STUDIES ON THE MANUFACTURE

OF AVIATION GASOLINE BY

HIGH PRESSURE HYDROCRACKING

OF SOYA BEAN OIL

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SUMMARY

The object of this project was to determine the optimum—operating conditions in the hydrocracking of soya bean oil for the manufacture of high octane aviation fuel. It was found that by hydrocracking soya bean oil over MoS₃ catalyst at 1.0 space velocity, 200 kg/cm² hydrogen pressure, and temperature of 420-450°C., an aviation gasoline was obtained in 40% yield, which had an octane number (with 0.15% lead) of 80-85.

I. INTRODUCTION

This project was started in January 1945 in order to obtain an additional source of high quality aviation fuel. No previous reports or data were available on this subject.

In order to find comparatively good conditions for hydrocracking soya bean oil, experiments were first made in small autoclaves of 2-5 liters capacity. Molybdenum sulphide, (MoS3), was selected for use in the pilot plant after testing several catalysts, including molybdenum oxide (MoO3), nickel oxide (NiO), tungsten oxide (WO3) and copper oxide (CuO). The optimum reaction temperature and hydrogen pressure were determined to be in the range of 420-450°C and 200 kg/cm², respectively. Next, experiments were performed in the small scale, continuous type pilot plant. The pilot plant used was the same as that described in the authors report on the hydrocracking of pine root oil. Although many unsolved problems still remain, the results are given in the following paragraphs

II. EXPERIMENTAL RESULTS

Properties of the raw material are tabulated below:

Specific	Gravity d15	0.9204
Boiling Todine V	Point OC	300–320
Sanonifi	cation Value	165.31

Records of experimental data obtained on autoclave scale were destroyed in August 1945. Pilot plant data are summarized in Tables I(B)18 and II(B)18.

The main problem in this process was to discover the best catalyst capable of producing aviation gasoline with at least 91-95 octane number. Various additional catalysts were subsequently tested on autoclave scale, including Cr₂O₃, Fe₂O₃, Fe₃, VO₂, TiO₂, and their mixtures, but only with TiO₂ catalyst was it possible to produce a superior gasoline with an octane number of 87. Pilot plant tests were made on MoS₃, which was the best known prior to discovery of the TiO₂, but it had a short life and produced a lower octane gasoline.

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ENCLOSURE (B) 18

III. COMOLUSIONS

An aviation gasoline of sufficiently high octane number could not be obtained from soya bean oil by means of high pressure hydrocracking with MoS3 catalyst. The most important problem for future study is the discovery of a more active catalyst for this type of hydrocracking. Because soya bean oil is composed of long paraffinic chains having many unsaturated double bonds, it is possible to convert it into iso-paraffinic or naphthenic hydrocarbons with high octane value. Therefore it is believed desirable to continue this study, putting stress on catalyst investigations. As a result of these experiments, it was shown that an aviation gasoline of 80-85 octane number (0.15% lead) could be obtained in yield of about 40% from raw soya bean oil under reaction conditions of 200 kg/om² hydrogen pressure, temperature of 420-450°C and space volocity about 1.0 over MoS3 catalyst.

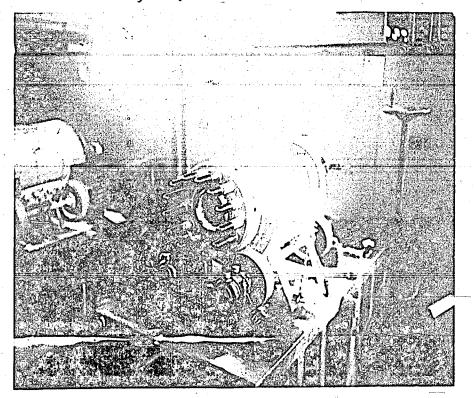


Figure 1 (B) 18
AUTYCLIAVE (51) PSED IN THE CRACKING OF SOYA BEAN OUL

Table 1(B)18

REACTION CONDITIONS & YIELDS (Pilot Flent Test Date)

		Run So.				
		1	2	3	4	
	Catalyst	Mo3 ₃	MoS ₃	MoS ₃	Mo33	
	Reaction Temperature OC	420	430	450	470	
	Preheaters Temperature °C	300	300	300	300	
America against a co	Reaction Pressure kg/cm2	200	200	200	200	
Reaction Conditions	.Charged Oil lit/hr	2,89	2,68	2,93	3.05	
Conditions	Total Charged Oil lit	23.17	5.77	17.59	24.40	
	Charged Hydrogen Gas m3/hr	3.29	3.12	3.44	3,11	
	Total Charged Hydrogen Gas m3	26.36	6,24	20,64	24.93	
	Space Velocity (Idquid)	1.0	1.0	1.0	1,0	
	Run Length hrs.	В	2 .	6	8	
	Total Idquid Products lit.	22,27	5.82	14.60	17,32	
!	Liquid Products lit/hr	3.22	2,91	2.46	2,16	
	Total Discharged Gas m3	15,39	4.16	13,38	16,12	
Products	Discharged Gas m3/hr	1.94	2,08	2,26	2,01	
	Water-wt≸ of Charged 011	1,71	1,16	2.42	2,06	
,	Absorbed H2-st\$ of Charged 011	5,68	4.56	5.42	4,81	
	Yield-wt% of Charged Oil	78.6	82,4	65.6	56.2	
	Kield-vols of Charged Oil	96.1	100,0	84.1	70,9	
	Acidic Matter is Cracked Oil Yols	2.0	0	0	0	
* * .	Indine Value (I. V.)		12,17	6.97	19,16	
	Saponification Value (S.V.)		0.536	1,369	0,69	
•	Specific Gravity (S.G.) d.15	0,7566	0,551	0,7200	0,73	
	Initial Boiling Point (I.B.P.) C	43.5	40.5	34.0	39.0	
	10% Boiling Point °C	93.0	72.5	58.5	65,5	
·	20% Boiling Point CG	126,2	94.5	74.5	91.0	
Cracked	30% Boiling Point C	165,0	119,0	89.0	109,0	
017	40% Boiling Point CC	222,2	248,0	90,6	136,0	
	50% Boiling Point 90	270.2	168.0	128.0	170.5	
	60% Boiling Point 40	296,0	234.5	253.5	215.0	
	70% Boiling Point 90	304.2	292,5	210.0	274.0	
w 1	80% Boiling Point 90	309.5	306,0	270.0	303.2	
	90% Boiling Point CC	318,0	313.0	308,0	316,0	
,	Final Boiling Point (F.B.P.) C	343.0	336.0	311.0	334,0	
`	Total Distillate Vols	97.0	96,5	95.0	94.0	
	Residue VolS	0.5	1.5	1,35	0,8	
	Loss Yold	2.5	2,0	3.65	5,2	
	CO2 Yels	0.1	0.2	0,1	10,2	
		0	0,1	0,1	0.3	
Residual Gas		5,9	5.6	5.0	4.8	
Composition	C _n H _{2m} Vol\$	0.2	0.2	0,3	0,2	
		61.2	12.0	78.9	78,8	
	H ₂ Vols	erra .	12,0	10,7	,,,,	

Table 11(B)18

PROPERFIES OF AVIATION CASOLIES PRODUCED (Pilot Plant Test Date)

The second second			Bun Ho.				
		1	2	3	4		
Reaction	Reaction Temperature CC	420	430	450	470		
Conditions	Specific Gravity (S.G.) d15	0,7030	0,6916	0,6910	0.6901		
	Acidic Matter in Aviation Gasoline Vols	0	0	0	0		
	Initial Boiling Point (I.B.P.) %	39.0	45.0	39.0	40.0		
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10% Boiling Point °C	67.0	65.0	59.0	<i>5</i> 9.0		
	20% Boiling Point °C	77.0	75.0	72.5	66.5		
· · · · · · · · · · · · · · · · · · ·	30% Boiling Point °C	88.5	85.5	81.5	74.2		
	40% Boiling Point °C	98.4	94.0	90.0	78.0		
e in a service of the	50% Boiling Point °C	107.6	102.0	98.0	89.0		
	60% Boiling Point OC	119.0	111.0	109.0	99.0		
Fractional Distillation	70% Boiling Point ℃	129.0	120.0	120.0	107.0		
Distillation	80% Boiling Point °C	139.9	131.0	133.0	121.0		
	90% Boiling Point °C	156.8	145.5	155.5	132,2		
	97% Boiling Point °C	185.0	170.0				
	Final Boiling Point °C	188.0	185.5	177.0	164.0		
	Total Distillate Vol%	97.4	98.0	93.0	95.0		
	Residue Vol%	0.12	0,6		1.0		
	Loss Vol%	2.45	1.4	. 4. 6.51.000	4.0		
	Yield-Vol% of Cracked Oil	31.7	48.0	64.9	51,0		
. •	Unsaturated Hydrocarbon (U.) Vol%	. 0	4.0	0	0		
	Aromatic Hydrocarbon (A.) Vol%	6.0	8.0	16.0	8.0		
composition	Naphthenic Hydocarbon (N.) Vols	6.0		7.8	14.4		
	Paraffinic Hydrocarbon (P.) Vol%	88.0	88.0	76.2	77.6		
	Aniline Point (A.P.) %	68.1	71.1	67.2	65.3		
ctane umber	Clear	. 59.1	58.0	60.3	62,3		
u4001	With 0.15% of Lead	83.0	83.4	85.3	85.4		