenyl	toluene xylenes	340 C	none
HDO	dihenzyl ether	decalin	biphenyl	toluene xylenes	300 C	CoMo/γ- Al ₂ O ₃
HDN,HDS & HDO	indole diphenyl sulfide diphenyl ether	trimethyl benzene	dodecane	benzene 4-amino- benzonitrile 2-ethyl- benzenamin e	300 C	CoMo/y- Al ₂ O ₃

	TABLE II				
Rea	ctor Conditions:				
•	Reactor	Autoclave Engineering, Inc. (Penn.)			
-	Reactor Volume	50 cc			
-	Pressure	1600-1650 psi			
-	Feed Flow Rate	30 cc/hr			
-	Reaction Gas	continuous flow H, 50 sccm			
-	Heating Speed	ambient> 300 C in ~18 min			
•	Final Reaction Temperature	thermal reaction 340 C, catalytic reaction 300 C			
-	Catalyst	~1 g sulfonated COMO/r-Al ₂ O ₃			
Pres	sure Reduction Line Conditions:				
-	Pressure Reduction Line	1 m x 10-15 um i.d. fused silica capillary tube			
-	Temperature	175 C			
-	Pressure	1600-1650 psi> ambient pressure			
-	Liquid Flow	~0.1 ml/min			
Sam	ple Inlet Conditions:				
•	Temperature	270 C			
-	Pressure	ambient pressure			
-	Dilution He Flow Rate	100 ml/min			
-	Carrier Gas He Flow Rate	40 ml/min			
•	Sampling Valve Flow Rate	43 ml/min			
-	Bleed Flow Rate	10 ml/min			
-	Sampling Pulse	550 ms at 2 min intervals for dibenzyl ether			
		550 ms at 3 min intervals for model compound			
		mixtures			
Tran	sfer Line Conditions:				
-	Column	1 m x 150 um i.d. coated with 0.12 um CP-SIL 5CB			
-	Temperature	dibenzyl ether reaction 105 C			
		model compound mixture reaction 80 C			
-	Pressure	ambient> 10 ⁶ torr			
MS	Conditions:				
-	Mass Spectrometer	Finnigan MAT Ion Trap MS			
-	Pressure	10 ⁴ torr			
-	Ion Trap Temperature	96 C			
•	Ionization	electron impact (with automatic gain control)			
-	Spectrum Scanning Speed	4 spectra/s			
•	Mass Range	m/z 50-200			

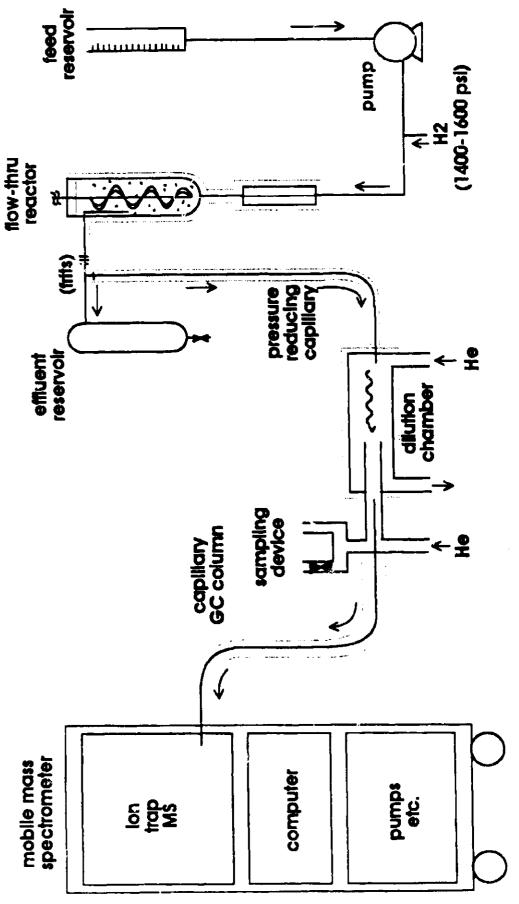


Figure 1. On-line GC/MS monitoring of ... igh pressure reactor.

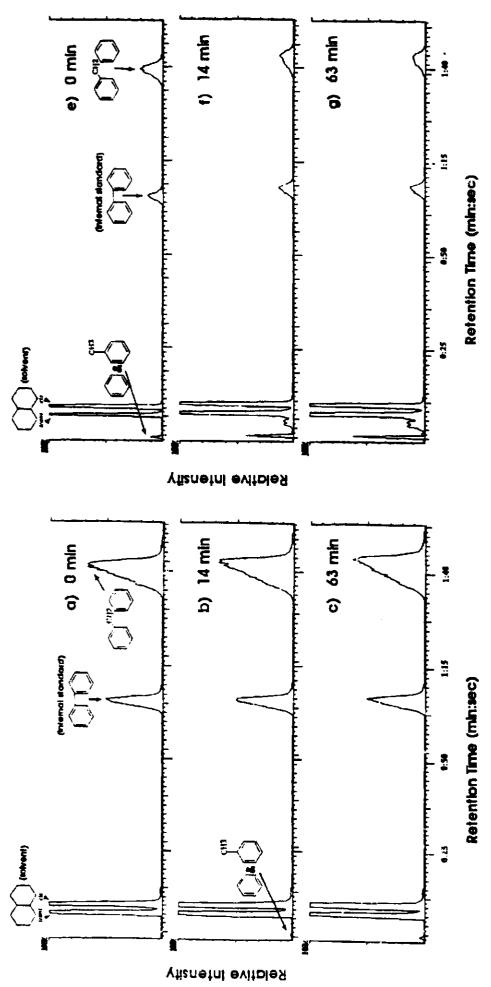


Figure 2. Total ion chromatogram profiles obtained at 350 C, for different reaction times of diphenyl methane under thermally (a-c) and catalytically (d-f) controlled hydrotreatment conditions. Note GC separation of decalin solvent isomers.

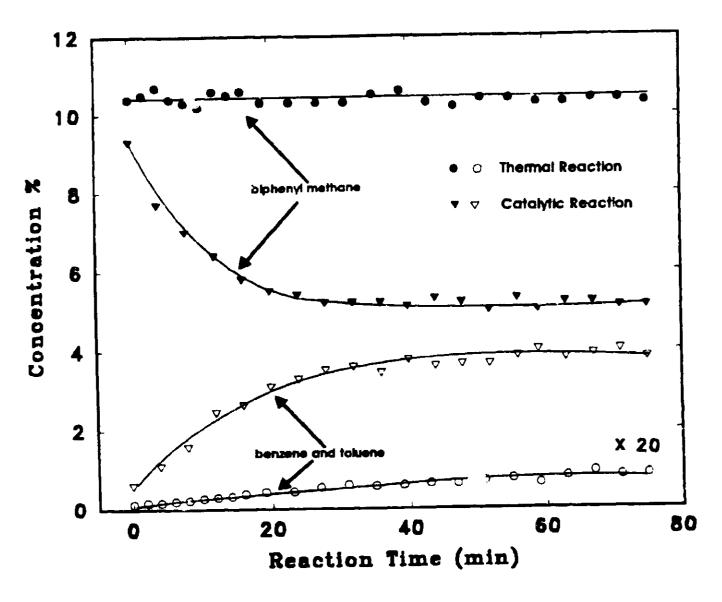
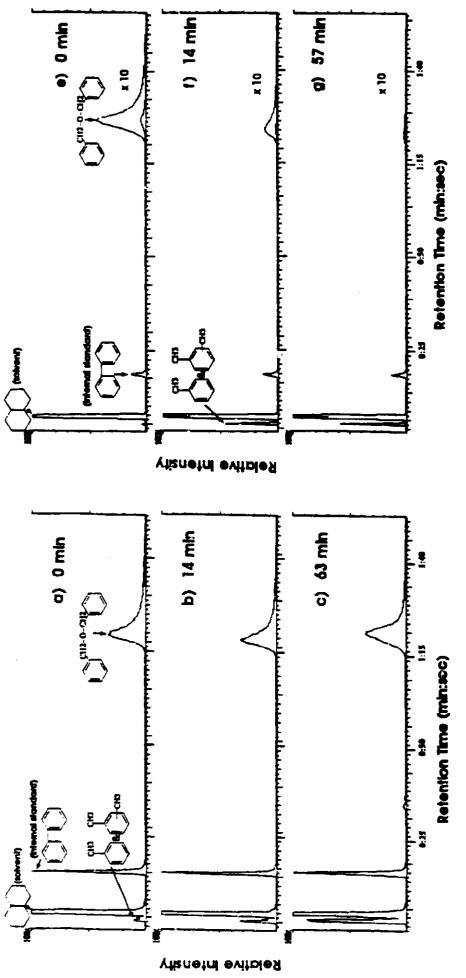


Figure 3. Kinetic profiles of diphenylmethane conversion (\bullet, \forall) and benzene and toluene formation $(\bigcirc, \triangledown)$ under thermally (\bullet, \bigcirc) and catalytically (\forall, \triangledown) controlled conditions. Note major increase in reaction rate in the presence of catalyst.



reaction times of dibenzyl ether under thermally (a-c) and catalytically (d-f) controlled hydrodeoxygenation conditions, respectively. Figure 4. Total ion chromatogram profiles obtained at 340 C and, 300 C for different

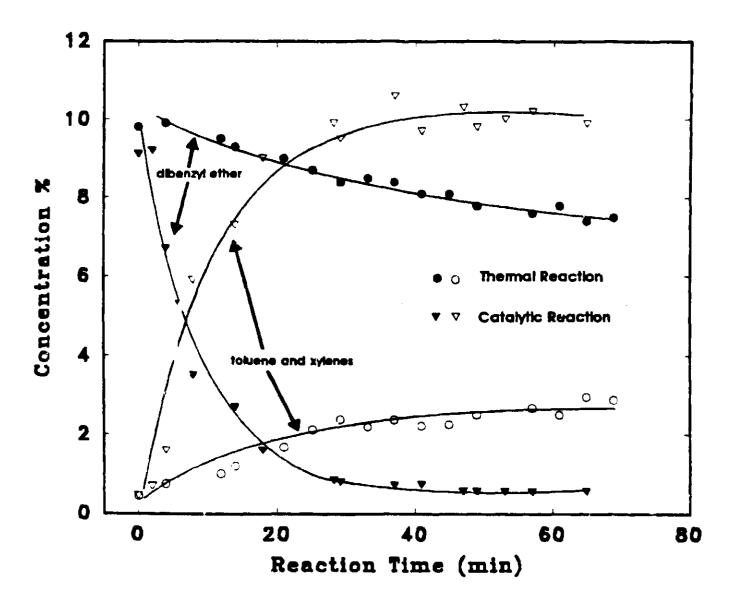


Figure 5. Kinetic profiles of dibenzylether conversion (\bullet . \forall) and toluene and xylenes formation (\bigcirc . ∇) under thermally (\bullet , \bigcirc) and catalytically (\forall , ∇) controlled conditions.

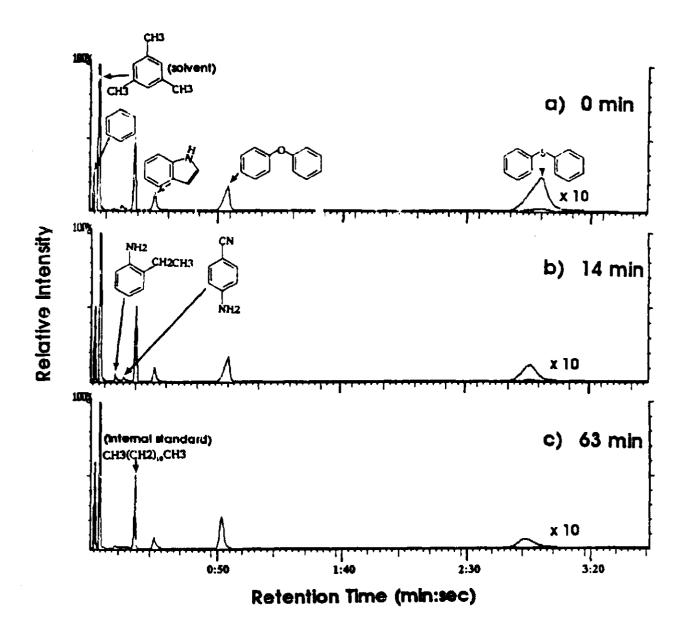


Figure 6. Total ion chromatogram profile obtained at 300 C, for different reaction times of diphenyl ether, indole and diphenyl sulfide under catalytically controlled hydrode(oxygen)(nitrogen)(sulfuriz)ation conditions.

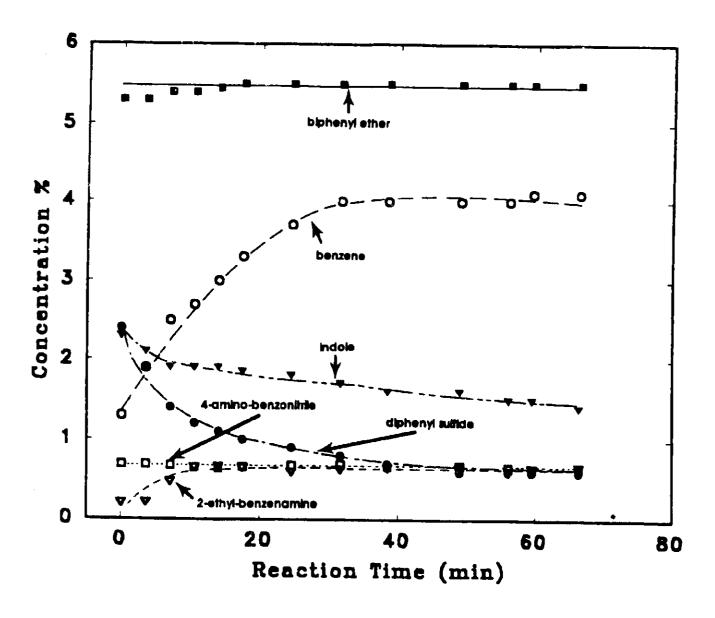


Figure 7. Kinetic profiles of diphenyl ether, indole and diphenyl sulfide conversion ($\blacksquare, \blacktriangledown, \bullet$) as well as benzene, 2-ethyl-benzenamine and 4-amino-benzonitrile formation ($\bigcirc, \blacktriangledown, \blacksquare$) under catalytically controlled conditions.