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43828 E/22 E17 H04 SHEL 12.12.80 (E(10-E4E, 10-H1) H(4-E5) N(2, 3-B, 3-D) SHELL INT RES MIJ BV *BE -891-195 12.12.80-NL-006751 (21.05.82) C07b C07c Prodn. of oxygenate(s) and paraffin(s) from synthesis gas - by oxygenate synthesis followed by paraffin synthesis from unconverted gas

Prodn. of oxygenates and paraffinic hydrocarbons is effected in a two-stage process where in the first synthesis gas with an H₂/CO molar ratio of at least 0.5 is contacted with a cataly st (I) contg. one or more metals capable of catalysing the conversion of synthesis gas to oxygenates. If the H₂/CO molar ratio in the 1st-stage effluent is at least 1.5, the 2nd stage is effected by contacting the CO and H2 components of the 1st-stage effluent (opt. together with other components) with a catalyst (IIa) contg. one or more metals (Co, Ni and/or Ru) capable of catalysing the conversion of synthesis gas to paraffinic hydrocarbons. If the H₂/CO molar ratio in the lst-stage effluent is less than 1.5, H2O is added in an amt. sufficient to react with CO and thus increase the H₂/CO ratio to at least 1.5, and the catalyst (IIb) in the 2nd stage also contains one or more metals capable of catalysing CO shift conversion.

ADVANTAGES

The process avoids problems associated with recycle of

unconverted synthesis gas to the 1st stage.

DETAILS

catalyst.

The initial synthesis gas is pref. produced by steam gasification of carbonaceous material at 900-1500°C and 10-100 bar and has an H₂/CO ratio of 0.75-2.5. If the H₂/CO ratio is too low, it can be increased by external or internal shift conversion.

The 1st stage is pref. effected at 225-325°C and 50-150 bar using a catalyst capable of converting synthesis gas to methanol and dimethyl ether. The 2nd stage is pref. effected at 175-275°C and 5-100 bar. A specified catalyst of type (IIa) comprises 10-40 pts. wt. Co and 0.25-5 pts. wt. Zr, Ti and Cr on 100 pts. wt. SiO2. Catalysts of type (IIa) can be used in alternate layers with a shift conversion

The oxygenates can be sepd. from the 1st-stage effluent and converted to elefine and/or aromatics by a specified additional process. Alternatively, the whole 1st-stage effluent can be passed to the 2nd stage, in which case the 2nd-stage effluent can be treated to recover Cc. hydrocarbons and the remainder then subjected to the additional BE-891195+ process. In another claimed embodiment, the whole lst-stage effluent is subjected to the additional process and the effluent from this process (after separating C4-olefins) is used as feed in the 2nd stage. (30pp 367).