FOSX 10.02.86 E(10-E4E1) H(4-E5) N(6) 87-229832/33 E17 H04 *EP -233-076-A FOSTER WHEELER ENER 10.02.86-US-827558 (19.08.87) C07c-29/15 C07c-31/04 (e) mixing the effluent gas from (d) with a H,-rich Prodn. of organic cpd., e.g. methanol, from hydrocarbon feed - via syn-gas prodn, in prim, and sec. reformers with recycle of hydrogen stream to form a final syngas stream; (f) injecting the final syngas into a synthesis loop, obtd. from purge gas forming organic cpds, therein, and extracting a purge gas R(DE ES FR GB IT NL) C87-096910 stream therefrom: (g) physically sepg. the purge gas stream into a H2-Prodn. of an organic cpd. from a hydrocarbon-contg. feedrich stream and a residual gas stream; and (h) recycling at least part of the H,-rich stream to step stock comprises: (a) dividing the feedstock into 2 fractions; (e). (b) subjecting the 1st fraction to primary steam reform-USE/ADVANTAGE ing by mixing with steam and heating the mixt, by indirect Feedstocks ranging from CH, to naphtha can be conheat exchange in presence of a reforming catalyst, to form verted to e.g. MeOH. The investment cost of the overall an H2-contg. gaseous effluent at 650-850°C. MeOH plant is reduced by reducing the size of the steam (c) mixing the effluent gas from (b) with the 2nd reforming heater. The size and wt. of the plant is reduced fraction from (a); making it easier to build as a large-scale single-stream plant (d) reacting in a single stage the gas mixt. from (c) or on ship or barge. Like BP 1,569,014, the invention with an O,-rich gas in a secondary reformer operating allows high-pressure operation by steam reforming at essentially adiabatically and contg. a single catalyst bed, to unusually low temp., but, unlike the BP, balancing of give a syngas at 850-1250°C contg. a & CH, equivalent of primary and secondary reformers is unnecessary: therefore less than 1/10th of that of the gas mixt. from (c) and with much less reforming is performed in the primary reformer. a z ratio of 0.80-1.00 (z = moles $H_2/(2(moles CO) + 3(moles$ which reduces the cost of the plant. EP-233076-A+ CO2)));

PREFERRED CONDITIONS The temp, of the effluent gas from (b) is pref. about 720-780°C, and that from (d) is pref. about 950-1100°C. The pressure in (b) and (d) is pref, above 30 bars. The O, rich gas used in (d) pref. contains at least 80 (esp. at least 95) vol. & O2. Pref. the effluent gas from (d) has z = 0.88-0.98, and that from (e) has z = essentially 1.00. The 1st fraction of the feedstock, treated in (b) is pref. 5-60 (esp. 10-30)% of the whole. PURGE GAS TREATMENT The purge gas may be shift converted by reacting with steam in presence of a shift catalyst, and the mixt. then physically sepd. (step (g)), with opt. CO2 removal before physical sepn. Physical sepn. may be effected by molecular sieve, selective membrane diffusion or low-temp, distn. (43pp1492CGDwgNo0/5) (E)ISR: No Search Report EP-233076-A